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CONTENTS OF THE ISSUE

- i. Copyright Notice
 - ii. Editorial Board Members
 - iii. Chief Author and Dean
 - iv. Contents of the Issue
-
- 1. Simulation of Gear Dynamics by Circuit Theory Methods. **1-6**
 - 2. An Inhomogeneous Gravitational Field and the Body without Center of Gravity. **7-10**
 - 3. Concept of the Dispersion of Electric and Magnetic Inductivities and its Physical Interpretation. **11-18**
 - 4. Passenger Safe Car. **19-22**
 - 5. Impact of the Smart Textile on the High Level Sport Performance and Patient Behavior in Medicine. **23-28**
-
- v. Fellows and Auxiliary Memberships
 - vi. Process of Submission of Research Paper
 - vii. Preferred Author Guidelines
 - viii. Index



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Simulation of Gear Dynamics by Circuit Theory Methods

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Abstract- A methodology of study of gear dynamics with the aid of the circuit theory and linear graph methods is presented. In terms of analogy of the force, electric tension is used for the composition of equivalent electrical circuit, which immediately gives the equations of motion. The application of the electrical analogy method for the automation of composition of equation of motion and their analysis are considered for the classical example of a one-stage gear transmission with flexible supports and coupling masses. This technique can be extended to analyse the dynamic characteristics of more complex dynamic systems as a planetary transmission with flexible supports.

Keywords: *dynamic gear model, equivalent electric circuit, linear graph, node equations, automation of composition of motion equations.*

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Simulation of Gear Dynamics by Circuit Theory Methods

Evgueni I. Podzharov^a, Jorge Alberto Torres Guillén^σ & Julia Patricia Ponce Navarro^ρ

Abstract- A methodology of study of gear dynamics with the aid of the circuit theory and linear graph methods is presented. In terms of analogy of the force, electric tension is used for the composition of equivalent electrical circuit, which immediately gives the equations of motion. The application of the electrical analogy method for the automation of composition of equation of motion and their analysis are considered for the classical example of a one-stage gear transmission with flexible supports and coupling masses. This technique can be extended to analyse the dynamic characteristics of more complex dynamic systems as a planetary transmission with flexible supports.

Keywords: dynamic gear model, equivalent electric circuit, linear graph, node equations, automation of composition of motion equations.

I. INTRODUCTION

The classical method of Lagrange equation (Genkin and Grinkevich, 1961) and the methods of dynamic stiffness or admittance (Airapetov et al. 1975) are used in studies of gear dynamics. These methods are cumbersome and laborious. In order to automate composition of equations of motion, the bond graph (Karnopp and Rosenberg, 1972) and some other methods are also used. However, the use of these methods presupposes presentation of a dynamic model as a system with concentrated parameters. Also, the bond graph of a relatively simple model, as, for example, a planetary gear transmission, is very cumbersome (Allen, 1979). On the other hand, electrical analogy method (Skudrzyk, 1968) and linear graph method (Mason and Zimmermann, 1960) allow us to model dynamic systems with both concentrated and distributed parameters (Podzharov, 1983, 1987, Sasa et al., 2004, Wojnarowski, 2006, Kalous, 2009).

In this paper a methodology of study of gear dynamics with the aid of the electric circuit theory methods is presented. The analogy between the force and electric tension is used to compose equivalent electric circuits for dynamic gear systems.

Table 1 : Equivalent Parameters

No.	Mechanical System	Electrical System
1	Force	Tension
2	Speed	Electric current
3	Displacement	Electric charge
4	Mass	Inductance
5	Flexibility	Capacitance
6	Absorber	Electrical resistance

NOMENCLATURE

J_i - moment of inertia of the mass m_i ,

k_i - torsional stiffness

C_{s2}, C_{s3} - support stiffnesses,

C_3 - stiffness of tooth engagement,

$T_1(t), T_2(t)$ - variable torsion moments,

μ_i - moment of inertia reduced to the mass moving on the line of action,

C_i - torsion stiffness reduced to linear stiffness on the line of action,

r_{bi} - base radius of a gear,

$F_i(t)$ - torsional moment reduced to a force applied in the line of action of gear engagement,

$S_i(t)$ - kinematic error in the gear engagement,

y_{ij} - element of the matrix of mechanical conductance,

Y - matrix of mechanical conductance,

Z - mechanical impedance,

T_{ij} - transmission in a graph between the points i and j ,

f - frequency,

$j = \sqrt{-1}$.

II. MODELLING ONE-STAGE GEAR TRANSMISSION

We shall now consider the use of electrical analogy for the automation of composition of equations of motion and their analysis in the example of one-stage gear transmission with flexible supports and coupled masses. The mechanical model of the transmission is shown in Fig.1 and in Fig. 2, presenting the equivalent electrical circuit. Here, the parameters of the torsion

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system reduced to the parameters of a linear system are determined as follows:

$$\mu_i = J_i / r_{bi}^2, C_{ki} = k_i / r_{bi}^2, F_i(t) = T_i(t) / r_{bi} \quad (1)$$

This system has 10 independent elements and 11 resonances and antiresonances (Skudrzyk, 1968), including zero and infinite frequencies. When the circuit is excited by variable tensions (forces) $F_1(t)$ and $F_2(t)$ the contours $C_1\mu_1$ and $C_3\mu_4$ act as low frequency filters filtering out high frequency components. Thus, the existence of large coupled masses linked to the gears by relatively low stiffness shafts means that the gears are dynamically isolated from external excitation in medium and high frequency ranges.

