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HIGHLIGHTS

Aluminium Stiffener Panel

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Emission and Performance

Cavitation of Propeller

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CFD Simulation for Cavitation of Propeller Blade

By O. O. Sulaiman, A.S.A.Kader, W.B.Wan Nick & A.H. Saharuddin

Universiti Malaysia Terengganu

Abstract - Propeller cavitation is a major problem in ship operation and the costs of repair and maintenance is high for ship-owners. Proper design of propeller plays a very important role in life cycle and the performance of a vessel. The use of simulation to observe various parameters that affect cavitations can be helpful to optimize propeller performance. This project designs and simulates cavitations flow of a Kaplan series, Fixed Pitch Propeller (FPP) of a 48-metres Multipurpose Deck Ship at 11 knots. Simulation test was carried out for laminar and turbulent flow using Computational Fluid Dynamics (CFD) approach to observe cavitations occurrence at selected radius.

Keywords : *Simulation, cavitation, performance, propeller, CFD.*

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CFD Simulation for Cavitation of Propeller Blade

O. O. Sulaiman^α, A.S.A.Kader^σ, W.B.Wan Nick^ρ & A.H. Saharuddin^ω

Abstract - Propeller cavitation is a major problem in ship operation and the costs of repair and maintenance is high for ship-owners. Proper design of propeller plays a very important role in life cycle and the performance of a vessel. The use of simulation to observe various parameters that affect cavitations can be helpful to optimize propeller performance. This project designs and simulates cavitations flow of a Kaplan series, Fixed Pitch Propeller (FPP) of a 48-metres Multipurpose Deck Ship at 11 knots. Simulation test was carried out for laminar and turbulent flow using Computational Fluid Dynamics (CFD) approach to observe cavitations occurrence at selected radius. The parameters considered are pitch angle, angle of attack, viscosity of sea water, operating vapour pressure in the sea water, engine power, lift and drag vectors of each of the blade sections, and resultant velocity of the fluid flow. Comparison of performance is made and it compares well with the theory. Thrust coefficient (K_T), torque coefficient (K_Q), thrust (T), advance coefficient (J), and cavitations number (σ), were calculated to deduce efficiency and validate the model. The study can be used to build a prototype physical model that could be beneficial for future additional experimentation investigation.

Keywords : Simulation, cavitation, performance, propeller, CFD.

1. INTRODUCTION

A marine propeller is a propulsion system which turns the power delivered by the engine into thrust to drive the vessel through water. Propeller cavitation is a general problem encountered by the ship owner, whereby it causes vibrations, noises, degradation of propeller performance, decreases engine efficiencies, effects the life cycle of the ship and also results in high cost of maintenance. The basic physics of cavitation occurs when the pressure of liquid is lower or equal to the vapour pressure, which depends on the temperature, thus forming cavities or bubbles. The compression of pressure surrounding the cavities would break the cavities into smaller parts and this increases the temperature. Collapse of bubbles in contact with parts of the propeller blades will create high localised forces that subsequently erode the surface of the blades. Simulation on cavitating flow using CFD can be carried out to determine the performance of the propeller. A model is generated in Gambit and fluid-flow physics are applied to predict the fluid dynamics and other physical phenomena related to the propeller. Ref. [1] stated that, CFD can provide potential flow analysis such as flow velocities and pressure at every point in the

problem domain as well as the inclusion of viscous effects.

a) Previous studies on propeller cavitation

Ref. [2] in their studies, generated hybrid grid of about 187 000 cells using Gambit and T Grid. The blade surface was firstly meshed with triangles including the root, tip and blade edges. The turbulent boundary layer was resolved with four layers of prismatic cells between blade and hub surfaces. In the cavitating propeller case, the boundary conditions were set to simulate the flow around a rotating propeller in open water. Inlet boundary, velocity components for uniform stream, blade and hub surfaces, and outer boundary were included. This ensured the rotational periodicity of the propeller on the exit boundary by setting the pressure corresponding to the given cavitation number and other variables was later extrapolated [3,11]. On the other hand, [3] applied a mixture of models with algebraic slip to simulate cavitating flow over a NACA 66 hydrofoil. This multiphase flow model which used incompressible fluids consisting of liquid and vapour was used as primary and secondary phase respectively. Structured quadrilateral grids of 19 490 cells were meshed. Inflow and outflow boundary were indicated as velocity magnitude and direction and zero gauge pressure respectively. Contour of vapour volume fraction shown in Figure 1 indicates that cavity can be observed at the mid-chord region [4,12].



Figure 1 : Cavity at the mid-chord region

This study is focussed mainly on simulating a cavitating flow at the propeller blade section of Kaplan series in order to optimize the propeller blade to increase its performance. Two-dimensional simulations of different radii were carried out at different revolutions per minute (rpm) and the results were compared based on the pressure difference. The objective is to simulate and investigate the water flow at the propeller blade

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section and to recommend measures to reduce cavitation in order to increase its efficiencies [4, 5].

II. METHODOLOGY

a) Model generation in Gambit

The Propeller Blade models of 0.2R and 0.6R were generated and computational domains were created to assume water is flowing from far towards the Propeller Blade. Figure 2 and Table 1 show far-field boundary conditions surrounding the Propeller Blade. Then, meshing was carried out between the boundaries and Propeller Blade to determine the accuracy of the model generation. Figure 3 and 4 show the meshing process [6, 13, 14].

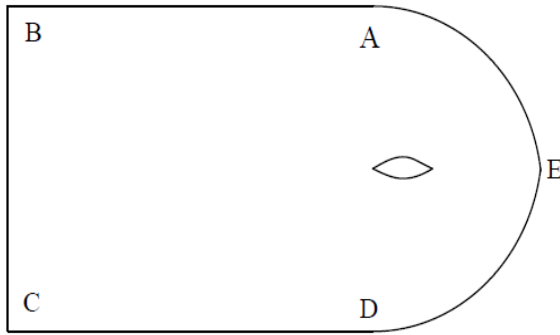


Figure 2 : Creation of far -field boundaries to simulate the fluid behaviour in Fluent.

Table 1 : Boundary conditions for simulating fluid behaviour

Curve	Boundary condition
AED	Far field 1
AB	Far field 2
CD	Far field 2
BC	Far field 3

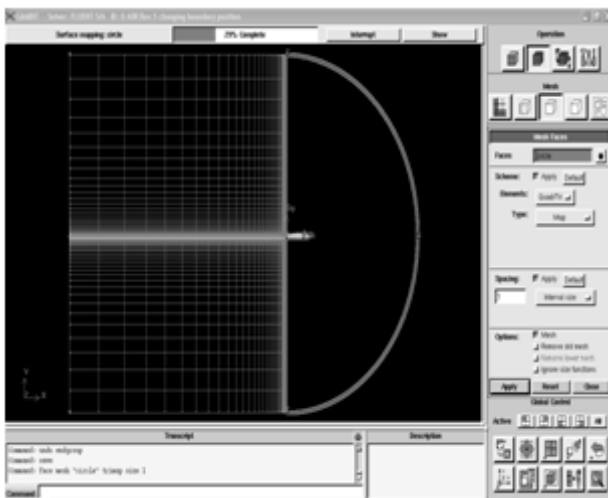


Figure 3 : Meshing process of 0.2R Propeller Blade section

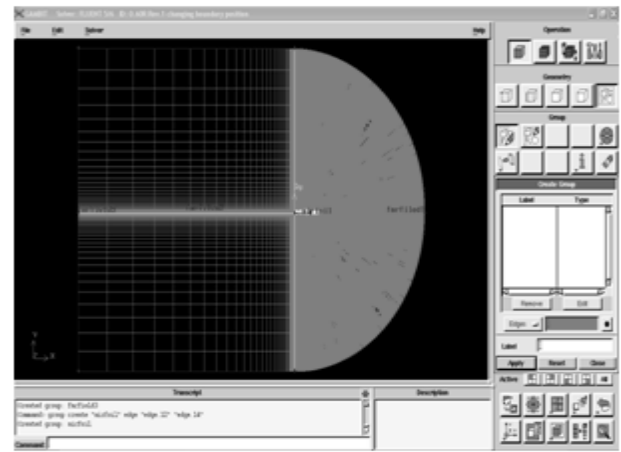


Figure 4 : Meshing result of 0.2R Propeller Blade section with boundaries creation

b) Numerical method

Propeller blades of 0.2R and 0.6R were simulated in Fluent 6.3.26. Pressure-based numerical solver, laminar and turbulent physical model were selected as the functioning base for 300rpm and 600rpm. Then, the material properties, for instance, the density of sea water and viscosity value were defined and calculated based on Table 2.. Consequently, the operating condition was set to be 2296 Pa, which is the condition for vapour pressure at sea water when the temperature is 20°C. On the other hand, the boundary conditions of far field 1 and far field 2 were specified as velocity inlet, whereby the velocity magnitude and direction were calculated[7,8].

As for far field 3, this boundary was specified as pressure outlet; the gauge pressure was set to be 0 Pa. The existence of inflow and outflow boundaries enables the characteristics of fluid to be observed by entering and leaving the flow domain. The turbulent viscosity ratio was set to correspond to the default value for 600rpm of both radii. Next, the solution procedure was set as simple algorithm, and under *discretisation*, the pressure and momentum were set as Standard and First Order Upwind respectively [9,10].

Table 2 : Water properties (Tupper, 2004)

Temperature (°C)	Density (kg/ m ³)		Kinematic viscosity (m ² /s x 10 ⁶)	
	Fresh water	Salt water	Fresh water	Salt water
0	999.8	1028.0	1.787	1.828
10	999.6	1026.9	1.306	1.354
20	998.1	1024.7	1.004	1.054
30	995.6	1021.7	0.801	0.849

At the temperature of 20°C, the density of sea water is 1025 kg/m³, and the kinematic viscosity is 1.054 x 10⁶ m²/s. Thus, in order to insert the value of dynamic

viscosity in Fluent, the following formula was used to convert kinematic viscosity to dynamic viscosity.

$$\text{Dynamic viscosity} = \text{kinematic viscosity} \times \text{density} \quad (1)$$

Therefore, the calculated dynamic viscosity is $1.08035 \times 10^{-9} \text{ kg/m.s}$.

Consequently, the operating condition was set to be 2296 Pa based on Table 3, which is the condition for vapour pressure at sea water when the temperature is 20°C.

Table 3 : Saturation vapour pressure, P_v for fresh and sea water (Carlton, 2007)

Temperature (°C)	0.01	5	10	15	20	25	30
Fresh water, P_v (Pa)	611	872	1228	1704	2377	3166	4241
Sea water, P_v (Pa)	590	842	1186	1646	2296	3058	4097

On the other hand, the boundary conditions of far field 1, far field 2 and far field 3 were specified to accommodate the fluid behaviour. Far field 1 and far field 2 were specified as velocity-inlet, whereby the velocity magnitude and direction were calculated as the following:

For 0.2R airfoil section profile,

$$\text{Pitch angle, } \theta = \tan^{-1}\left(\frac{P}{2\pi r}\right), \quad (2)$$

where, P is pitch and r is radius of the blade section

Thus, resultant velocity of the fluid flow at 0.2R is calculated as,

$$\text{Resultant velocity, } v = \left(\frac{2\pi r n}{\cos \theta}\right), \quad (3)$$

Where, n is equal to the rotational speed of the propeller

$$\text{Resultant velocity, } v = \left(\frac{2\pi r n}{\cos \theta}\right), \quad (4)$$

Velocity-inlets at both far fields were then indicated as 729 m/s for 0.2R airfoil section. As for far field 3, this boundary was specified as pressure-outlet, whereby the gauge pressure was set to be zero Pascal. The existence of inflow and outflow boundaries enables the characteristics of fluid to be observed by entering and leaving the flow domain. Parameters in the solution control were set up to select the suitable iterative solvers. Under *pressure-velocity coupling*, the solution procedure was set as SIMPLE algorithm, which equipped an accurate linkage between pressure and velocity. SIMPLE algorithm was used due to the assumption of steady flows. Besides, under *discretization*, the pressure and momentum were set as Standard and First Order Upwind respectively. The First Order Upwind was set due to convection terms in solution, thus the face value would be set to cell-centre

value. This was done before any CFD calculation was performed. The solution was then initialised and computed from far field 1.

Monitoring of the convergence of the solution was performed. There were three differential equations to be solved in a two-dimensional incompressible laminar flow problem, which indicated the three residuals to be monitored for convergence, that is, *continuity*, *x-velocity* and *y-velocity*. The default convergence criteria were set as 0.001 for all three of these. As the code iterates, the *residuals* were calculated for each flow of equation. These residuals represented an average error in the solution. Moreover, monitoring lift and drag force was carried out and calculated as following:

For 0.2R airfoil section profile,

$$\text{Angle of attack, } \alpha = \left(\frac{2f_{\max}}{C}\right) \quad (5)$$

Where, $f_{\max}$ is thickness of the airfoil section and C is chord length of the airfoil section

$$\text{Angle of attack, } \alpha = \left(\frac{2f_{\max}}{C}\right) \quad (6)$$

Lift force is defined as a force perpendicular to the direction of the freestream. Therefore, X and Y are formulated as *sin* θ and *negative cos* θ , respectively, as shown in Figure 5.

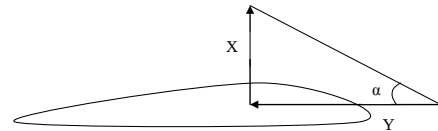


Figure 5 : A lift force vector of an airfoil section profile

To calculate the lift force vector of an airfoil,

$$X = \sin \alpha \text{ and } Y = -\cos \alpha \quad (7)$$

Where, α is the angle of attack

$$\begin{aligned} X &= \sin 55^\circ \\ &= \underline{0.8192} \\ Y &= -\cos 55^\circ \\ &= \underline{-0.5736} \end{aligned}$$

Therefore, lift force vector at X and Y was 0.8192 and -0.5736 respectively.

As for the drag force vector, it is defined as the force component in the direction of the freestream. Thus, X and Y are formulated as *negative cos* θ and *sin* θ respectively, as shown in Figure 6.

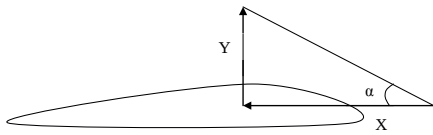


Figure 6 : A drag force vector of an airfoil section profile

To calculate the lift force vector of an airfoil,

$$X = -\cos \alpha \text{ and } Y = \sin \alpha \quad (8)$$

Where, α is the angle of attack

$$\begin{aligned} X &= -\cos 55^\circ \\ &= -0.5736 \end{aligned}$$

$$\begin{aligned} Y &= \sin 55^\circ \\ &= 0.8192 \end{aligned}$$

Therefore, lift force vectors at X and Y were – 0.5736 and 0.819 respectively.

The solution was solved and iterated in order to remove the unwanted accumulations, so that the iterative process would converge rather than diverge. A converge solution is usually achieved when the residuals fall below some convergence criteria, that is 0.001. Besides examining residuals, variables such as lift and drag force were monitored to find out the convergence of the numerical computations.

Last but not least, the CFD results were visualised and analysed at the end of the computational simulation in different categories, such as vector plots and contour plots for a better relevant physical characteristics view within the fluid - flow problem.

The simulation process was repeated by inserting various operating pressure values below 2296 Pa in order to observe the pressure difference for cavitation to occur and also to examine the sensitivity for accuracy of the results and performance. Finally, document the findings of the analysis.

III. RESULTS AND DISCUSSIONS

Three Propeller Blade section profiles at different radii, such as 0.2R, 0.6R and 1.0R were simulated. The CFD results were then visualised and analysed for comparison.

a) Result of 0.2R Propeller Blade section

The CFD results, for instance, three residuals of CFD calculation, lift and drag force, velocity vector plot, and contour plot were visualised and analysed

b) Iteration 0.2R

Figure 7 shows 250 iteration results, whereby the continuity, x-velocity and y-velocity were calculated for flow equation.