Let us consider stationary vibrations and assume that the gear is a linear dynamic system. Then, the solution of this system with periodic force or kinematic excitation can be found as a sum of harmonics. In this case the equations of motion can be composed as Kirchhoff equations of the equivalent electric circuit.

The total conductance between the points a and b will be equal to the sum of the conductances of parallel branches (Skudrzyk, 1968).

$$Y_{ab} = Y_0 + Y_1 + Y_2 + Y_3 + Y_4, \quad (2)$$

where

$$\begin{aligned} Y_0 &= j\omega / C_2, \quad Y_2 = (j\omega m_2 + C_{S2} / j\omega)^{-1}, \\ Y_1 &= \left[\left(\frac{1}{j\omega \mu_1} + \frac{j\omega}{C_1} \right)^{-1} + j\omega \mu_2 \right]^{-1}, \\ Y_3 &= (j\omega m_3 + C_{S3} / j\omega)^{-1}, \\ Y_4 &= \left[\left(\frac{1}{j\omega \mu_4} + \frac{j\omega}{C_3} \right)^{-1} + j\omega \mu_3 \right]^{-1}. \end{aligned} \quad (3)$$

The input impedance between points a and b can be found as inverse of Y_{ab}

$$Z_{ab} = 1 / Y_{ab}. \quad (4)$$

Substituting the equations (3) in the equation (2) and (4) and making Z_{ab} equal zero, we can find a frequency characteristic of Z_{ab} , which is shown in Fig. 3 for the transmission with the following parameters:

$$\begin{aligned} J_1 &= 0.012 \text{ kg m}^2, & J_2 &= 0.000686 \text{ kg m}^2, \\ J_3 &= 0.00471 \text{ kg m}^2, & J_4 &= 0.02 \text{ kg m}^2, \\ m_2 &= 1.56 \text{ kg}, & m_3 &= 3.8 \text{ kg}, \\ C_{S2} &= 0.455 \cdot 10^8 \text{ N/m}, & C_{S3} &= 0.101 \cdot 10^8 \text{ N/m}, \end{aligned}$$

$$\begin{aligned} C_{S2} &= 0.27 \cdot 10^9 \text{ N/m}, & k_1 &= 4270 \text{ N} \cdot \text{m}, \\ k_3 &= 2000 \text{ N} \cdot \text{m}, & r_{b2} &= 0.0383 \text{ m}, & r_{b3} &= 0.0634 \text{ m}. \end{aligned}$$

It was calculated neglecting the damping in the system and, according to the Foster theorem (Skudrzyk, 1968), it has a monotonous character. We can find from the curve that the poles are at frequencies 55 Hz, 209 Hz, 300 Hz, 794 Hz and 5200 Hz. The zeros are at the frequencies 115 Hz, 259.5 Hz, 408 Hz and 859.5 Hz.

The poles f_{pi} and zeros f_{sj} can also be found approximately from the concepts of parallel and successive resonances or resonances of tensions and currents:

$$f_{p1} = \frac{1}{2\pi} \sqrt{\frac{C_1}{\mu_4}} = 50 \text{ Hz}, \quad (5)$$

$$f_{p2} = \frac{1}{2\pi} \sqrt{\frac{C_2 + C_{S2}}{\mu_3 + m_3}} = 232 \text{ Hz},$$

$$f_{p3} = \frac{1}{2\pi} \sqrt{\frac{C_{S1}}{m_2 + \mu_1 + \mu_2}} = 336 \text{ Hz}, \quad (7)$$

$$f_{p4} = \frac{1}{2\pi} \sqrt{\frac{C_1 + C_{S2}}{\mu_{23} + m_2}} = 778 \text{ Hz}, \quad (8)$$

$$f_{p5} = \frac{1}{2\pi} \sqrt{C_2 (\mu_2^{-1} + \mu_3^{-1} + m_2^{-1} + m_3^{-1})} = 5162 \text{ Hz} \quad (9)$$

$$f_{s1} = \frac{1}{2\pi} \sqrt{\frac{C_3}{\mu_3}} = 104 \text{ Hz}, \quad (10)$$

$$f_{s2} = \frac{1}{2\pi} \sqrt{\frac{C_{S3}}{m_3}} = 259.5 \text{ Hz}, \quad (11)$$

$$f_{s3} = \frac{1}{2\pi} \sqrt{\frac{C_1}{\mu_2}} = 397 \text{ Hz}, \quad (12)$$

$$f_{s4} = \frac{1}{2\pi} \sqrt{\frac{C_{S2}}{m_2}} = 859.5 \text{ Hz}, \quad (13)$$

As we see, the approximate and exact frequencies are very similar to each other. Therefore, the formulas (5) – (13) can be used for the analysis of resonances.

Now, let us use the linear graph method (Mason and Zimmermann, 1960) to obtain a general form for this model. A linear graph for the circuit in Fig. 2 is constructed in Fig. 4. This graph illustrates the relations between forces F_i (upper nodes) and velocities v_i (lower nodes). The lines between them are transmissions, which in this case are mechanical

admittances y_i or mechanical impedances z_i . Thus, in this graph we use relations

$$v_i = y_i \cdot F_i \text{ and } F_i = z_i \cdot v_i \quad (14)$$

In order to simplify the graph, the number of nodes can be reduced retaining only the nodes which we need to determine. Further simplification of the graph can be implemented by adding parallel transmissions and excluding the nodes, which we do not need to determine, by splitting them. Hence, splitting the nodes $F_{\mu i}$, v_{Ci} , $v_{\mu i}$ and excluding the loops l_i , we can obtain the transformed graph presented in Fig. 5. Here,

$$y_{\mu i} = 1/(j\omega \mu_i), \quad y_{Ci} = j\omega / C_i, \\ y_{Si} = 1/(j\omega \mu_i + C_i / (j\omega)) \quad (15)$$

The transmissions of this graph can be determined by the following formulas

$$T_{11} = \frac{y_{\mu 1}}{y_{Ci}(1-l_1)}, \quad T_{12} = \frac{y_{\mu 2}}{y_{Ci}(1-l_1)}, \\ T_{21} = \frac{y_{\mu 2}}{y_{C2}(1-l_2)}, \quad T_{22} = \frac{1}{y_{C2}(1-l_2)}, \\ T_{23} = \frac{y_{\mu 3}}{y_{C2}(1-l_2)}, \quad T_{32} = \frac{y_{\mu 3}}{y_{C3}(1-l_3)}, \\ T_{33} = \frac{y_{\mu 4}}{y_{C3}(1-l_3)}. \quad (16)$$

Where

$$l_1 = -(y_{\mu 1} + y_{\mu 2})/y_{C1}, \quad l_3 = -(y_{\mu 3} + y_{\mu 4})/y_{C3}, \\ l_2 = -(y_{\mu 2} + y_{\mu 3} + y_{S2} + y_{S3})/y_{C2}. \quad (17)$$

This graph can also be described by the equations determining the nodes in relation to adjacent nodes and transmissions that link them:

$$F_{C1} - T_{12}F_{C2} = T_{11}F_1(t) \\ -T_{21}F_{C1} + F_{C2} - T_{23}F_{C3} = T_{22}\dot{S}_2(t) \quad (18) \\ -T_{32}F_{C2} + F_{C3} = T_{33}F_4(t)$$

Substituting (16) and (17) in (18) and multiplying each of the i th equation (18) by $y_{Ci}(1-l_i)$, we have

$$y_{11}F_{C1} - y_{12}F_{C2} = y_{\mu 1}F_1(t) \\ -y_{21}F_{C1} + y_{22}F_{C2} - y_{23}F_{C3} = \dot{S}_2(t) \quad (19)$$

$$-y_{32}F_{C2} + y_{33}F_{C3} = F_4(t)$$

Where $y_{11} = y_{C1} + y_{\mu 1} + y_{\mu 2}$, $y_{12} = y_{21} = y_{\mu 2}$,

$$y_{22} = y_{C2} + y_{\mu 2} + y_{\mu 3} + y_{S2} + y_{S3}, \quad (20)$$

$$y_{23} = y_{32} = y_{\mu 3}, \quad y_{33} = y_{C3} + y_{\mu 3} + y_{\mu 4}.$$

As we can see from equation (19) and (20), equation (19) has the form

$$Y \times F_c = P, \quad (21)$$

Here, the matrix of the mechanical conductance Y is symmetrical; each its diagonal element is positive and equal to the sum of the input mechanical conductances of the elements, which enter the i th node. Each non-diagonal element is negative and equal to the transition conductance of the elements, which locate between i th and j th nodes. This type of matrix is known in the circuit theory as matrix of node equations (Karni, 1966).

The excitation term in the right-hand part of the i th equation is equal to the velocity of cinematic error in the gear engagement, in the case of cinematic excitation. In the case of force excitation, it equals to the product of the exciting force and the transition conductance between the point of application of the force and the i th node.

Therefore, it is not necessary to compose equivalent electric circuits and graphs. Instead, following the rules explained above, we can directly compose the matrix of mechanical conductance and the vector of the right-hand part of the equations.

The above formulated rules can be extended to more complicated systems and systems with distributed parameters.

A dynamic calculation of the gear with the parameters mentioned above was implemented using the equations (15) – (20). The damping in elastic elements was considered by introducing complex stiffness (Skudrzyk, 1968).

$$\bar{C}_i = C_i(1 + j\eta_i), \quad (22)$$

Where η_i - loss factor in i th elastic element.

The results of calculation of dynamical forces F_{Ci} in elastic elements are presented in Fig.6; the amplitude of kinematic excitation $\dot{S}_2 = 5 \mu m$ and the loss factor in all of the elastic elements was taken equal to 0.1. As we see from the graph, in the low frequency range the dynamic forces in each elastic element are the same. The resonance at the frequency 55 Hz corresponds to the frequency of natural vibrations of mass μ_4 at the stiffness C_3 , and the high frequency resonance at 5200 Hz is the natural frequency of

vibrations of all masses at the stiffness C_2 of the gear engagement. The origin of all other resonances can be checked with the aid of equations (5) – (9).