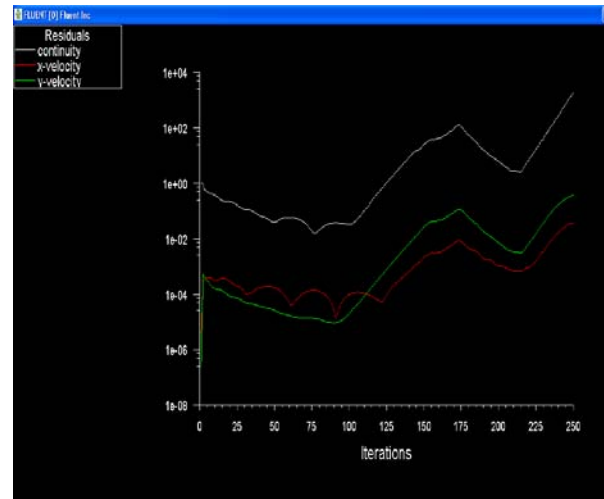


Figure 7 : Iteration results of three residuals

Based on Figure 6, it can be seen that the residuals were moving upwards and not fulfilling the converging criteria, that is to be below 0.001. This shows that the solution was diverging instead of converging. As for the lift and drag vector force, Figure 8 and 9 shows a divergence result which is not compatible with the convergence criteria.

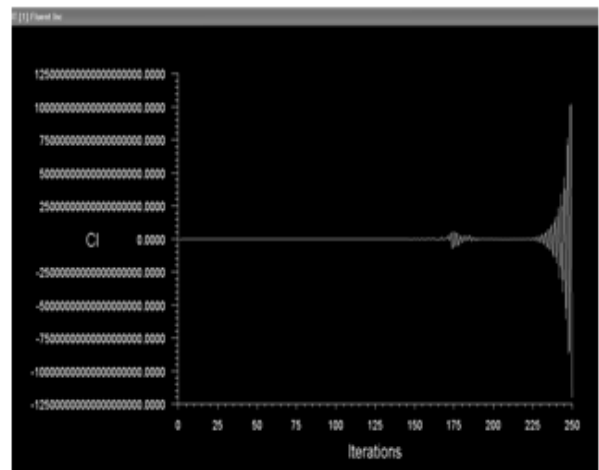


Figure 8 : Lift vector force iterated by CFD solver

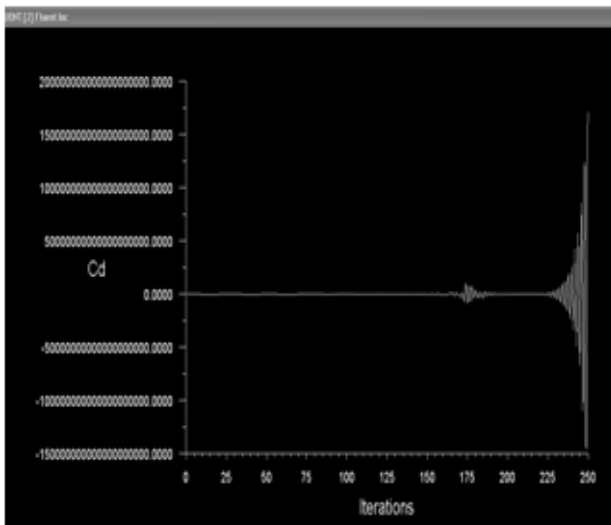


Figure 9 : Drag vector force iterated by CFD solver

c) *Contours of Velocity Vectors*

Laminar flow of 0.2R Propeller Blade section at 300rpm is observable in Figure 10. There is no pressure gradient observed surrounding the Propeller Blade section. This indicates that the possibility of cavitation to occur is very small.

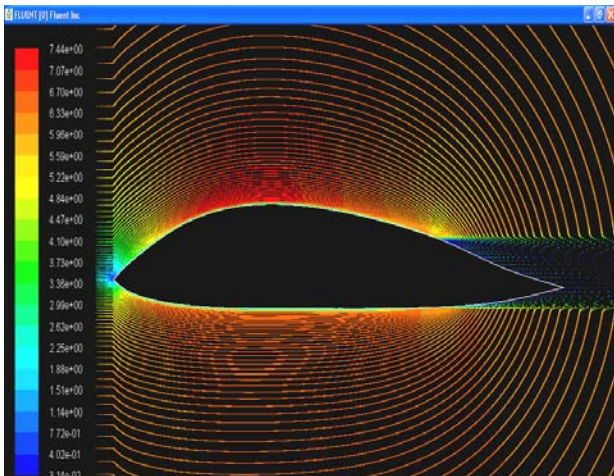


Figure 10 : Contour of velocity vector of 0.2R at 300rpm and 600rpm

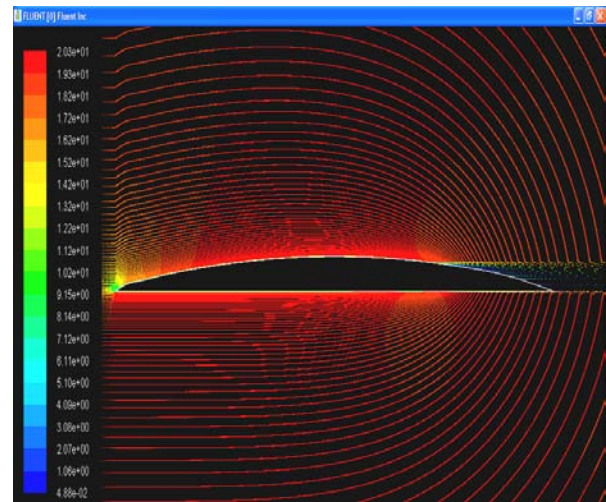


Figure 11 : Low velocity vector of 0.6R at leading and trailing edge at 300rpm and 600rpm

d) *Contours of Absolute Pressure*

Laminar flow of 0.2R Propeller Blade section at 300rpm is observable in Figure 12. There is no pressure gradient observed surrounding the Propeller Blade section. This indicates that the possibility of cavitation to occur is very small.

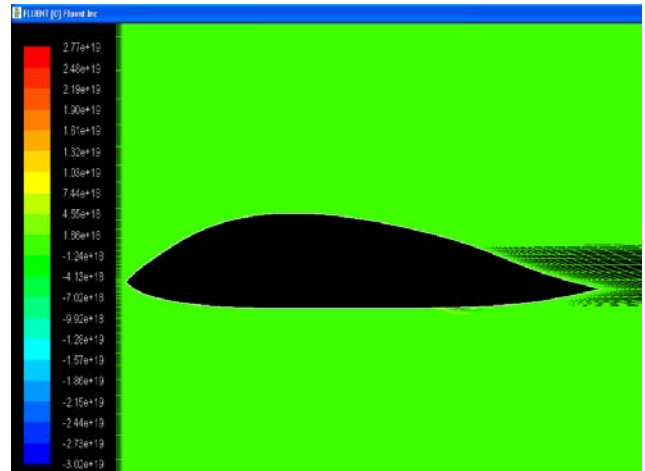


Figure 12 : No pressure gradient which indicated no cavitation occurrence at 300rpm

Turbulent flow at 600rpm shows pressure difference in Figure 13. Lowest pressure is observed below the Propeller Blade section. This indicates that possibility of cavitation to occur is high.

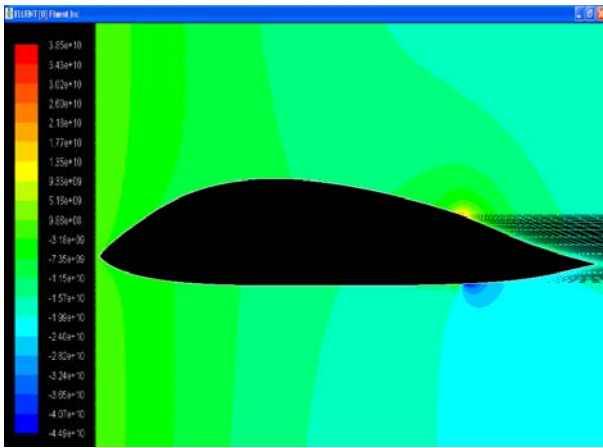


Figure 13 : Lowest pressure is observed below 0.2R Propeller Blade section

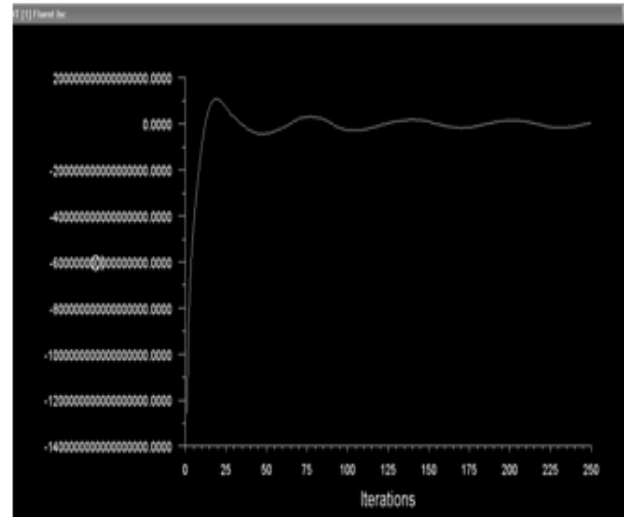


Figure 15 : Monitoring the solution convergence through lift convergence history

e) Result of 0.6R Propeller Blade Section

For 0.6R Propeller Blade section, the CFD results, for instance, three residuals of CFD calculation, lift and drag force, velocity vector plot, and contour plot were visualised and analysed (Figure 11).

f) Iteration of 0.6R

Figure 14 shows 250 iteration results, whereby the continuity, x-velocity and y-velocity were calculated for flow equation. It can be seen that the residuals were moving downwards equivalent to the convergence criteria, which is 0.001. This shows that the solution was converging.

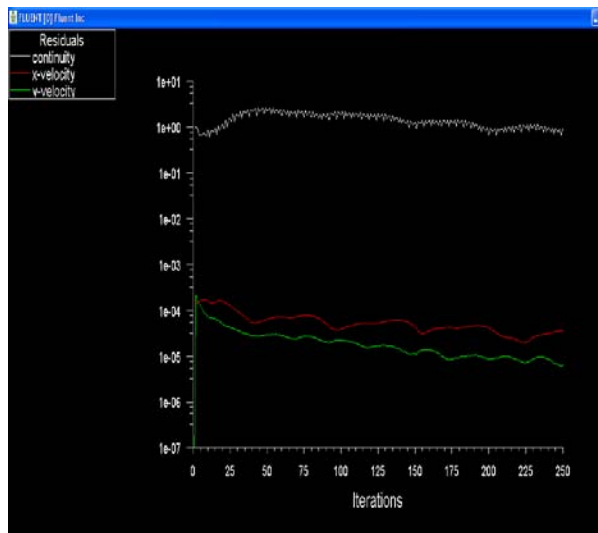


Figure 14 : Iteration results for continuity, x-velocity and y-velocity

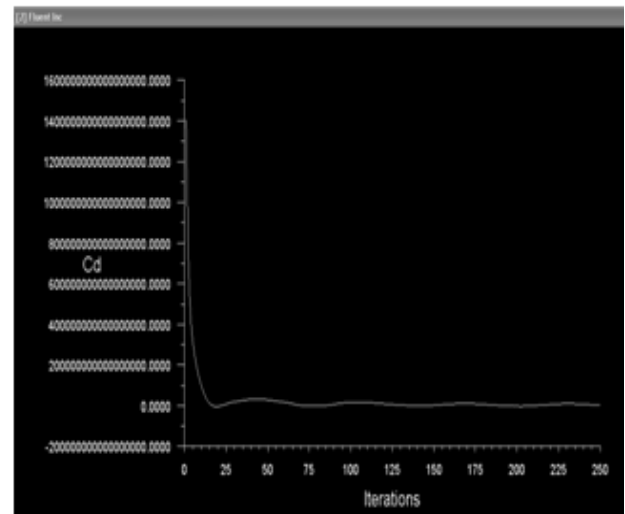


Figure 16 : Monitoring solution convergence through drag convergence history

On the other hand, laminar flow simulation of 0.6R at 300rpm resulted in lower pressure observable at the trailing edge as shown in Figure 15.

Lift and drag vector force as shown in Figure 15 and 16 shows a convergence solution through the lift and drag convergence history.

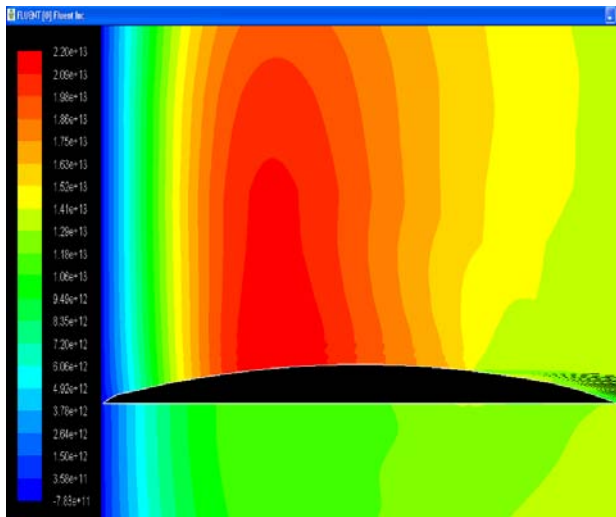


Figure 15 : Lower pressure at trailing edge of 0.6R

Besides, turbulent flow for 0.6R of 300rpm is seen that cavitation occurred at the upper surface of the Propeller Blade section as shown in Figure 17.

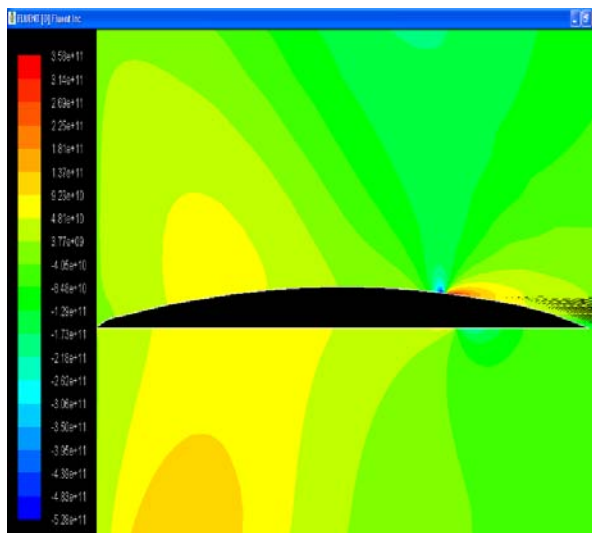


Figure 17 : Low pressure is spotted at the upper surface of the Propeller Blade section

For the 600rpm, huge area of lower pressure is observed at the upper surface of the 0.6R Propeller Blade section of the turbulent flow as shown in Figure 18.

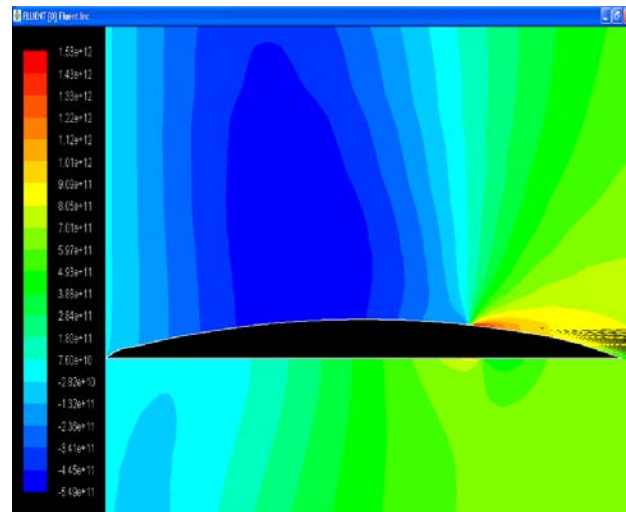


Figure 18 : Huge area of lower pressure is observed at the upper surface

Based on the above contours, cavitations can happen if the Propeller Blade radius section increases, especially for 0.6R compared to 0.2R. This is because the bigger the radius, the more pressure would be concentrated at that location. Besides this, in the turbulent flow, cavitation is more likely to be induced compared to laminar flow due to its fluid characteristics. Also, the higher the rpm, the lower the absolute pressure.

g) Graph of absolute pressure versus curve length

The graph in Figure 19 shows that, the pressure decreases when it passes by the Propeller Blade equivalent to the diagrams shown above and as it leaves the Propeller Blade, the pressure slowly increases back to its actual pressure.