The measurement of noise and vibration of this gear shows that it has high levels at frequency 5200 Hz.

III. CONCLUSIONS

- The use of electric analogy allows us to avoid the derivation of equations of motion and to make a frequency analysis without solving the equations.
- Equations analogous to node equations known in the circuit theory can be used in the gear dynamics for the systems with concentrated and distributed parameters.
- There is no need to compose any electric circuit and linear graph to obtain linear equations of motion of a dynamic system. They can be composed as node equations directly for a dynamic model.

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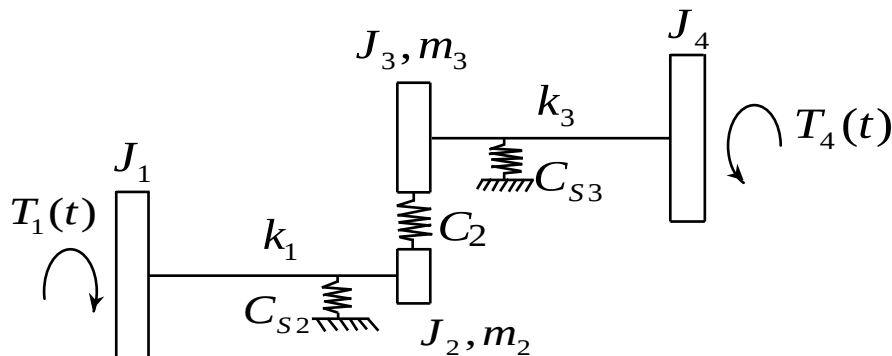