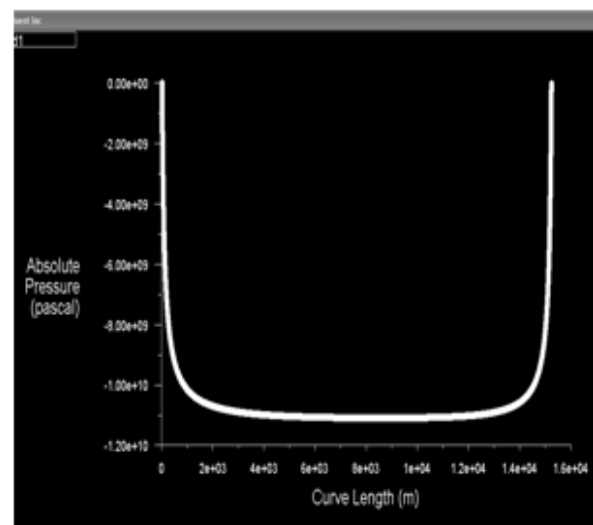


Figure 19 : Absolute pressure characteristic moving across a Propeller Blade

Figure 20 shows cavitation number, σ versus advance coefficient, based on the graph. When the propeller rotates at 300rpm, the operating condition falls in the region for a conventional propeller, which is suitable for most of the merchant vessels, whereas, at 600rpm, propeller operating condition falls in the poor region for high - speed propeller operation. This indicates low efficiency for propeller since low advance coefficient implies high propeller power coefficient. This is probably due to inaccurate application of propeller rotational speed with engine load and gear box used.

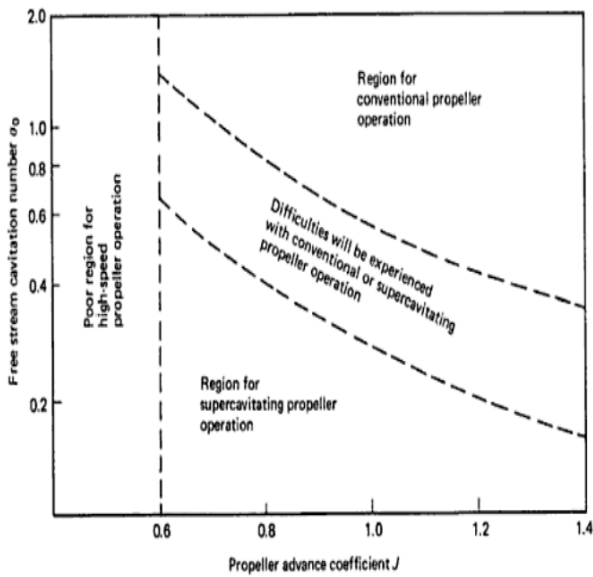


Figure 20 : Cavitation number, σ versus advance coefficient

When the propeller rotates at 300rpm, the advance coefficient and cavitation number reaches the region for conventional propeller operation. This means that, at 300rpm, the propeller rotates at a good condition suitable to the engine load and gear box required. On the other hand, when the propeller rotates at higher speed, it reaches a poor region for high - speed propeller operation which indicates damages, vibration and cavitation would occur. Based on the results of velocity and contour plots of 300rpm and 600rpm, the higher the rpm, the lower the absolute pressure, which is the condition for cavitation to occur. This is caused by high rotational rates of the propeller which creates high - pressure and low- pressure region on the blades. Besides, when the radius increases along the propeller, cavitation might happen too. Airfoil section profile at 0.2R does not have cavitation due to less pressure concentration in that region compared to 0.6R airfoil section profile. At 0.6R airfoil section profile, more works is required to be done in that region [14, 15].

IV. CONCLUSION

The paper presents the result of water flow at the blade section profile. Cavitation occurrence is

observed to be at the upper surface of 0.6R compared to 0.2R of propeller blade section due to different pressure concentrations. Besides, cavitation is predicted at low absolute pressure when the rpm is high and this correlates with theory hypothesis. Optimisation of the propeller can be achieved by increasing the blade area ratio (BAR) and compare it with the standard Kaplan BAR value that is, 0.85. The result deduced from this study can be added to existing databased for validation purposes especially for ship navigating within Malaysian water. This could provide information on environmental differential impact on propeller. It is recommended that further multiphase, experimental simulation should carried out to test rotational speed of propeller at different powers produced by the engine load.

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Ship Structural Integrity of Aluminium Stiffener Panel for Consequence Reduction

By O. O. Sulaiman, A.S.A.Kader, W.B.Wan Nick & A.H. Saharuddin

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Abstract - The aluminium stiffener panels in ship structure are paramount to ensure safety and to guarantee the structural strength and integrity of the ship. The aluminium stiffener panel is very important to ship building, especially when the ship faces collision or unstabilized structure; the aluminium stiffener panel tends to increase bending moment, vertical shear force and stresses. This study investigate the strength of the aluminium stiffener panel at the amidship bulkhead with different shapes and types in order to determine the strength of the aluminium stiffener from its features. AA 5083-H116 aluminium stiffener panel used has been approved by the recognized organization for shipbuilding. The aluminium stiffener panel has been tested using bending moment test and compressive load to obtain the highest endurance. Three types of aluminium stiffener panels, which are a flat shaped, L-shaped and T-shaped panel, are used in order to obtain the best panel ability for a better ship structural system. The aluminium stiffener panel is tested at the area where it is different to determine area where they are affected by extreme heat due to the welding results and fabrication. The result has showed that the aluminium stiffener panel in shipbuilding process effect in an area without extreme heat is more stable.

Keywords : *Ultimate strength, heat affected zone, collision damage, aluminium stiffener panel, bulkhead, amidships.*

GJRE-B Classification: *FOR Code: 091207*



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Ship Structural Integrity of Aluminium Stiffener Panel for Consequence Reduction

O. O. Sulaiman^α, A.S.A.Kader^σ, W.B.Wan Nick^ρ & A.H. Saharuddin^ω

Abstract - The aluminium stiffener panels in ship structure are paramount to ensure safety and to guarantee the structural strength and integrity of the ship. The aluminium stiffener panel is very important to ship building, especially when the ship faces collision or unstabilized structure; the aluminium stiffener panel tends to increase bending moment, vertical shear force and stresses. This study investigate the strength of the aluminium stiffener panel at the amidship bulkhead with different shapes and types in order to determine the strength of the aluminium stiffener from its features. AA 5083-H116 aluminium stiffener panel used has been approved by the recognized organization for shipbuilding. The aluminium stiffener panel has been tested using bending moment test and compressive load to obtain the highest endurance. Three types of aluminium stiffener panels, which are a flat shaped, L-shaped and T-shaped panel, are used in order to obtain the best panel ability for a better ship structural system. The aluminium stiffener panel is tested at the area where it is different to determine area where they are affected by extreme heat due to the welding results and fabrication. The result has showed that the aluminium stiffener panel in shipbuilding process effect in an area without extreme heat is more stable.

Keywords : Ultimate strength, heat affected zone, collision damage, aluminium stiffener panel, bulkhead, amidships.

I. INTRODUCTION

a) Background

The stiffener panel on ship structure is one of the support element from basic of building ship structure such as type flat bar, T bar and L bar used in shipbuilding construction, they are used commonly in the bulkhead and amidships. Study on ship strength and integrity determined from life cycle of ship and return of investment leads to ship own or spending more money on maintenance. Stiffened plates in ships revealed that other structures may be exposed to complex stress patterns due to simultaneously acting in-plane biaxial and shear stresses in design of such elements, buckling and ultimate strength are important issues researched by Brubak, L. and Hellesland J. (2008). Stiffened plates are required to resist extreme loading conditions, for example in term of axial compressive loads or lateral pressures studied by Khedmati M.R., and Ghavami K. (2009). The principal variables studied are the plate thickness, boundary conditions and the stiffener geometries beside the

geometrical imperfection, the width of the welding heat-affected zone (HAZ) and welding residual stresses are also examined.

The study involved of ship structure construction and testing of different part of aluminium stiffener panel to investigate be more strength because they can cause support load weight on the ship such as machinery, fuel, oil and other equipment. Aluminium stiffener should be more strengthen for support the ship body, Therefore, it is important to find ship structure in respect to fatigue to determine structural integrity.

b) Inherent Problem Associated with Ship Structure integrity

- The variation in the buoyant forces increased the bending moment, vertical shear force, , stresses and amidships the buoyancy forces design in such situation will tend to 'hog' the vessel, if the trough is amidships the buoyancy forces will tend to 'sag' the ship.
- The stiffness against bending tend to increased by a hollow section with space between the stiffeners which is reduced by the twin-wall section shape compared to the single-wall stiffeners such as T-shaped or L-shaped stipulated by Ye N. and Moan T. (2007).
- Fatigue becomes the governing criteria in the design of the mid-ship stiffener/web frame connections at the top and bottom has studied by Ye N. (2007).

The study asses ship structure reliability strength of aluminium stiffener panel from outside pressure and consequential damages. The study investigated the aluminium stiffener strength by shape and type of stiffener at bulkheads and amidships and determined reliable effect of aluminium stiffener strength from their behavior.

II. METHODOLOGY

The study process involves the following stages:

a) Theoretical Modeling

The theory of stress and strain is compared with the value of lab test for validation purpose to deduce and recommendation as required. Compressive stress acts to reduce the length of the material (compression member) in the axis of the applied load is modelled.

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b) Field Work at Shipyard

The plate of aluminium alloys 5083-H116 was prepared at shipyard before the construction the aluminium stiffener panel. The plate is cut and prepared to get the dimension based on the ship requirement. Aluminium stiffener is resized to deduce the parameter smaller than panel dimension suitable for the tester machine. The methods for fabricating aluminium stiffener panel are presented by MIG welding technique.

c) Laboratory Test Panel

The aluminium stiffener panel work at shipyard as followed by determination of the type and dimension. A three panel with L-shaped, T-shaped and flat shaped stiffeners fabricated from extruded aluminium profiles in alloy AA5083-H116, joined by welding, was defined.

d) Compression Test

The method of research to determined behavior of materials under crushing loads. Compressive stress and strain is calculated and plotted as a stress-strain diagram test purposed to determine ultimate strength of aluminium stiffener panel under load. The result determined when the frequency of breakage or limit of aluminium stiffener panel test. The specimen was prepared to test at universal testing machine the best environmental condition. For aluminium stiffener, good condition and room temperature to avoid the other effect on the test specimen is providing for the test.

e) Bending Test

Three-point bending test involve involved simple two-dimensional analysis of a simply supported aluminium stiffener panel loaded. The formation of the process zone and failure of the specimen are simulated in aluminium stiffener dimension steps, controlled by the displacement under the applied load. The load-displacement diagram is deduced as final result for bending test.

f) Heat Affected Zone Test

The test specimen was conducted by hardness test to find the material properties in aluminium stiffener panel and material composition in the welding process.

The Vickers hardness test is conducted to measuring and assesses the extent of the structural

weakness. The Hardness test required for welding process for construction of all type of aluminium stiffener panel. The Vickers Hardness test measurement was produced at allocated aluminium stiffener panel welding process for measurement on effected zone on panel extrusion.

g) Data Acquisition and analysis

The analysed for bending, compression test and Vickers hardness measurement has provided. The numerical analysis based on the result that was obtained from the compression test is provided. The theoretical modeling provided the theoretical and formulation of aluminium stiffener panel compressive strength. The comparison data from the compression test deduced the different of imperfection and fatigue of material strength. The reliable effect on aluminium stiffener panel from their behaviour with the characteristic of each type of stiffener panel dimension has determined. The classification society validation requirement process approval the license and ship seaworthiness is used for necessary checking of the result.

III. RESULT AND DISCUSSION

a) Stiffener Panel Dimension

Stiffener panel dimension is calculated theoretically according to suggested requirement and comparison is made. The bending test require the dimension of aluminium stiffener panel the values of thickness and area of body applied load, A. The length of specimen, L is same and width of specimen, b. The range of dimension L/b is 6.9 of each specimen.

The total overall dimension for aluminium stiffener panel is likely to be the same with the bending test. The measurement weight of specimen, W slightly different and thickness of stiffener is also different. The flat bar (fb) is 3mm, T-bar (tb) is 4mm and angle bar (lb) is 5mm. The range of measurement is L/b that is 0.9 respectively. The aluminium stiffener panel has a cross sectional area with their body plating, have the area of dimension, sectional dimension of stiffener panel and type stiffener panel difference values and arrangement. The cross sectional area is analysed in Table 4.3 with specimen is considered.

Table 4.3 : Cross-Sectional Area Type Of Aluminium Stiffener Panel

Type specimen	Cross-section (nominal values)						
	a (mm)	b (mm)	t (mm)	t _w (mm)	h _w (mm)	t _f (mm)	b _f (mm)
Flar bar (fb)	345	50	4	3	51	-	-
T-bar (tb)	345	50	4	4	47	4	50
Angle bar (lb)	345	50	4	5	46	5	50

The requirement of body plate used is similar to other but structural strength of stiffener panel is slightly different compare to research by Khedmati M.R. et al.

(2009). Table 4.4 shows the type of aluminium stiffened plate by type of stiffener panel. The used of average value of initial deflection in ship plating is investigated

and evaluated by Khedmati M. R. et al as $W_0^{\max} = 0.05\beta^2 t$. The material properties were taken from the previous study. The Young modulus and the Poisson ratio of the material are 70 GPa and 0.33, respectively.

Table 4.4 : Type Of Aluminium Stiffened plate

Type Specimen	Stiffened plate				
	I (mm ⁴)	r	β	λ	$W_0^{\max}/L$ ($\times 10^{-3}$)
Flar bar (fb)	33162.7	5.6604	0.87966	0.001023	0.449
T-bar (tb)	34607.6	5.0077	0.65974	0.001157	0.252
Angle bar (lb)	40556.7	4.8488	0.52779	0.001195	0.161

b) Ultimate Strength And Maximum Load On Aluminium Stiffener Type

i. Bending Test

Graph 4.1 shows the result of angle bar type of stiffener panel in called L shaped. The initial angle bar

specimen test has a disturbance of stresses between 0-1mm on deflection body because the material of plate has higher load better than load applied from the machine test. The result of the ultimate load of structural body is a 1083.69 kN.

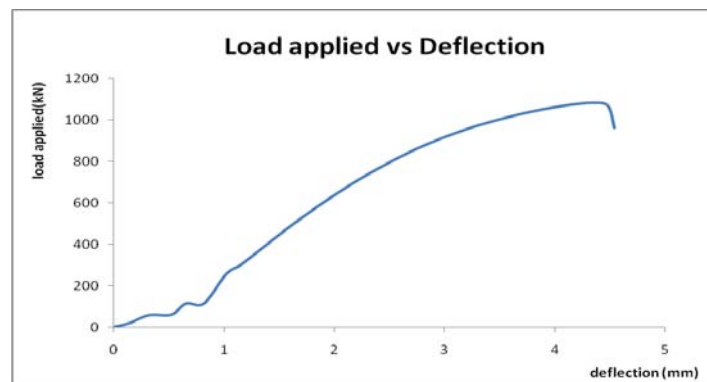


Figure 4.1 : Graph Load Applied Against Deflection Of Angle Bar

Figure 4.2 has shows the graph of flat bar (fb) type of stiffener panel, the load applied against deflection has proved the deflection of stiffener in the

initial of bending test for flat bar specimen has a disturbance area of body plate between 0-0.7mm on deflection body.

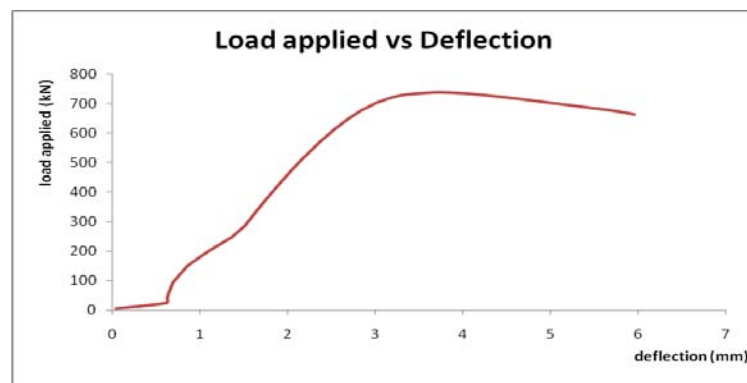


Figure 4.2 : Graph Load Applied Against Deflection Of Flat Bar

Figure 4.3 has shows the graph result of T-bar (tb) type of stiffener panel on the load applied against deflection has proved the deflection of stiffener. The T-bar result shows that the ultimate load of structural body is a 4089.146 kN. The percentage of successful of damage body required 5.12 % in area of deflection.

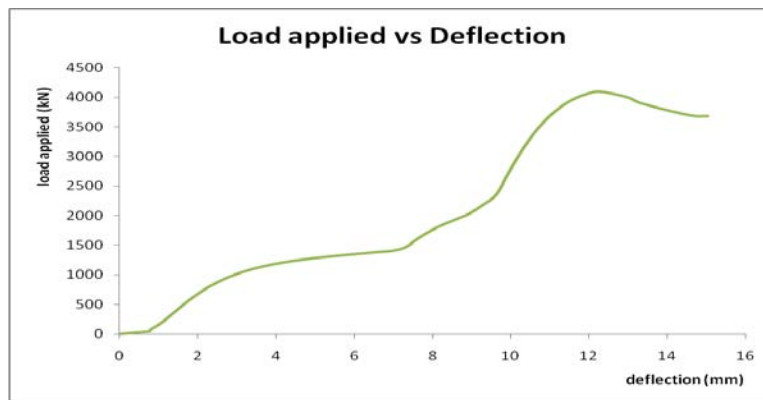


Figure 4.3 : Graph Load Applied Against Deflection Of T-Bar

The final value of test response by bending test is shown in Table 4.5. This is required to determine the ultimate capacity load with the sample of specimen. The

comparison has achieved their properties and strength values, the ultimate strength break the applied load with the stiffener panel.

Table 4.5 : The Final Value Of Test Response By Bending Test

Type specimen	Test Response				
	Max. Load,k (N/mm ²)	Deflection (mm)	Break,k (N)	Elastic Modulus,E (N/mm ²)	Yield Strength (N/mm ²)
Flat bar	0.051	5.952	6513.113	0.091	0.16
Tbar	0.185	15.030	36077.32	0.332	0.184
Angle bar	0.042	4.537	9445.379	0.076	0.114

The aluminium stiffener is the most important in the local strength because the part is stable in that area and produced the higher strength and very reliable to use in the bulkhead amidships to prevent the consequential damage from outside.

ii. Compression Test

The result of angle bar process has show that is 8.671 kN was used to pressure the aluminium stiffener

panel for testing the strength of aluminium stiffener panel. The higher load required for machine needs more applied load to damage their body until 4742.487 kN recorded. Finally the ultimate load applied with the body 5233.571 kN for the angle bar specimen has recorded. The graph of compressive load against strain is shown in figure 4.4.

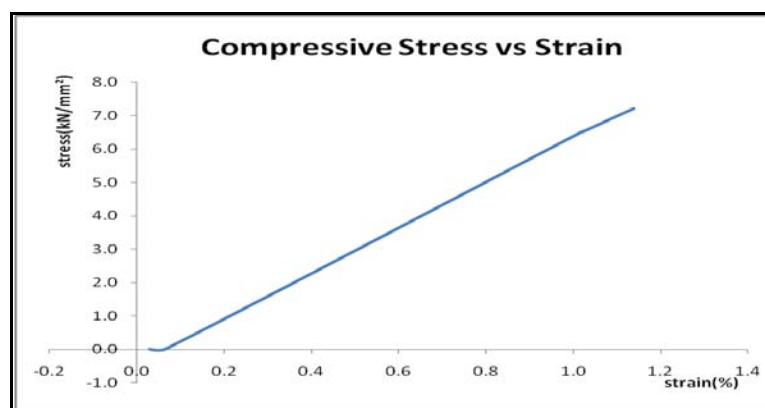


Figure 4.4 : The Graph Compression Test Of Angle Bar

The experiment of flat bar is shown, when the first value 5.017 kN was used to pressure the aluminium stiffener panel. The higher load required for machine because the strength of body needs more applied load to damage their body until 1946.741 kN recorded.

Finally the values of flat bar totally reduce down because of the fatigue and failure mode on the structure. The graph compressive load against strain of flat bar is represented in Figure 4.5.

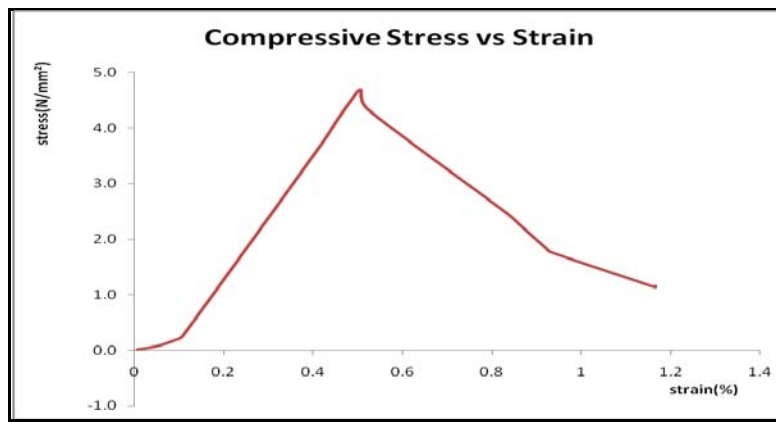


Figure 4.5 : The Graph Compression Test Of Flat Bar

The experiment has shows, that at first value of T-bar it only 2.733 kN used to pressure the aluminium stiffener panel. The higher load required for machine because the strength of body needs more applied load to damage their body until 5225.155 kN recorded. The T-bar has most structural stiffener panel in stay in the

good condition because the stability of aluminium stiffener panel is covered all of body plate. The final load of aluminium stiffener panel of T-bar becomes 5189.425 kN. The graph compressive load against strain of T-bar has shown in Figure 4.6.

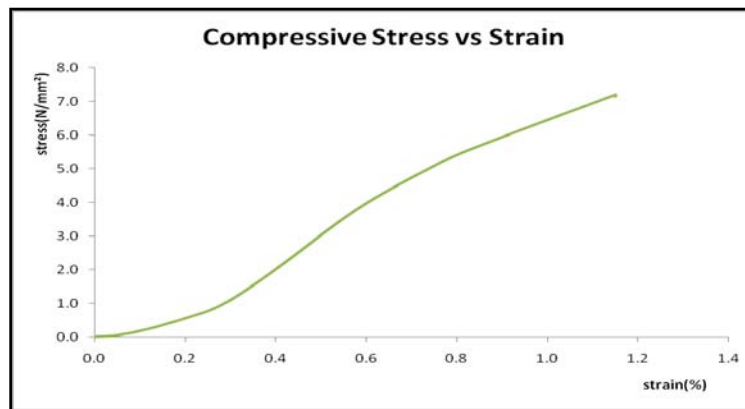


Figure 4.6 : The Graph Compression Test Of T-Bar

Table 4.9 showS the final result for compression test for requirement of test response determined a functional of each specimen in various side.

Table 4.9 : The Final Test Response of Compression Test

Type	Test Response							
	E (N/mm ²)	Yield point (N)	Max.load Fu (N/mm ²)	Break (N)	Extension Vu (mm)	Stress σ_u (kN/mm ²)	Strain ϵ_u (%)	kb/EA
(fb)	20.701	19090	0.23	4696	4.661	4.690	1.165	27.33
(tb)	38.692	51449	0.43	50890	4.583	7.157	1.151	90.71
(lb)	38.138	46681	0.424	51323	4.553	7.218	1.138	92.81

The result has expected the difference in type of aluminium stiffener panel iss defined and determine the strength of aluminium stiffener panel in difference of ultimate strength.

c) The Effect on Reliable of HAZ at Aluminium Plates and Stiffener Panel

The measurement of HAZ modeling with type of specimen based on distance from weld centre was used

to find the reliable effect of HAZ on the characteristic of each specimen type. The Figure 4.7 shows the hardness of measurement by flat bar type of specimen.

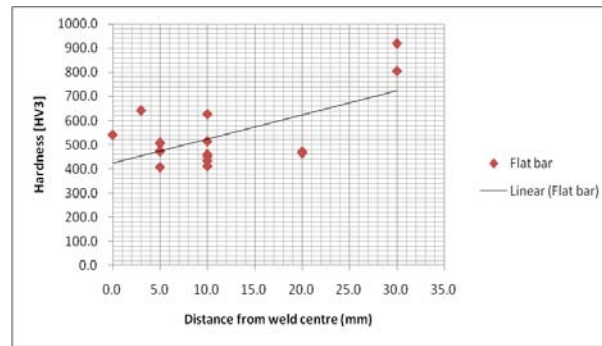


Figure 4.7: The Hardness Measurement Of Flat Bar

Figure 4.8 has shown the hardness of measurement by T-bar type of specimen. The linearity graph shows that the value of HAZ is higher than very far

distance over than nearest of distance weld centre with the influence of HAZ is very reliable because of effect of heat temperature of stiffener panel.

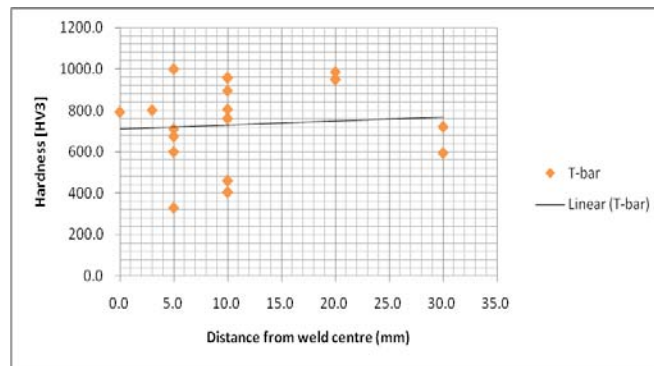


Figure 4.8: The Hardness Measurement of T-Bar

Figure 4.9 shows the hardness of measurement by angle bar type of specimen with values of HAZ.

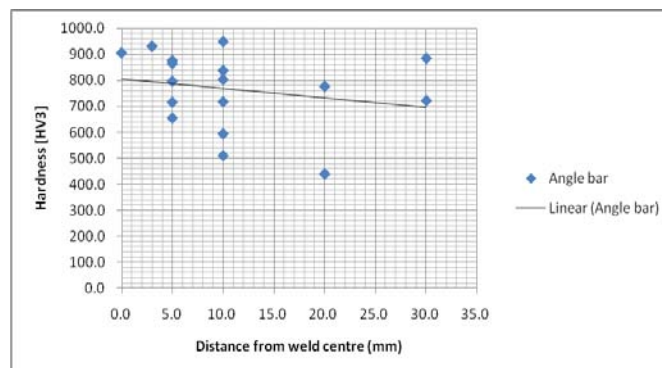


Figure 4.9: The Hardness Measurement of Angle Bar

The hardness measurement in units HV3 use the 3kg load in Hardness test. The T bar graph show the concentration value from the distance weld centre, it is observed that the highest point in the hardness test produced 997.9 in 5mm from weld centre.

d) The Energy of Collision Stiffener Panel and Ship Structure

The variable of aluminium stiffener panel has required the energy of load collision in ship structure requirement of structural damage has reconsidered by

owner ship to determine a value and loss of damage in their body. In the element of load of collision, the theoretical modeling energy of ship tonnage and energy load of collision is provided by the equation:

$$E_T \text{ (mJ)} = \frac{1}{2} \times (M_{\text{stiff}} V^2) \text{ k} \quad -1$$

$$E_{\text{load}} \text{ (mJ)} = E_T/2 (M_{\text{stiff}} V^2) \quad -2$$

Table 4.11 : Calculation Of Energy Of Load Applied, Energy Of Collision

Specimen	E (kN/m ²)	M _{stiff} (kg)	F _u (kN)	V _u	Tonnage of ship (ton)	E _T (mJ)	E _{load} (mJ)
Flat bar	2.07	0.38	19.09	0.16	1000	14.08	211.43
					2000	28.16	422.86
					3000	42.24	634.28
					4000	56.32	845.71
					5000	70.4	1057.14
T-bar	3.81	0.72	51.44		1000	14.08	1987.18
					2000	28.16	3974.36
					3000	42.24	5961.54
					4000	56.32	7948.72
					5000	70.4	9935.90
Angle bar	3.87	0.64	46.68		1000	14.08	1627.92
					2000	28.16	3255.85
					3000	42.24	4883.77
					4000	56.32	6511.69
					5000	70.4	8139.61

IV. CONCLUSION AND RECOMMENDATION

a) Conclusion

The result showed that the aluminium stiffener panel area with lower heat is more stable and has reliability for approve in ship structural system. The stiffener panel strength is determined by the ultimate strength of the load collision applied. The effect of stiffener height on average tears length for the weld configuration shows increasing tearing threshold for a decreasing stiffener height. The deformation is slightly a symmetric with the centre in the plate and proceeds along the stiffener, when the tear reaches the weld it deviates around the weld and then proceeds along the weld and plate intersection. The importance of structural dimension of specimen prevents the outside pressure from structural damage and collapse.

b) Recommendations

- i. *The following recommendation is proposed for future improvement of this study*

Firstly, the actual design study compared application to a ship structure design. Also, prediction of the possible impact on structural design, development arising from these conditions is that navies have increasingly turned to the application of classification society processes and resources to help them in establishing and applying technical criteria for naval ship design and construction including those related to the ship structure. Furthermore, the study of innovative designs for maximum the crashworthiness in an

accidental impact is necessary. Lastly, probabilistic approach to consequent evaluation of damaged stability and vessel survivability can be researched from this study.

II. ACKNOWLEDGE

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Effect of Exhaust Gas Recirculation on the Emission and Performance of Hydrogen Fueled Spark- Ignition Engine

By Zuhdi Salhab

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Abstract - Exhaust gas recirculation (EGR) is a designed widely used system to reduce the exhaust emissions, particularly nitrogen oxides (NO_x). At high temperatures, the nitrogen and oxygen in the engine combustion chamber can chemically combine to form NO_x, which, when combined with hydrocarbons and the presence of sunlight, produce an ugly haze known commonly as smog. The EGR system recirculates a fraction of exhaust gases into the intake manifold where it mixes with the fresh incoming charge. By diluting the air- fuel charge, peak combustion temperatures and pressures are reduced resulting in a reduction of NO_x concentration. In this paper, an experimental study was conducted to observe the effect of different quantities of EGR on emission and performance of four- stroke single cylinder hydrogen fueled spark- ignition engine with different excess- air ratio. Experiments were carried out for mass flow measuring of EGR with simplifying adjustment (manual designed EGR system) on the engine.

Keywords : *Hydrogen fueled engine, EGR, NO_x emissions, engine performance.*

GJRE-B Classification: *FOR Code: 090201*



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Keywords : Hydrogen fueled engine, EGR, NOx emissions, engine performance.

I. INTRODUCTION

The emission problem is one of the most interesting challenges in automotive technology and it is reached at alarming level. Because exhaust pollutants emitted to atmosphere by automobiles are the serious hygienic and environmental risk and the main source of air pollution, particularly in developing countries, the greatest interest and attention was devoted to use an effective technique to reduce the level of these pollutants. So research on improving the engine fuel economy and reducing exhaust emissions has become imperative in combustion and engine development [1].

In internal combustion engines, NOx formation is temperature dependent phenomenon and takes place when the temperature of the charge in the engine combustion chamber exceeds 2000 K [2]. So, to reduce

the NOx emission levels in the exhaust, it is necessary to keep the combustion temperature under control. Exhaust gas recirculation is one of the most effective techniques for NOx reduction.

The literature survey shows many studies of the various effects of EGR on NOx emissions on internal combustion engines (petrol and diesel engines).

II. BASIC EGR OPERATION

The NOx formation is controlled by reducing the temperature in the engine combustion chamber. This temperature is controlled by introducing a metered amount of inert gas into the engine cylinder to partially quench the flame, much like misting barbecue when it flares. It does not put out the fire, but it slows things down a bit. The result is that the fire in the combustion chamber is less intense. Recirculated exhaust gas occupies space that would otherwise contain air. With EGR, the fire is more like a smoldering pile of leaves than a blast furnace [3]. EGR system must precisely control the flow of recycled gases. Too much flow will retard engine performance and cause a hesitation on acceleration. Too little flow will increase NOx and cause engine ping. A well-designed systems will actually increase engine performance and economy [4]. Therefore, the EGR quantity must be controlled.

The EGR systems work with EGR valve which recycles exhaust gases into intake systems. Exhaust gases have already combusted, so they do not burn again when they are recycled. These gases displace some of the normal intake charge. This chemically slows and cools the combustion process by several hundred degrees, thus reducing NOx formation [4]. The decrease in NOx emissions with increasing EGR rate is the result of the following effects:

a) The thermal effect

Increase of inlet specific heats (heat capacities) due to higher specific capacity of recirculated carbon dioxide (CO₂) and water vapor (H₂O) compared with oxygen (O₂) and hydrogen (N₂) at constant pressure resulting in lower gas temperature during combustion process, and particularly in a lower flame temperature [5,6].