Fig. 1 : Gear dynamic model

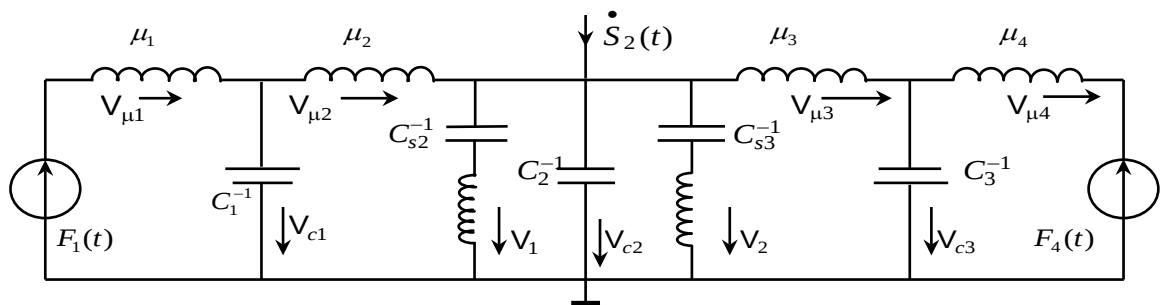


Fig. 2 : Equivalent electrical circuit

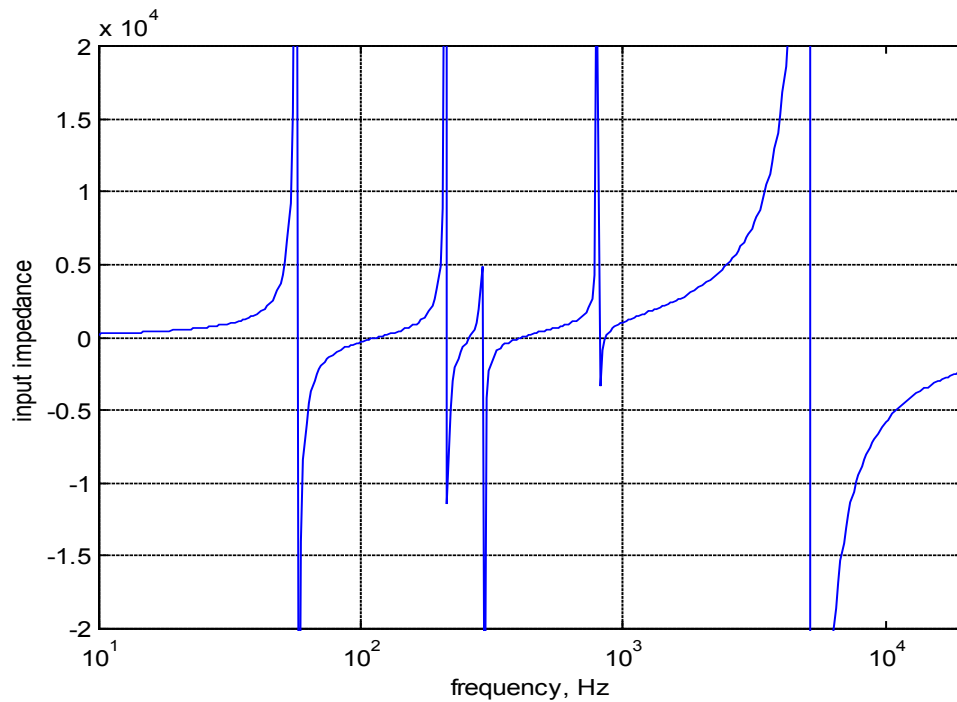


Fig. 3 : Frequency characteristic of input impedance

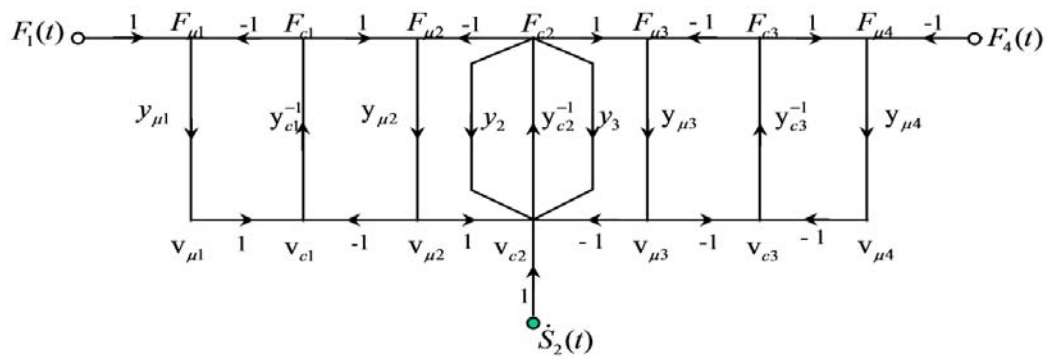


Fig. 4 : Linear graph of gear dynamic model

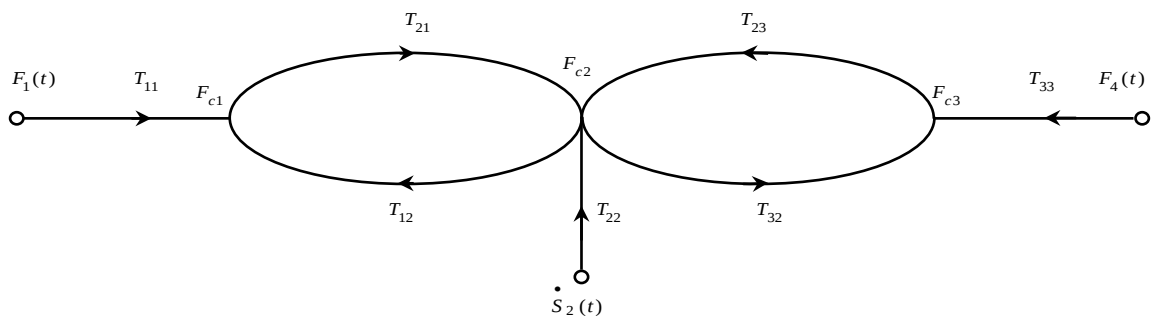


Fig. 5 : Transformed linear graph of gear dynam

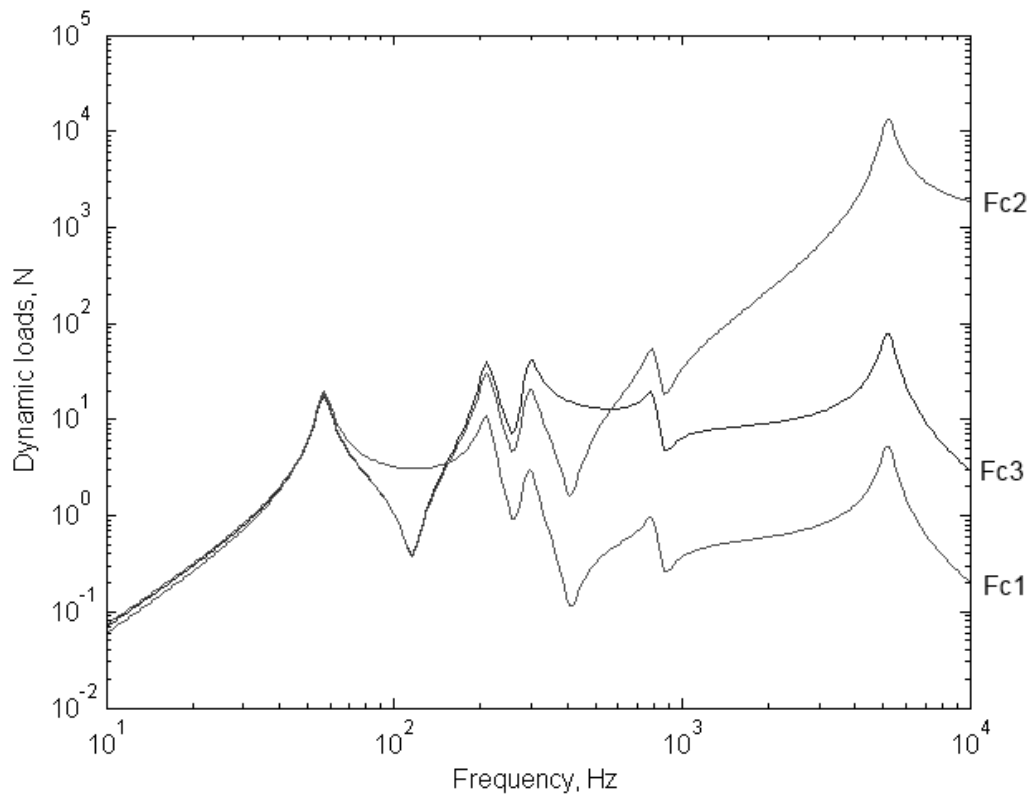


Fig. 6 Frequency characteristic of dynamic loads in the gear:
 Fc1 - in the gear support, Fc3 – in the pinion support,
 Fc2 – in the gear engagement

Fig. 6 : Dynamic loads in the gear



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An Inhomogeneous Gravitational Field and the Body without Center of Gravity

By Milutin Marjanov

Introduction- Concept of homogeneity (or inhomogeneity) of the gravitational field is a rather specific one. Namely, according to the Newton's law of gravitation, either intensity or direction, or each of these two characteristics of the gravitational force acting on the body, depend on its position in the gravitational field. So, in fact, for the body as a whole, the gravitational field is always an inhomogeneous one. Such a classification makes sense only if it is restricted to the active part of the gravitational field, that is, on the part occupied by the body.