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b) *The dilution effect*

A decreasing in inlet oxygen concentration, whose principal consequence is the deceleration of the mixing between oxygen and fuel resulting in the extension of flame region. Also, the gas quantity that absorbs the heat release is also increasing which results in a lower flame temperature [5,6]. As a result, one consequence of the dilution effect is the reduction of local temperatures that can be also considered as a thermal effect (local thermal effect). Another consequence of the dilution effect is the reduction of the oxygen partial pressure and its effect on kinetics of the elementary NO formation reactions.

c) *The chemical effect*

The recirculated H_2O and CO_2 are dissociated during combustion, modifying the combustion process and the NO_x formation. In particular, the endothermic dissociation of H_2O results in a decrease of the flame temperature [5,6].

d) *An increase of the ignition delay*

With EGR rate is generally observed [7], so that the premixed part of combustion is higher, without EGR, it may increase NO_x emissions [8], but in the presence of EGR, the rate of heat release premixed peak is lower, so that it would reduce NO_x emissions.

e) All the combustion process is delayed with diluted air. Consequently, the whole combustion process is shifted further into the expansion stroke, which leads to lower combustion temperature [6].

It is also necessary to mention that the amount of recirculated gases in the combustion chamber depends on the following operating conditions [9]:

1. High EGR flow is necessary during cruising and mid-range acceleration, when combustion temperatures are very high.
2. Low EGR flow is needed during low speed and light load conditions.
3. No EGR flow should occur when it could adversely affect the engine operating efficiency or vehicle driveability (engine warm up, ideal open throttle, etc.). So the main aim of this paper is to investigate and observe some effects of EGR rates on NO_x emissions and engine performance (indicated mean effective pressure, maximum pressure of cylinder charge, and specific fuel consumption).

III. EXPERIMENTAL APPARATUS

All experiments have been performed and conducted on a computerized direct injection, single cylinder four- stroke hydrogen fueled spark- ignition engine (it is also modified to run on gasoline) at the laboratory of Mechanical Engineering Department at Palestine Polytechnic University. All experiments have been realized with various EGR rates at 1500 RPM/100 kPa/15° BTDC.

A fraction of the exhaust gases is to be recirculated back to the engine combustion chamber along with intake air. The quantity of EGR is to be measured and controlled. Because the possibilities available in the laboratory and political conditions did not allow programming the EGR system and engine control unit, a by-pass for the exhaust gases was provided along with the handle (manually) EGR valve to control the quantity of EGR mass flow.

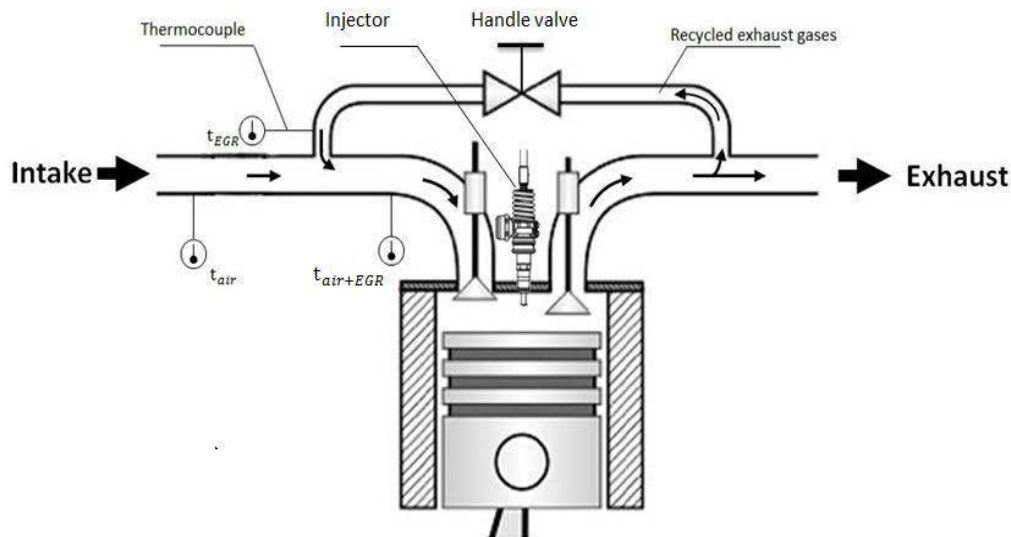


Fig. 1 : A schematic diagram of the proposed EGR system

The engine is coupled with three thermocouples to measure the temperatures of the intake air, EGR, and mixture of air and EGR. A schematic diagram of the components of the EGR proposed system is illustrated in figure 1.

Specifications of the engine are as given in table 1.

Table 1 : Specifications of the engine

Item	Unit	Value
Type of injection	-	Direct
Type of engine	-	OKC-OCTANE
No. of cylinders	-	1
Bore	mm	82.52
Stroke	mm	114.3
Connecting rod length	mm	254.5
Compression ratio	-	10
Engine speed	RPM	1500
Ignition timing	°	-15
Intake open	°	715
Intake closed	°	225
Exhaust open	°	480
Exhaust closed	°	35

The quantity of recycled exhaust gases was calculated by the use of the measured temperatures due to the energy balance equation (at constant pressure) expressed as [10]:

$$C_{P/a} \cdot \dot{m}_a \cdot t_a + C_{P/EGR} \cdot \dot{m}_{EGR} \cdot t_{EGR} = C_{P/m} \cdot \dot{m}_m \cdot t_m$$

Where:

- index m is equal to: $m = a + \text{EGR}$,
- $C_{p/a}$: the specific heat of air at constant pressure,
- $C_{p/EGR}$: the specific heat of recycled exhaust gases at constant pressure,
- $C_{p/m}$: the specific heat of the mixture of air and recycled exhaust gases at constant pressure,
- t_a : the temperature of fresh air,
- t_m : the temperature of mixture,
- t_{EGR} : the temperature of recycled exhaust gases,
- $\dot{m}_a$: air mass flow,
- $\dot{m}_{EGR}$: recycled exhaust gases mass flow, and
- $\dot{m}_m$: mixture mass flow.

The values of specific heats were calculated and then the percentage of recycled exhaust gases was determined from the following equation [10]:

$$\%EGR = \frac{\dot{m}_{EGR}}{\dot{m}_{(m_a + m_{EG})}} * 100$$

During measurements the speed of engine was kept constant (1500 RPM) and ignition timing as well (15° BTDC before top dead center).

The following parameters were measured:

- Temperatures of EGR, air, and mixture with temperature thermocouples.
- Fuel flow and air flow by digital indicators.
- NOx and excess-air ratio by Sun Diagnostic Gas Analyzer.

The indicated mean effective pressure and cylinder maximum pressure were observed during measurements with different rates of EGR and different values of excess-air ratio. The performance parameters were compared with different EGR and without EGR for same engine operating conditions. The quantity of exhaust gases is recirculated into the engine combustion chamber with air and is achieved with manually controlled EGR valve.

IV. RESULTS AND DISCUSSION

Substantial reduction in NOx concentrations are achieved with 5-15% EGR. 15% EGR was the maximum percentage achieved. The effect of EGR on NOx emissions and engine performance, is similar to addition of excess-air. Both EGR and excess air dilute the unburned mixture. Figure 2 shows the effect of increasing EGR on NOx emissions with excess air. The variation of NOx concentration is a result as the exhaust gases absorb some energy and hence lowers the peak combustion temperature.

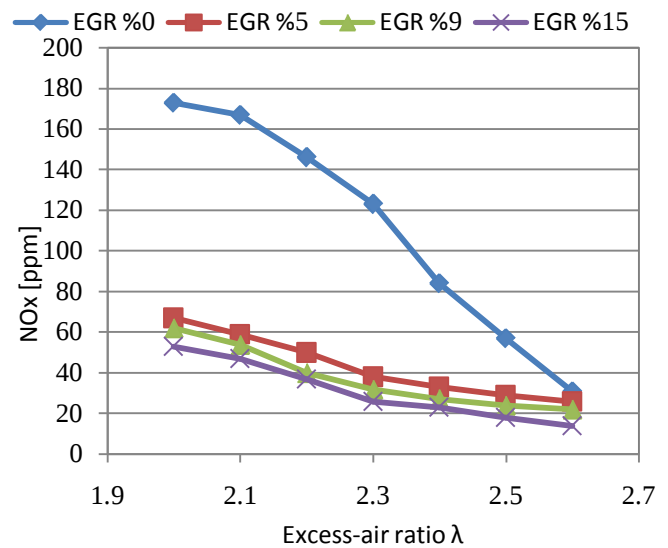


Fig. 2 : NOx vs. excess-air ratio λ with different EGR rates

At low load conditions, very low NOx can be obtained with higher EGR rates and excess air at constant pressure, because the combustion process is delayed due to higher dilution. This is accompanied with an increase of specific fuel combustion (about 8%). And this may be due to the oxygen deficiency which leads to incomplete combustion. Figure 3 shows the variation of indicated specific fuel consumption with excess air and without EGR and 15% EGR.

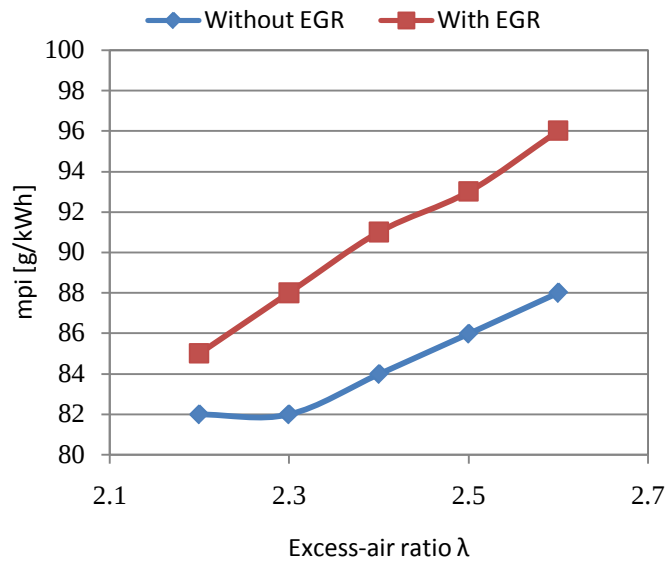


Fig. 3 : Specific fuel consumption as a function of excess-air ratio λ at 0% EGR and 15% EGR

When increasing EGR rate and with extreme lean mixture, the combustion occurs later in the cycle during expansion at a lower in-cylinder temperature, thus reducing combustion speed, the rate of heat release and the value of peak pressure.

Figures 4-5 illustrate the relation of indicated mean effective pressure and maximum pressure of cylinder charge with excess-air ratio λ at 0% EGR and 15% EGR.

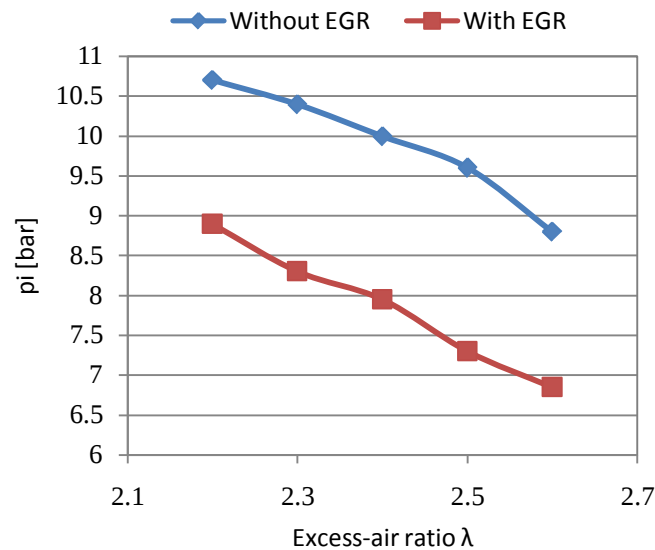


Fig. 4 : Indicated mean effective pressure vs. excess air ratio λ at 0% EGR and 15% EGR

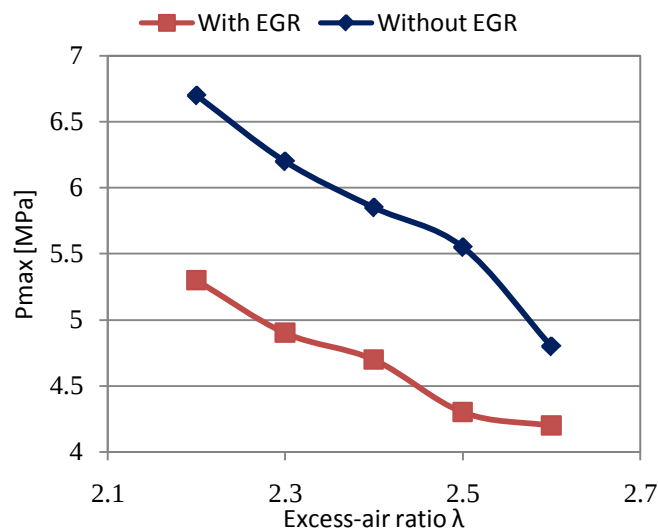


Fig. 5: Maximum pressure vs. excess-air ratio λ at 0% EGR and 15% EGR

V. CONCLUSION

It can be concluded from the measured results that employing EGR is an efficient technique in internal combustion engines (petrol, diesel, and gas engines) for NO_x reduction as it was seen from figure 2. Further it was also indicated that the engine performance of the engine are slightly independent on EGR. Peak cylinder pressure and indicated mean effective pressure are reduced and ignition delay period was prolonged with 15% EGR.

Further experimental investigations must be done taken into consideration using other engine operating conditions.

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Automotive Door Design & Structural Optimization of Front Door for Commercial Vehicle with ULSAB Concept for Cost and Weight Reduction

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Abstract - This research papers describes the drawbacks of existing automotive door structure and suggest design changes to overcome the present drawbacks. This research paper details out the analysis of the existing structure and identifies the drawbacks and explains the process of door system design. Changes required can be found out with correct method as explained in this paper. Validation of the design parameters is of vital importance so the way by which validation of newly designed or modified parts can be done is briefly explained in this paper. Designer from an automobile engineer faces so many different problems during their work. Some of the major problems in automobile door are taken as problem for this research paper and those problems like high weight, high cost, excessive reinforcements, and water leakage. At first theoretically study of the existing system is done. After that deciding the key areas of modification is the flow of this paper. After finding the modification areas we tried some parameters for calculation. On the basis of calculations the design of new parts are finalized.

Keywords : *ULSAB Concept, Problems in TWB technology, new inner panel for hardpad, water leakage issue.*

GJRE-B Classification: *FOR Code: 090299*



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Keywords : ULSAB Concept, Problems in TWB technology, new inner panel for hardpad, water leakage issue.

I. INTRODUCTION

Recently, there have been two approaches in reducing automobile weight. One is by using material lighter than steel and the other is by redesigning the steel structure. Although the former seems very effective, it is very expensive so that it may only be used for an expensive automobile. Therefore, the automobile industry is trying to use steel,

which is not costly and recyclable. Lightweight steel can be achieved by improving the performance of the structure or adopting new manufacturing techniques. One of the efforts is the ULSAB (ultra light steel autobody) concept. ULSAB suggests three main weight reduction techniques such as hydro-forming and the tailor welded blank (TWB). In this research, the TWB technique is utilized for lightweight door design, and a design process is proposed for optimizing the automobile TWB door. In the automotive door assembly, door inner panel is divided into different thickness without reinforcement components and different thickness sheets, plates are assembled by laser welding. The use of tailored steel solutions eliminates the need for additional reinforcements and overlapping joints in the body, saving material and further reducing total weight. In this way, tailored blanks are a significant enabler to meet specified CO2 targets. Reducing the weight of a car, reduces CO2 emissions. Objective of this paper is Low cost door design for developing countries India, Srilanka, South Africa without compromising any performance and regulatory requirements for example removing molded trim with hard pad, cost saving approximately 1400 Rs/set. Reducing the weight of door assembly by reducing number of components and by using advance technologies like tailor welded blank and high strength material. Existing design has a water leakage problem from the assembly of inner door panel and seal because of different thickness of inner panel. The parts which are newly designed or modified are designed on the basis of space constrained. The main constrained is that avoids as much as modification in the machined parts.

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II. EXSISTING INNER DOOR PANEL DESIGN

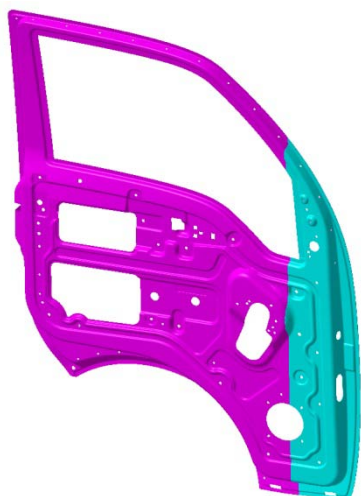


Fig 1 : Front Door Inner Panel, Weight: 6.3 kg

Inner door panel is a component which is use for strengthening the door assembly and it is one of the most important components on witch all accessories are mount like hinges, glass guide channel. Front door sill, window winding regulator, hard pad, molded trim, latch etc. Front door inner panel is use for sealing purpose when the primary sill is mounted on this. The weight of Door inner panel is near about 7to8kg depends upon its material and its thickness. The possible method is the integration method. In the integration method, the part is stamped out of a single blank. This reduces the number of tools needed; the assembly cost, and eliminates any fit ability problem. However, the design engineer is forced to work with same grade, thickness, and corrosion resistance throughout the entire part. Since the most demanding of all these conditions must be satisfied for the entire blank, this would increase the cost and weight of the part



Fig 2 : Assembly of molded trim and with inner panel

a) *Material used for exsisting inner door panel*
0.7mm thick, EDD 513, 1.6mm thick, St40e

Table 1 : For material properties

	Grade St 35E	Grade St 40E
% Carbon	30 PPM max	30 PPM max
% Mangnese	0.35-0.45	0.35-0.45
%Sulphur	0.010 max	0.010 max
%Phosphorus	0.06 max	0.06 max
% Silicon	0.015 max	0.015 max
% Alumini	0.02 -0.04	0.02 -0.04
% Titanium	0.015-0.025	0.015-0.025
% Niobium	0.035-0.045	0.035-0.045
% Boron	5-10 PPM	5-10 PPM

	Grade St 35E	Grade St 40E
Yield Strength	180-220 MPa	230-270 MPa
Tensile Strength	345 -386 MPa	390 MPa min
% Elongation	35 min	34% min
R	1.6 -1.9	1.5 -1.9
N	0.21 -0.24	0.20 -0.24

III. DESIGN OF NEW DOOR INNER PANEL FOR REDUCING COST AND WEIGHT OF FRONT DOOR ASSY

In this paper we are going to reduce weight of a front door assembly by using tailor welded blank concept for front door inner panel and using less thickness high strength material and reducing cost by replacing molded trim with hard pad in front door assembly and saving 1400 Rs/set.

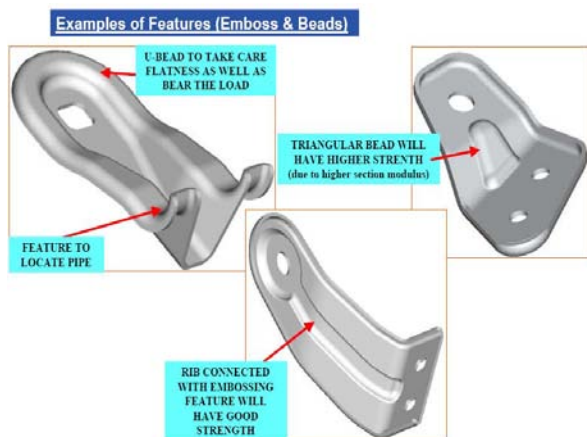
a) *Methods of preparing inner door panel*

1. In current automotive stamping technology, there are two basic paths that can be followed to arrive at the final inner door panel. The first method is part disintegration or part separation. In this technique, each different section of the blank is stamped separately and then spot welded together in the shape of the final part. This method has numerous advantages such as the ability to select the specific properties, i.e. the strength, thickness, corrosion resistance, etc. of each area of the blank. This method also gives a higher yield ratio of material used.
2. The other possible method is the integration method. In the integration method, the part is stamped out of a single blank. This reduces the

number of tools needed; the assembly cost, and eliminates any fit ability problem. However, the design engineer is forced to work with same grade, thickness, and corrosion resistance throughout the entire part. Since the most demanding of all these conditions must be satisfied for the entire blank, this would increase the cost and weight of the part significantly.

3. A solution to the problems listed above is the utilization of tailor-welded blanks. A tailor-welded blank is a blank that is comprised of two separate pieces of sheet metal that has been welded together previous to stamping. Tailor welded blanks allow the welding of the different grades, different thickness or different corrosion coatings together in order give the properties needed in different areas, without increasing the number of tools needed to form the part and eliminating the fit ability concerns. They also allow a high degree of flexibility in designing parts and large blanks can be formed from much smaller sheets .The use of tailor-welded blanks would reduce the weight of the car. Having the ability to selectively place different thickness of material would result in weight reductions. An example of this used in production is the door inner panel. The only strength requirement on a door inner is in the region where the hinges attach to the panel.

b) Design guidelines for designing door inner panel



Beads and ribs increases the cross sectional area of component and load taking capacity increases. By adding beads we are able to reduce spring back effect of component.

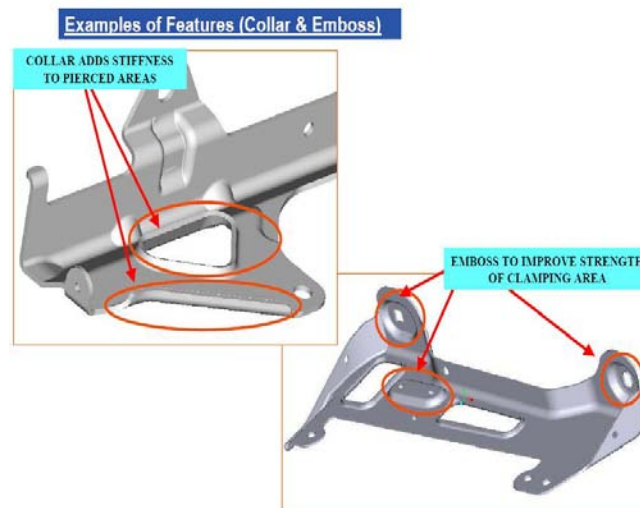


Fig 3 : Significance of ribs and beads

c) Material used for new door inner panel

0.7mm thick, EDD 513, 1.2mm thick, DP590

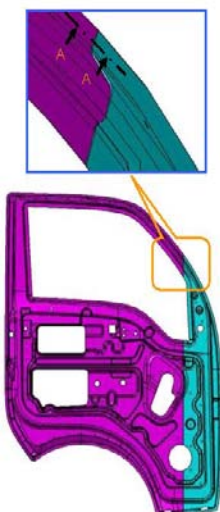
Table 2 : For material properties

Element	DP 590
% Carbon	0.08-0.12
% Manganese	1.1-1.6
%Sulphur	0.004 max
% P	0.02 max
Yield Strength	350min MPa
Tensile Strength	590min MPa
% Elongation	24 min

d) Design of new door inner panel for solving water leakage issue

Tailor Welded Blanks are made from individual steel sheets of different thickness, strength and coating which are joined together by laser welding. When we design inner door panel with tailor welded blank in witch some portion of a panel having different thickness and other is different. In our case some portion of door inner panel is 0.7mm thick shown below with pink color and another is 1.2mm thick shown below with sky color. There is a 0.5mm gap between these two thicknesses and this is the reason that water is leakage between door inner panel and secondary sill in shower test. Below figures gives the idea of existing and new coditions.

Existing front door inner panel design
- Thickness offset is on inside



Front door inner panel design - Proposed
- Thickness offset is on the outside towards Outer

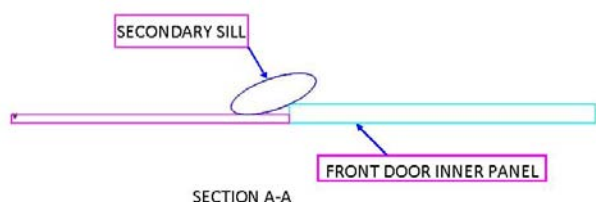
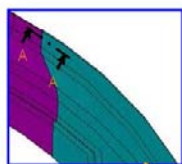


Fig 4 : Existing inner door panel condition with inside thickness

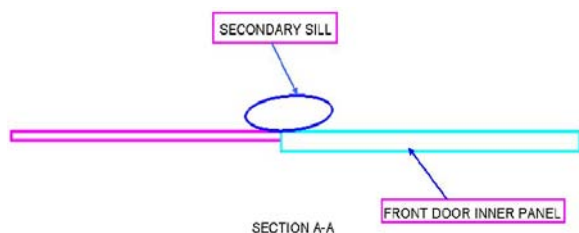


Fig 5 : New inner door panel condition with outside thickness

New front door inner panel for hardpad & no water leakage issue, weight-5.9kg

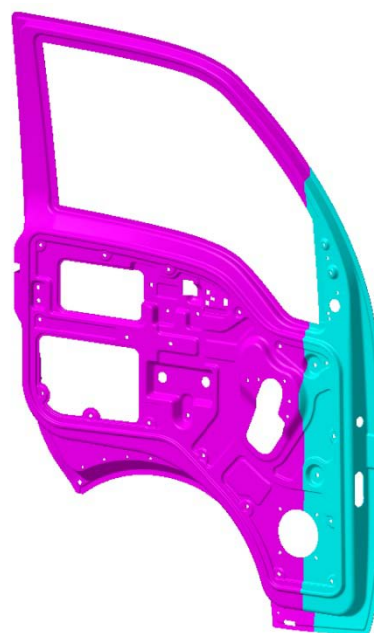


Fig 6 : New front door inner panel

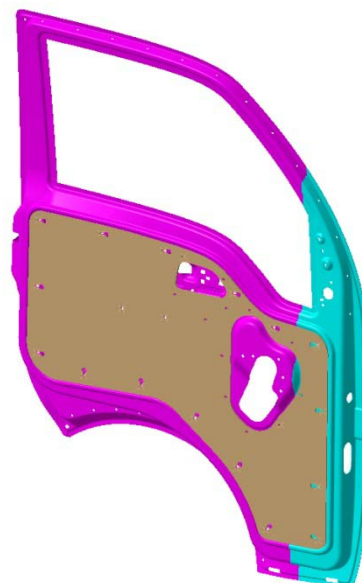


Fig 7 : Assembly of new door inner panel & hard pad

IV. FORMING ANALYSIS

The technique of sheet metal forming analysis requires non-contact optical 3D deformation measuring system. The system analyzes, calculates and documents deformations of sheet metal parts, for example. It provides the 3D coordinates of the component's surface as well as the distribution of major and minor strain on the surface and the material thickness reduction. In the Forming Limit Diagram, the measured deformations are compared to the material characteristics. The system supports optimization

processes in sheet metal forming by means of; Fast detection of critical deformation areas, Solving complex forming problems. The optical forming analysis with forming analysis system provides for precise and fast measurement of small and large components using a high scanning density. Forming analysis system operates independently of the material. It can analyze components made from flat blanks, tubes or other components manufactured by an internal high pressure forming process (Hydro forming). The Forming limit curve is used in sheet metal forming for predicting forming behavior of sheet metal. The diagram attempts to provide a graphical description of material failure tests, In order to determine whether a given region has failed, a mechanical test is performed. The mechanical test is performed by placing a circular mark on the work piece prior to deformation, and then measuring the post-deformation ellipse that is generated from the action on this circle.

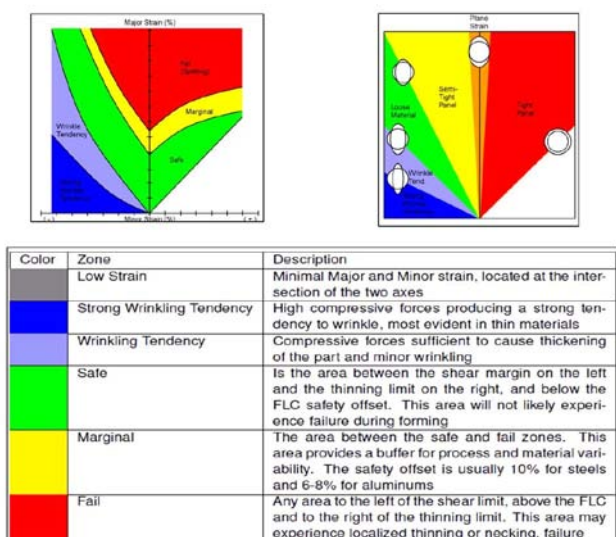


Fig 8 : Color bands in forming limit dig

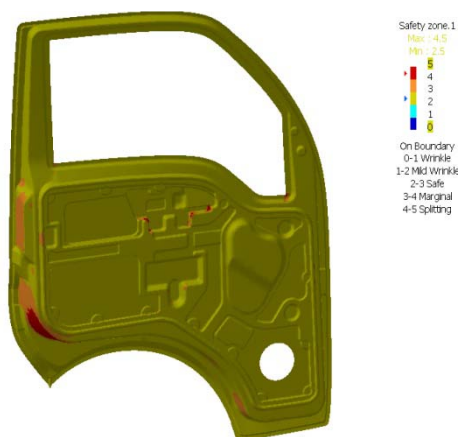


Fig 9 : Inner panel in safety zone

V. CAE ANALYSIS

To evaluate the stiffness and sag performance of the front door for both existing and hard pad. Different stiffness's considered for front door assemblies are. The objective of this analysis is to predict the vertical sag behavior of the front door assembly of CUB (Goods Carrier). As per the procedure, there should not be a permanent set exceeding 1 mm and maximum latch point deflection (elastic) should not be more than 10 mm. At the latch point under two conditions

Table 3 : Boundary and Load conditions

Location No	Load Cases	Force
2	Torsional rigidity top	An inboard force 1000N is applied to the door inner corner(top)
3	Torsional rigidity bottom	An inboard force 1000N is applied to the door inner corner(bottom)
4	Beltline inner	A horizontal force of 600N is applied to the beltline reinforcement at the midpoint of the window opening (inner)
5	Beltline outer	A horizontal force of 600N is applied to the beltline reinforcement at the midpoint of the window opening (outer)

a) Results

Stiffness Analysis :

- 1) Predicted vertical stiffness of door with hard pad interiors is lower than existing front door design
- 2) Predicted beltline inner stiffness of door with hard pad interiors is lower than existing front door design
- 3) Predicted beltline outer stiffness of door with hard pad interiors (CAE Proposed design) is equivalent to existing front door design

Door Sag Analysis :

Predicted maximum elastic deflection and permanent set in door under worst door sag load case are as follows.

- 1) Existing design: Maximum elastic deflection is 7.75mm and permanent set is 0.23
- 2) Hard pad design: Maximum elastic deflection is 9.27mm and permanent set is 0.34

VI. CONCLUSION

In this paper we design new front door assembly components with tailor welded blank technology for reducing weight and cost of door assembly. Tailor-welded blanks allow combining different strengths of steel in one part without adding complications at the joints. Weight of a door assembly is

reducing by 0.4 kg, by reducing weight of a door inner panel by using less thickness high strength material, reduce cost by replacing molded trim with hard pad. We are successfully solved water leakage problem by modeling front door inner panel correctly.

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Autonomous UAV (Unmanned Aerial Vehicle) For Navigation & Surveillance Purposes

By Chetan Khemraj, Jitendra Kumar, Ashish Srivastava & Gaurav Srivastava

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Abstract - The use of autonomous vehicles, for a wide variety of applications, has been increasing during the latest years. Land-based vehicles can be used for many purposes, but are not as versatile as could be desired, because they are dependent on the terrain. Aerial vehicles, such as aero planes and helicopters, do not depend on the terrain in the area of operation, as the land based vehicle. An autonomous helicopter has an advantage in maneuverability compared to an autonomous aero plane, which is not able to hover (stand still in the air). This and the ability to take off and land in limited spaces are clear advantages of the autonomous helicopter. An autonomous helicopter is a versatile platform for a wide variety of applications. It can be used in situations as agricultural crop dusting, search and rescue missions, inspection of bridges or power lines, surveillance of larger areas etc. Helicopters are complex, high performance machines designed to ensure the safety of their occupants during their expected lifetimes. To accomplish their goals, helicopters require extensive maintenance during their lifetimes at set intervals, whether necessary or not. To help alleviate the need for unnecessary maintenance, condition based maintenance systems are under heavy development, with the military expressing much interest in such systems. As the name implies, condition-based maintenance systems rely on information about the condition of various mechanical components to determine when maintenance is necessary. This has the potential to greatly reduce cost and enhance safety.