Keywords: homogeneous and inhomogeneous gravitational field newton's gravitational force gravitational moment.

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AN INHOMOGENEOUS GRAVITATIONAL FIELD AND THE BODY WITHOUT CENTER OF GRAVITY

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I. INTRODUCTION

Concept of homogeneity (or inhomogeneity) of the gravitational field is a rather specific one. Namely, according to the Newton's law of gravitation, either intensity or direction, or each of these two characteristics of the gravitational force acting on the body, depend on its position in the gravitational field. So, in fact, for the body as a whole, the gravitational field is always an inhomogeneous one. Such a classification makes sense only if it is restricted to the active part of the gravitational field, that is, on the part occupied by the body.

II. HOMOGENEOUS AND INHOMOGENEOUS GRAVITATIONAL FIELD

Consider a body of mass m moving in the gravitational field of the dominant gravitational center of

mass m^* . Assume that $m/m^* \ll 1$, so the gravitational field is a stationary one. Gravitational noise, as well as the gravitational anomalies, are excluded.

The motion of the body is composed: while moving in its orbit, it revolves about its principal central axis of inertia (1), which is perpendicular to the orbital plane. The mass center C of the body is chosen to be at the origin of two moving frames of reference xCy and $\xi C\eta$. The first one is related to the geometry of the orbit, Cx being oriented toward the gravitational center, that is toward its mass center C^* . The orbital angle is ψ . The second frame is related to the geometry of mass of the body, $C\xi$ having direction of the principal axis (3) and $C\eta$ – direction of the axis (2) of the ellipsoid of inertia. Position of the second reference frame with respect to the first one is defined by the angle of relative rotation ϕ (Fig.1).

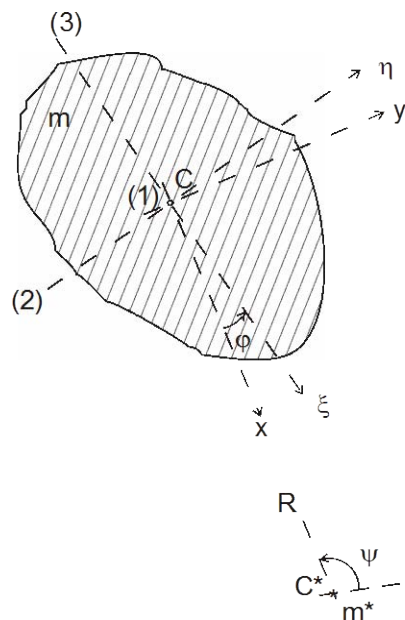


Fig. 1 : Body in the gravitational field and two frames of reference

In a homogeneous gravitational field, intensities and directions of the elementary gravitational forces

acting on the body's particles depend on the position $(\overline{CC^*} = R, \psi)$ of the mass center in the gravitational field, solely. They are functions neither of

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the positions of the particles (ξ, η) within the body, nor of the angle of relative rotation ϕ . All these forces have the same direction, that is, they are parallel to the coordinate axis Cx and their sum, the "weight" of the body, coincides with that line, regardless of the relative position of the body in the frame of reference xCy . In a homogeneous gravitational field the resultant of the

elementary gravitational forces always passes through the mass center of the body and the gravitational moment does not exist. In fact, the mass center of the body in a homogeneous gravitational field represents the center of gravity, as conceived by Archimedes some 2,5 centuries B.C. (Fig. 2).

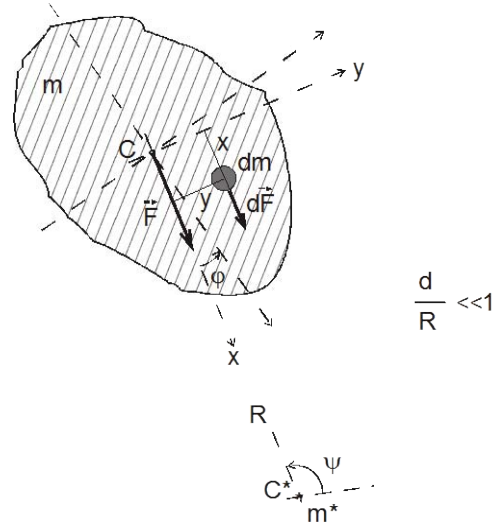


Fig. 2 : Homogeneous gravitational field

Such an interpretation of the gravitational field acting on the body is only possible if the dimensions of the body are negligible compared to the distance between the mass center of the body and of the gravitational center. If the largest dimension of the body is d , invariability of intensities and directions of the gravitational forces acting on the body's particles imply $d/R \approx 0$ compared to unity in the approximate calculus of the gravitational load $\vec{F}, \vec{M}^C$.