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Abstract - The use of autonomous vehicles, for a wide variety of applications, has been increasing during the latest years. Land-based vehicles can be used for many purposes, but are not as versatile as could be desired, because they are dependent on the terrain. Aerial vehicles, such as aero planes and helicopters, do not depend on the terrain in the area of operation, as the land based vehicle. An autonomous helicopter has an advantage in maneuverability compared to an autonomous aero plane, which is not able to hover (stand still in the air). This and the ability to take off and land in limited spaces are clear advantages of the autonomous helicopter. An autonomous helicopter is a versatile platform for a wide variety of applications. It can be used in situations as agricultural crop dusting, search and rescue missions, inspection of bridges or power lines, surveillance of larger areas etc. Helicopters are complex, high performance machines designed to ensure the safety of their occupants during their expected lifetimes. To accomplish their goals, helicopters require extensive maintenance during their lifetimes at set intervals, whether necessary or not. To help alleviate the need for unnecessary maintenance, condition based maintenance systems are under heavy development, with the military expressing much interest in such systems. As the name implies, condition-based maintenance systems rely on information about the condition of various mechanical components to determine when maintenance is necessary. This has the potential to greatly reduce cost and enhance safety. The system developed here uses data from three sensors to monitor the condition of a radio-controlled helicopter. Data from the sensors is transmitted to a microcontroller, where it is processed before being transferred to actuators and eventually to a computer for storage and visualization. The system must fulfill several requirements imposed by the constraints of the radio-controlled helicopter, mainly small size and low power usage, while still being powerful enough to perform processing on sensor data with on-board processing. The system is able to communicate with two different types of sensors, an inertial measurement unit and global positioning satellite receiver, perform calculations of statistics, and transmit the processed data reliably to a computer, where it is displayed in a custom graphical interface.

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I. BACKGROUND AND MOTIVATION

An Unmanned Aerial Vehicle (UAV) as the name suggests is a remote-controlled or completely autonomous vehicle designed to carry out a pre-specified task in a particular way. The vehicle is either programmed or trained beforehand to accomplish such a task. Development of remotely controlled vehicles is as old as the 1950s. However, the history of Vertical Take-Off and Landing (VTOL) UAVs started in early 1960s when the US Navy studied the feasibility of such a vehicle for the first time. Some close and short range (50km and 200km respectively) vehicles were developed. Recent advances in controls, microelectronics, micro electromechanical systems (MEMS) and wireless communication have led to the development of long range UAVs. Currently long range i.e. endurance aircraft is being developed that is meant to be used for cinematography, search, surveillance and transportation.

Research is being carried out in different universities to develop a completely autonomous vehicle that is able to perform complex tasks on its own and different groups are exploring new techniques to make this concept practical. Towards this end engineers are exploring different configurations of VTOLs to exploit specific advantages associated with their particular design. For example Autonomous Helicopter' group at Carnegie Mellon University is working on vision based stability. A group at Stanford University is trying to achieve acrobatic maneuvers using apprenticeship and reinforcement learning. In simple words, reinforcement learning involves adaptive algorithms that a machine learns by observing actions taken by an intelligent teacher agent, which in most cases is human, in certain environmental situations.

II. MAIN CHALLENGES

In designing a system like a UAV one need to take care of certain issues. The basic consideration in designing an autonomous or remote control aircraft is the choice of electronics. It should have minimum but sufficient electronics to carry out complex maneuvering tasks. The weight and placement of electrical components also play an important role and should be distributed carefully about the center of gravity. The system also needs to have a robust communication link

because in case of an autonomous vehicle it would be utilized in sending important information back to a base station.

The major challenge in this report was integration of different off-the-shelf components and modifying their firmware to meet the timing and rate synchronization requirements among them. Even in the design phase i.e. system identification, which is not needed for the vehicle once the model is established, the hard thing was to keep track of input/output time periods for analysis purposes.

Another issue was to mount a rigid platform on the helicopter that can carry all the electronics and sensors. Again this platform has a weight and care was taken to mount it so that the overall weight distribution remained unchanged.

Since the helicopter was built starting only from the mechanical structure a lot of things were adjusted manually and by performing experiments, which included but are not limited to adjustment of:

- (1) servos/ swashplates linkages for collective pitch
- (2) position given to each servo for varying collective and cyclic pitch
- (3) calibration of collective and cyclic pitch using a pitch gauge
- (4) throttle given to brushless DC motor
- (5) gear ratio for enough RPM to take-off
- (6) position of Inertial Measurement Unit (IMU) etc.

This project concerns the problem of modeling an autonomous helicopter (UAV) and thereafter stabilizing the model using optimal control for the purpose of surveillance and reconnaissance.

This system can be used for target & decoy, reconnaissance & civil purposes, which are very tedious and dangerous, if performed by humans. Thus this system can be proved much more efficient and helping for human beings.

III. HARDWARE DESIGN & METHODOLOGY

The choice of hardware in any UAV is dependent upon a number of criteria, which include, but are not limited to, compatibility with other components, light weight, cost, and ease of integration in the system and the flexibility in firmware. Fortunately most of these criteria are design considerations of companies like Spark fun, a company based in Boulder Colorado, whose products have been used in this project.

Below is the list of all the hardware (mechanical and electronics) components that have been used and which is subsequently explain in detail:

- (1) Single Rotor Trex-450 Frame
- (2) Brushless DC Motor
- (3) Electronic Speed Controller (ESC)
- (4) Battery Eliminator Circuit (BEC)
- (5) Nylon Gear Servos
- (6) Arduino Duemilanove(CPU)

- (7) Inertial Measurement Unit(IMU)
- (8) Power Board
- (9) Battery

IV. METHODOLOGY

Step 1 : Designing and testing of helicopter prototype for providing mechanical stabilization.

Step 2 : Calibration of servo motors and Rotor head motor for proper swash plate orientation and proper Rotor head speed.

Step 3 : Installing CPU and IMU units for testing stabilization of the platform.

Step 4 : Programming CPU with Arduino IDE.

Step 5 : Installing GPS with IMU unit for providing Autonomous Navigation to the UAV platform.

Step 6 : Installing Camera and mount with gesture capability.

Step 7 : Interfacing the system with computer for telemetry.

Step 8 : Installing distance sensor for providing ability, to this system to avoid any object in its path.

V. CONTROL SYSTEM

Our control system is made from the CPU, IMU, Telemetry system and sensors. We use the Arduino Duemilanove 328 for the CPU. It acts as brain of the system. IMU unit is made up from accelerometer & Gyro which stabilizes our system. We use wireless camera for live video streaming and RF 434 module for the transmitting & receiving of data. We take supply from the battery of 11.1 V and 20C Li-Po(Lithium Polymer) and give to the system. Our CPU i.e. Arduino takes all the data from sensors and gives the processed data to all the motors i.e. servo and out runner brushless motors. There are four types of servo motors i.e. aileron servo, elevator servo, pitch and rudder servo which is used for cyclic, collective and tail rotor pitch control respectively.

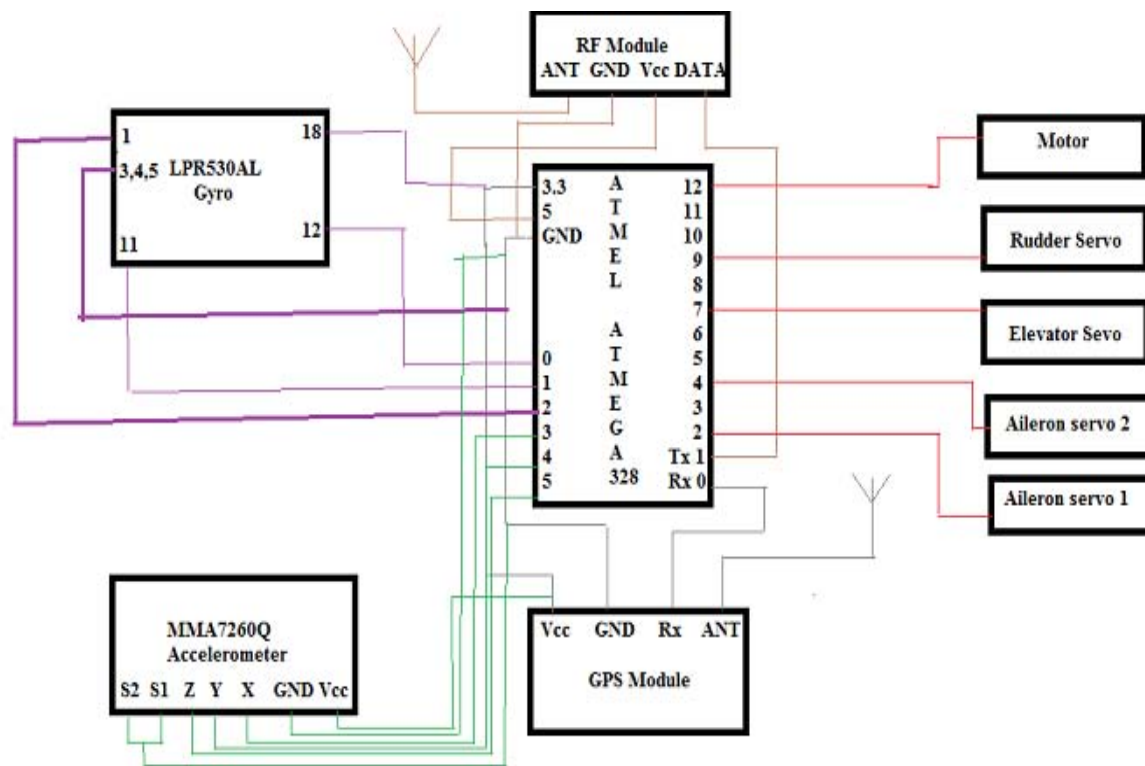


Fig 1 : Block diagram representation of UAV

VI. APPLICATIONS

a) Present Applications

An autonomous helicopter is a versatile platform for a wide variety of applications such as:

- Search and rescue missions
- Surveillance of larger areas
- Inspection of bridges, or power lines
- Traffic control
- Detection of land mines
- Agricultural crop dusting
- High altitude photography
- Mapping of topology

b) Future Applications

- With decreased cost, the area of application can be widened
- These systems can be armed with less lethal weapons for combat purposes
- These can be used by homeland security

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Investigation on Effect of Variation in Compression Ratio on Performance and Combustion Characteristics of C.I Engine Fuelled With Palm Oil Methyl Ester (POME) and its Blends by Simulation

By Sanjay Patil & Dr. M.M.Akarte

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Abstract - The paper describes the development of zero dimensional single zone thermodynamic model for compression ignition engine cycle simulation. Rate of heat release due to combustion is modeled with double wiebe function, takes care of premixed as well as diffusive phase of combustion. Adjustable parameters of wiebe function are obtained by fitting it to experimental mass fraction burned profile by least square method. Empirical correlations are established between adjustable parameters of wiebe function, relative air-fuel ratio and engine operating conditions. The simulation is used to analyze the engine performance fuelled with diesel, Palm Oil Methyl Ester (POME) and its blends. Effect of change in compression ratio on peak pressure, net heat release rate and brake thermal efficiency is analyzed and discussed. The model is validated by comparing predicted peak pressure and brake thermal efficiency with diesel and POME –diesel blends at 17.5:1 compression ratio with that of experimental results.

Keywords : Biodiesel, compression ignition engine, double wiebe function, simulation.

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I. INTRODUCTION

Energy is prominent requirement of present society. Internal combustion engines have been the prime movers for generating power for various applications for more than a century [1]. The increasing demand, depletion and price of the petroleum prompted extensive research worldwide on alternative energy sources for internal combustion engines. Use of straight vegetable oils in compression ignition engine for long term deteriorates the engine performance and is mainly because of higher viscosity [2-6]. The best way to use vegetable oils as fuel in compression ignition engines is to convert it into biodiesel [7] Biodiesels such as rape seed, soybean, sunflower and Jatropha, etc. are popular substitutes for diesel [8]. In the present energy scenario efforts are being focused on use of bio diesel in

compression ignition engine, but there are many issues related to performance and emission [8]. The optimum operating parameters can be determined using experimental techniques but experimental procedure will be time consuming and expensive [9]. Computer simulation [10] serves as a tool for a better understanding of the variables involved and also helps in optimizing the engine design for a particular application thereby reducing cost and time. The simulation approach allows examining the effects of various parameters and reduces the need for complex experimental analysis of the engine [11]. A validated simulation model could be a very useful tool to study engines running with new type of fuels.

A zero-dimensional single-zone model as compared with multi-zone models is much simpler, quicker and easier to run. [12,13] and it is capable of predicting engine performance and fuel economy accurately with a high computational efficiency [14]. Hence a zero-dimensional single-zone model is developed similar to the one developed previously by the authors [15] where Single Wiebe function is used. In this paper double Wiebe function is used to model heat release rate.

II. DESCRIPTION OF MATHEMATICAL MODELING

a) *List of symbols:*

r = compression ratio.

L = length of connecting rod (mm).

B = bore diameter (mm).

V_{disp} = displacement volume (m³).

θ = angular displacement in degrees with respect to bottom dead center (BDC).

θ_s = crank angle at the start of combustion.

γ = specific heat ratio.

P = pressure (bar).

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V = volume (m³).

m_c = number of moles of carbon in one mole of fuel.

m_h = number of moles of hydrogen in one mole of fuel.

m_o = number of moles of oxygen in one mole of fuel.

m = mass of the charge (kg).

h_c = coefficient of heat transfer due to convection (W/m².K).

A = interior surface area of cylinder (m²).

T = instantaneous gas temperature (Kelvin).

T_w = cylinder wall temperature (Kelvin).

R = universal gas constant (kJ/kmole.kelvin).

C_m = piston mean speed (m/s).

U = internal energy.

H = enthalpy.

C_p = specific heat at constant pressure (kJ/kg.kelvin).

C_v = specific heat at constant volume (kJ/kg.kelvin).

$\Delta\theta$ = combustion duration in crank angle (degrees).

Q_r = heat released per cycle (kJ).

$\frac{dQ_r}{d\theta}$ = rate of heat released during combustion (kJ/degree CA).

$\frac{dQ_h}{d\theta}$ = rate of heat transfer (kJ/degree CA).

$\frac{dw}{d\theta}$ = rate of work done.

$\frac{du}{d\theta}$ = rate of change of internal energy.

$\frac{dV}{d\theta}$ = incremental change in cylinder volume (m³/degree CA).

$\frac{dT}{d\theta}$ = rate of temperature change (Kelvin / degree CA).

Q_p = heat released during premixed phase (kJ).

Q_d = heat released during diffusive phase (kJ).

m_p = shape factor of premixed phase.

m_d = shape factor of diffusive phase.

θ_p = burning duration of premixed phase.

θ_d = combustion duration.

b) Energy balance equation

According to the first law of thermodynamics, the energy balance equation for the closed cycle is

$$m \frac{du}{d\theta} = \frac{dQ_r}{d\theta} - \frac{dw}{d\theta} \quad (1)$$

The heat term (rate of heat release) can be split into the heat released due to combustion of the fuel and the heat transfer that occurs to the cylinder walls or from the cylinder walls to gases. The equation (1) can be written as

$$m \frac{du}{d\theta} = \frac{dQ_r}{d\theta} - \frac{dQ_h}{d\theta} - \frac{dw}{d\theta} \quad (2)$$

Replacing the work transfer by $p \frac{dV}{d\theta}$ or by the

ideal gas law $PV = mRT \frac{dV}{d\theta}$, rate of heat transfer by

$h_c = A(T - T_w)$ and the internal energy can be related to specific heat through the relationship $\frac{du}{d\theta} = C_v \frac{dT}{d\theta}$

Upon simplification we get equation (2) as

$$\frac{dT}{d\theta} = \frac{1}{mC_v} \frac{dQ_r}{d\theta} - \frac{h_c A(T - T_w)}{mC_v} - \frac{RT}{C_v V} \frac{dV}{d\theta} \quad (3)$$

Solving above equation by Range-kutta fourth order algorithm, the temperature at various crank angles during combustion can be calculated.

c) Cylinder volume at any crank angle

The slider crank angle formula is used to find the cylinder volume at any crank angle [10]

$$V(\theta) = V_{disp} \left[\frac{r}{r-1} - \frac{1-\cos\theta}{2} + \frac{1}{2} \sqrt{\left(2\frac{L}{S}\right)^2 - \sin^2\theta} \right] \quad (4)$$

d) Compression and Expansion strokes

The compression stroke starts from the moment the inlet valve closes (IVC) to the moment the fuel injection starts. The expansion stroke starts from the moment combustion ends to the moment the exhaust valve opens (EVO). During these processes the temperature and pressure at each step are calculated using ideal gas equation and an isentropic process [15].

e) Combustion Process

$$\frac{dQ_r}{d\theta} = 6.908 \frac{Q_p}{\theta_p} m_p \left(\frac{\theta}{\theta_p} \right)^{m_p-1} \exp \left[-6.908 \left(\frac{\theta}{\theta_p} \right)^{m_p} \right] + 6.908 \frac{Q_d}{\theta_d} m_d \left(\frac{\theta}{\theta_d} \right)^{m_d-1} \exp \left[-6.908 \left(\frac{\theta}{\theta_d} \right)^{m_d} \right] \quad (5)$$

The parameters θ_p and θ_d represent the duration of the premixed and diffusion combustion phases. Also, Q_p and Q_d represent the integrated energy release for premixed and diffusion phases respectively. Shape factors m_p and m_d for premixed and diffuse phase of combustion have to be such that the simulated heat release profile matches closely with experimental data. These shape factors are obtained by fitting Wiebe function to experimental mass fraction burned profile using least square method. Prior knowledge of actual overall equivalence ratio is necessary because the fuel/air equivalence ratio depends on the amount of fuel injected inside the cylinder, from which the mass of fuel admitted can be calculated [18]. The amount of heat released in premixed mode is 40% of the total heat released per cycle is assumed.

f) Heat transfer

The convective heat transfer between gases and cylinder wall is considerable and hence it directly affects the engine performance. The convection heat transfer in kJ/degree crank angle is given by

$$\frac{dQ_h}{d\theta} = h_c A (T - T_w) \quad (11)$$

Where Heat transfer coefficient due to convection (h_c) is given by Hohenberg equation [19].

$$h_c = \frac{130 P^{0.8} (C_m + 1.48)^{0.8}}{V^{0.06} T^{0.4}} \quad (12)$$

g) Ignition delay

An empirical formula, developed by Hardenberg and Hase [20] is used for predicting Ignition delay in crank angle degrees.

$$ID = (0.36 + 0.22 C_m) \exp \left[E_A \left(\frac{1}{RT} - \frac{1}{17,190} \right) \left(\frac{21.2}{P - 12.4} \right)^{0.63} \right] \quad (13)$$

Where ID = ignition delay period.