On the other hand, if the gravitational field is inhomogeneous one, at least the first power of the fraction d/R has to be retained in the expression

containing unity in the course of calculus of the gravitational load. Depending on the retained power of d/R it is possible to speak of the first, the second, or the higher order inhomogeneity of the field. In the inhomogeneous gravitational field intensities and directions of the elementary forces depend on the position of the mass center in the gravitational field, but also on the position of the particles within the body, as well as on the relative position of the body.

$$d\vec{F} = d\vec{F}(R, \Psi, \xi, \eta, \phi)$$

All these forces converge toward the gravitational center and so does their resultant.

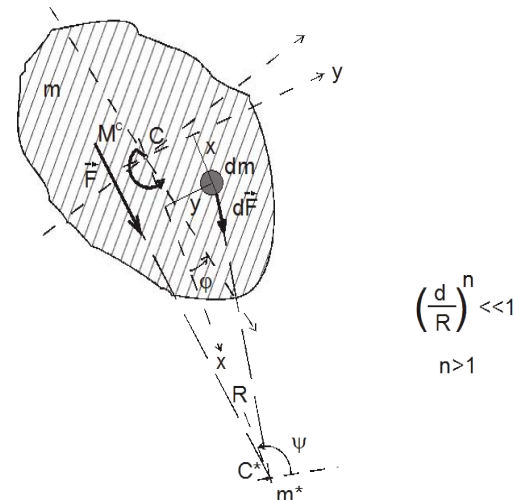


Fig. 3 : Inhomogeneous gravitational field.

Generally, this resultant doesn't pass through the mass center of the body, so it has to produce the gravitational moment (Fig. 3).

Within the first order inhomogeneity case, the gravitational force is the same as in the homogeneous gravitational field

$$F = G \frac{m \cdot m^*}{R^2}$$

Where G is the gravitational constant and the gravitational moment for the described motion is equal

$$M^C = -\frac{3}{2} G \frac{m^* (I_2 - I_3)}{R^3} \sin 2\varphi,$$

Where I_2 and I_3 are the medium and the minimum principal moments of inertia for the mass center of the body. Obviously, the gravitational moment is a harmonic function of the double angle of relative rotation, with the amplitude depending on the mass of the gravitational center, on the distance between the

body and this center and finally, on the mass distribution in the body.

When the small body goes around the large body in a closed orbit, its orbital and rotational motions gradually become resonant just because of the gravitational torque existence ($3/4$). For example the Moon circulates around Earth and rotates around its axis in the $1/1$ resonance

The first characteristic of inhomogeneity of the gravitational field is the existence of the gravitational moment, in the general case. The second one is the absence of the center of gravity of the body.

III. BODY WITHOUT CENTER OF GRAVITY

Authors of many of textbooks are not quite precise about that point. Having, probably, in mind the existence of the gravitational moment in such a field, they often claim implicitly, or even explicitly, that in an inhomogeneous gravitational field the center of gravity doesn't coincide with the mass center of the body. This is definitely wrong, of course, because such an assertion may lead the reader to the false

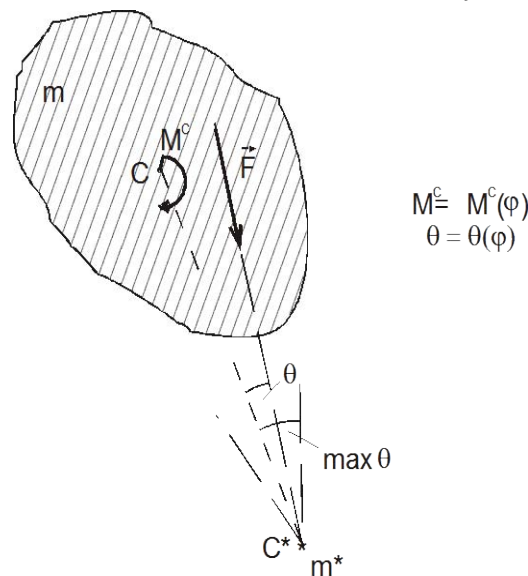


Fig. 4 : Oscillation of the gravitational force around the gravitational center

conclusion that there exists something like a "moving center of the gravity" in the rotating body exposed to the inhomogeneous gravitational field. There is no such a point in, or in the vicinity of the body, satisfying the definition of the center of gravity, if the body is exposed to the field of the convergent gravitational forces. The "weight" vector of the body has to pass through the point toward which converge all its components and that is the gravitational center. The relative rotation of the body produces tilting of this vector about this center (Fig. 4).

The angle between the gravitational force and the direction CC^* is equal

$$\theta = \frac{3}{2} \frac{I_2 - I_3}{mR^3} \cdot \sin 2\varphi.$$

IV. CONCLUSION

We have stressed the distinction between homogeneous and inhomogeneous gravitational fields. A homogeneous gravitational field is marked by the existence of the center of gravity and the absence of the gravitational moment acting on the body. On the other hand, in an inhomogeneous gravitational field the body has no center of gravity and the gravitational moment, generally, exist. Concerning the calculus of the

gravitational load, one has to adopt $d/R \approx 0$, compared to unity, for the homogeneous and at least $d/R \neq 0$, compared to unity, for an inhomogeneous gravitational field.