E_A is apparent activation energy

h) Gas properties calculation:

A hydrocarbon fuel can be represented by $C_x H_y O_z$. The required amount of oxygen Y_{cc} for combustion per mole of fuel is given by:

$$Y_{cc} = m_c + 0.25 m_h - 0.5 m_o \quad (14)$$

The minimum amount of oxygen required (Y_{min}) for combustion per mole of fuel is $Y_{min} = Y_{cc} - 0.5 m_c$

The gaseous mixture properties like internal energy (U), enthalpy (H) specific heats at constant pressure (C_p) and constant volume (c_v) depend on the chemical composition of the reactant mixture, pressure, temperature and combustion process and can be calculated using following equations.

$$U(T) = A + (B - R) * T + C * \ln(T) \quad (15)$$

$$H(T) = A + B * T + C * \ln(T) \quad (16)$$

$$C_p(T) = B + \frac{C}{T} \quad (17)$$

$$C_v(T) = (B - R) + \frac{C}{T} \quad (18)$$

Here A, B and C are the coefficients of the polynomial equation.

i) Friction losses

Total friction loss calculated by the equation [21].

$$FP = C + 1.44 \frac{C_m * 1000}{B} + 0.4 (C_m)^2 \quad (19)$$

Where FP is total friction power loss and C is a constant, which depends on the engine type, $C = 75$ kPa for direct injection engine.

III. METHODOLOGY

a) Simulation

A thermodynamic model based on the First law of thermodynamics has been developed. The molecular formula of diesel fuel is taken as $C_{10} H_{22}$ and biodiesel is

approximated as $C_{19}H_{34}O_2$. A computer program has been developed using MATLAB software for numerical solution of the equations used in the thermodynamic model described in Section 2. This computes pressure, temperature, brake thermal efficiency, brake specific fuel consumption and net heat release rate etc, for the fuels considered for analysis. Fuels considered for analysis are namely B20, B60, and B100, 20%, 60%, and 100% POME with petroleum diesel respectively.

b) Experimental

A stationary single cylinder, 4 stroke, water cooled diesel engine developing 5.2 KW at 1500 rpm is used for investigation. The technical specifications of the engine are given in Table 1. The fuel properties are determined using standard procedure and tabulated in table 2. The cylinder pressure data is recorded by using piezoelectric transducer for 80 cycles. The average of data for 80 cycles is computed to evaluate mass fraction burned profile and combustion duration within the framework of first law of thermodynamics.

Table 1 : Specifications of Engine

Sl.No	Parameter	Specification
1	Type	Four stroke direct injection single cylinder diesel engine
2	Software used	Engine soft
3	Injector opening pressure	200 bar
4	Rated power	5.2KW @1500 rpm
5	Cylinder diameter	87.5 mm
6	Stroke	110 mm
7	Compression ratio	17.5:1
8	Injection timing	23 degree before TDC

Table 2 : Properties of Diesel and POME

Properties	Diesel(B0)	POME(B100)
Viscosity in cst(at 30°C)	4.25	4.7
Flash point(°C)	79	190
Fire point(°C)	85	210
Carbon residue (%)	0.1	0.64
Calorific value(kj/kg)	42700	36000
Specific gravity(at25°C)	0.830	0.880

IV. RESULTS AND DISCUSSION

a) Effect of compression ratio on

i. Peak pressure

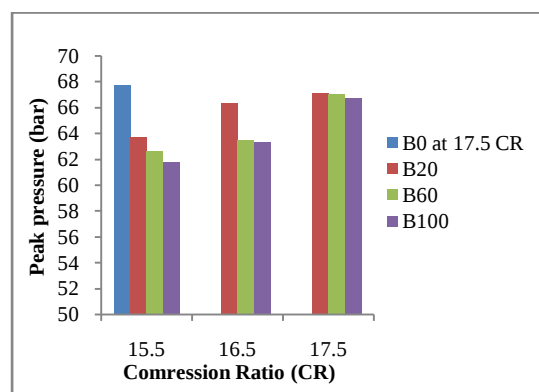


Figure 1 : Variation of Peak pressure with test fuels

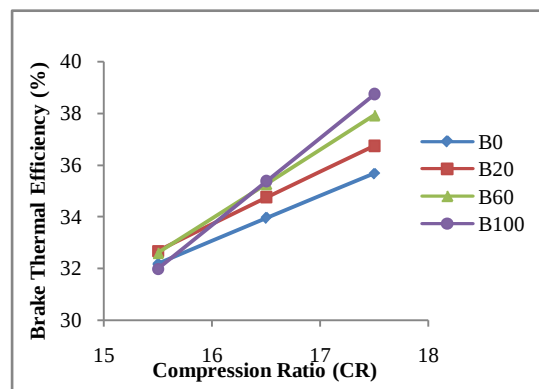


Figure 2 : Variation of Brake thermal efficiency at different Compression Ratio with test fuels at different Compression Ratio

Figure 1. shows the variation of peak pressure with various test fuels at different compression ratios. With increase in compression ratio, the peak pressure is increased for all test fuels. At every compression ratio, the peak pressure decreases with increase in proportion of biodiesel in the blend and also found that the peak pressures of all test fuels are less in comparison with that of diesel.

Increase in compression ratio enhances the pressure and temperature of air-fuel mixture in compression stroke results in increased peak pressure. Increase in proportion of biodiesel in blend burns more fuel during diffusion phase of combustion and lower calorific value of blend causes in decrease of peak pressure.

ii. Brake thermal efficiency

Figure 2. Shows the variation of brake thermal efficiency for various test fuels at different compression ratios. It is observed that brake thermal efficiency for all the test fuel is increased with increase in compression ratio. From the results it is also observed that the brake thermal efficiency at every compression ratio is increased with increase in proportion of biodiesel in the blend. This is due to the presence of oxygen molecule in

the biodiesel which enhances combustion phenomenon. The brake thermal efficiency of test fuels is lower at compression ratio of 15.5:1 and 16.5:1 and higher at compression ratio of 17.5:1 in comparison with diesel.

iii. Net Heat Release Rate

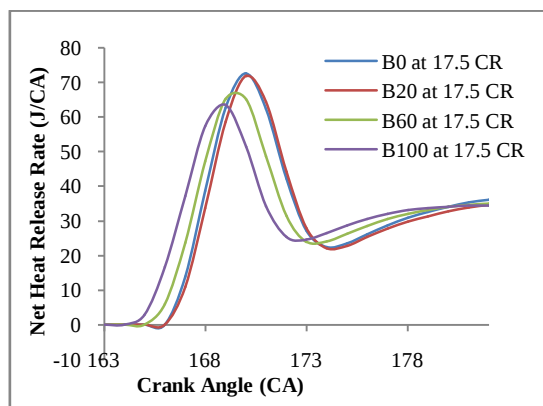


Figure 3(i) : Variation of Net heat release rate with

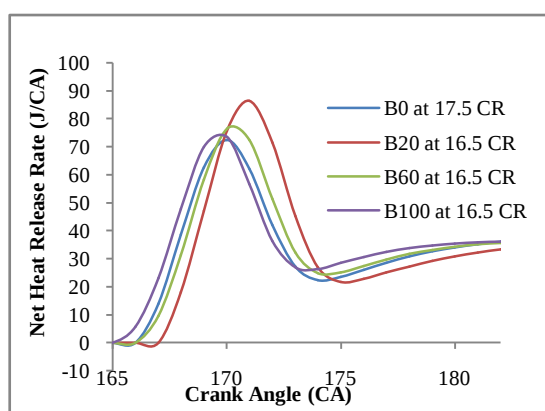


Figure 3(ii) : Variation of Net heat release rate with test fuels at 16.5 Compression Ratio

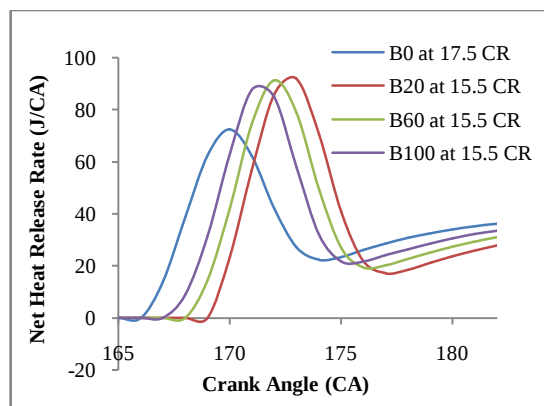


Figure 3(iii) : Variation of Net heat release rate with test fuels at 15.5 Compression Ratio

Figures 3 (i, ii & iii). Shows the variation of net heat release rate for various test fuels at different compression ratios. From the results it is observed that decrease in compression ratio increases heat release in premixed phase; however occurrence of maximum heat release moved away from TDC. This is because decrease in compression ratio increases the ignition delay period, which causes more fuel to burn late in the expansion stroke. Same trend is observed for all the test fuels. Increase in proportion of biodiesel increases the cetane number of blend, decreasing the delay period. Decrease in delay period burns less amount of fuel in premixed phase, hence decrease in net heat release rate is observed at every compression ratio.

b) Effect of load on

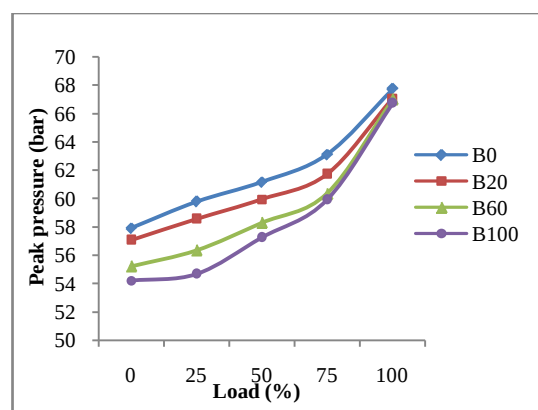


Figure 4 : Variation of Peak pressure with test fuels

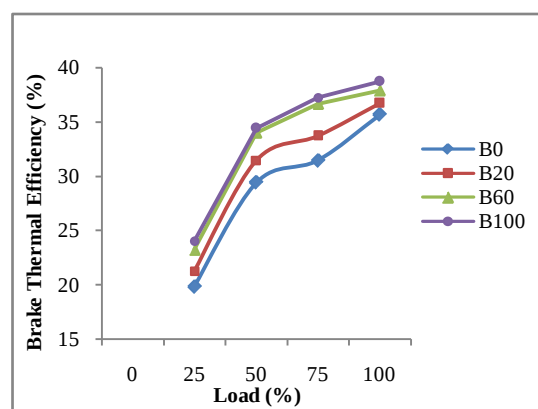


Figure 5 : Variation of Brake thermal efficiency at different load with test fuels

Figures 4 & 5. Shows the Variation of peak pressure and brake thermal efficiency with test fuels at different load. From the predicted results it is observed that increase in load increases the peak pressure and brake thermal efficiency. Same trend has been observed with all test fuels.

V. MODEL VALIDATION

With the help of developed model theoretical results are predicted for brake thermal efficiency and peak pressure for all test fuels. The same are compared with that of experimental results. The figures below highlight the features. Predicted brake thermal efficiency and peak pressure at full load when engine is fuelled with B0, B20, B60 and B100 are compared with experimental results are found in closer approximation.

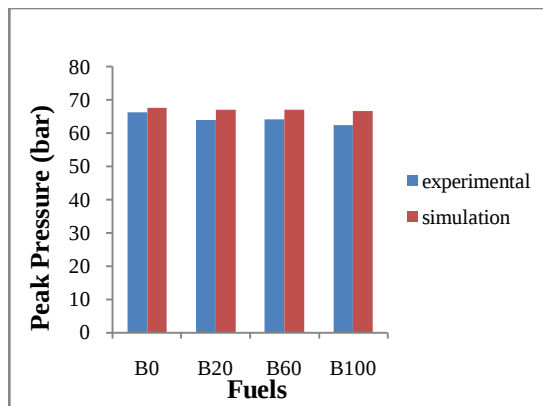


Figure 6 : Peak Pressure at full load

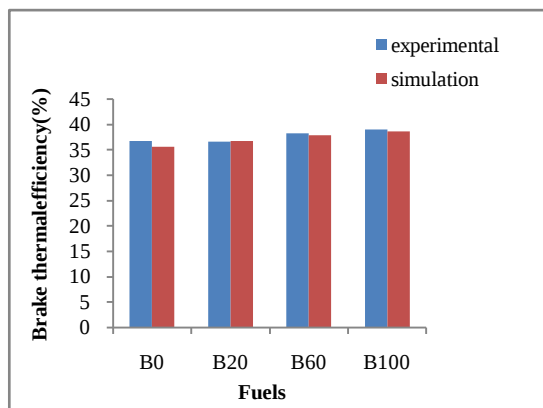


Figure 7 : Brake thermal efficiency at full load

VI. CONCLUSIONS

The thermodynamic model developed is used for analyzing the performance characteristics of the compression ignition engine. The modeling results showed that, with increase in compression ratio peak pressure and brake thermal efficiency are increased for all test fuels. At every compression ratio, increase in proportion of biodiesel in the blend decreased peak pressure and increased brake thermal efficiency. This model predicted the engine performance characteristics in closer approximation to that of experimental results. Hence, it is concluded that this model can be used for the prediction of the performance characteristics of the compression ignition engine fueled by any type of hydrocarbon fuel.

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A major linchpin in research work for the writing research paper is the keyword search, which one will employ to find both library and Internet resources.

One must be persistent and creative in using keywords. An effective keyword search requires a strategy and planning a list of possible keywords and phrases to try.

Search engines for most searches, use Boolean searching, which is somewhat different from Internet searches. The Boolean search uses "operators," words (and, or, not, and near) that enable you to expand or narrow your affords. Tips for research paper while preparing research paper are very helpful guideline of research paper.

Choice of key words is first tool of tips to write research paper. Research paper writing is an art. A few tips for deciding as strategically as possible about keyword search:



- One should start brainstorming lists of possible keywords before even begin searching. Think about the most important concepts related to research work. Ask, "What words would a source have to include to be truly valuable in research paper?" Then consider synonyms for the important words.
- It may take the discovery of only one relevant paper to let steer in the right keyword direction because in most databases, the keywords under which a research paper is abstracted are listed with the paper.
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Keywords are the key that opens a door to research work sources. Keyword searching is an art in which researcher's skills are bound to improve with experience and time.

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Acknowledgements: Please make these as concise as possible.

References

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Result	Well organized, Clear and specific, Correct units with precision, correct data, well structuring of paragraph, no grammar and spelling mistake	Complete and embarrassed text, difficult to comprehend	Irregular format with wrong facts and figures
Discussion	Well organized, meaningful specification, sound conclusion, logical and concise explanation, highly structured paragraph reference cited	Wordy, unclear conclusion, spurious	Conclusion is not cited, unorganized, difficult to comprehend
References	Complete and correct format, well organized	Beside the point, Incomplete	Wrong format and structuring

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