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Concept of the Dispersion of Electric and Magnetic Inductivities and its Physical Interpretation

By F.F. Mende

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Abstract- In a number of scientific publications is asserted that the permittivity and permeability of material media depends on frequency. But even Maxwell himself, who was the author of the basic equations of electrodynamics, believed that ϵ and μ were frequency-independent fundamental constants. The article shows that Max well was right, and the recognition of the presence of dispersion in the dielectric constant and magnetic permeability is a physical and methodological error. In it is shown that the kinetic inductance of charge has the same fundamental value as the dielectric and magnetic constant of material media. Are introduced the new concepts of the magneto electro kinetic wave and electro magneto potential waves, and also the kinetic capacitance.

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Keywords: max well questions; plasma media; dielectric media; magnetic media; permittivity; permeability; kinetic inductivity; polarization vector; london equation; magnetic resonance; magneto electro kinetic wave; electro magneto potential waves; kinetic capacitanc.

I. INTRODUCTION

How the idea of ϵ and μ -dispersion appeared and evolved is illustrated vividly in the monograph of well-known specialists in physics of plasma [1]: while working at the equations of electrodynamics of material, media, G. Maxwell looked upon electric and magnetic inductivities as constants (that is why this approach was so lasting). Much later, at the beginning of the XX century, G. Heavisidr and R.Wull put forward their explanation for phenomena of optical dispersion (in particular rainbow) in which electric and magnetic inductivities came as functions of frequency. Quite recently, in the mid-50ies of the last century, physicists arrived at the conclusion that these parameters were dependent not only on the frequency but on the wave vector as well. That was a revolutionary breakaway from the current concepts. The importance of the problem is clearly illustrated by what happened at a seminar held by L. D. Landau in 1954, where he interrupted A. L. Akhiezer reporting on the subject: "Nonsense, the refractive index cannot be a function of the refractive index". Note, this was said by L. D. Landau, an outstanding physicist of our time.

What is the actual situation? Running ahead, I can admit that Maxwell was right: both ϵ and μ are frequency – independent constants characterizing one or another material medium. Since dispersion of electric and magnetic inductivities of material media is one of

the basic problems of the present – day physics and electrodynamics, the system of views on these questions has to be radically altered again.

II. PLASMA MEDIA

It is noted in the introduction that dispersion of electric and magnetic inductivities of material media is a commonly accepted idea [1-5]. The idea is however not correct.

To explain this statement and to gain a better understanding of the physical essence of the problem, we start with a simple example showing how electric lumped-parameter circuits can be described [6]. As we can see below, this example is directly concerned with the problem of our interest and will give us a better insight into the physical picture of the electro dynamic processes in material media.

In a parallel resonance circuit including a capacitor C and an inductance coil L , the applied voltage U and the total current I_Σ through the circuit are related as

$$I_\Sigma = I_C + I_L = C \frac{dU}{dt} + \frac{1}{L} \int U dt ,$$

where $I_C = C \frac{dU}{dt}$ is the current through the capacitor, $I_L = \frac{1}{L} \int U dt$ is the current through the inductance coil. For the harmonic voltage $U = U_0 \sin \omega t$

$$I_\Sigma = \left(\omega C - \frac{1}{\omega L} \right) U_0 \cos \omega t . \quad (2.1)$$

The term in brackets is the total susceptance σ_x of the circuit, which consists of the capacitive σ_c and inductive σ_L components

$$\sigma_x = \sigma_c + \sigma_L = \omega C - \frac{1}{\omega L} .$$

Eq. (2.1) can be re-written as

$$I_\Sigma = \omega C \left(1 - \frac{\omega_0^2}{\omega^2} \right) U_0 \cos \omega t ,$$

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Where $\omega_0^2 = \frac{1}{LC}$ is the resonance frequency

of a parallel circuit.

From the mathematical (i.e. other than physical) standpoint, we may assume a circuit that has only a capacitor and no inductance coil. Its frequency – dependent capacitance is

$$C^*(\omega) = C \left(1 - \frac{\omega_0^2}{\omega^2} \right). \quad (2.2)$$

Another approach is possible, which is correct too.

Eq. (2.1) can be re-written as

$$I_\Sigma = - \frac{\left(\frac{\omega^2}{\omega_0^2} - 1 \right)}{\omega L} U_0 \cos \omega t.$$

In this case the circuit is assumed to include only an inductance coil and no capacitor. Its frequency – dependent inductance is

$$L^*(\omega) = \frac{L}{\left(\frac{\omega^2}{\omega_0^2} - 1 \right)}. \quad (2.3)$$

Using the notion Eqs. (2.2) and (2.3), we can write

$$I_\Sigma = \omega C^*(\omega) U_0 \cos \omega t, \quad (2.4)$$

or

$$I_\Sigma = - \frac{1}{\omega L^*(\omega)} U_0 \cos \omega t. \quad (2.5)$$

Eqs (2.4) and (2.5) are equivalent and each of them provides a complete mathematical description of the circuit. From the physical point of view, $C^*(\omega)$ and $L^*(\omega)$ do not represent capacitance and inductance though they have the corresponding dimensions. Their physical sense is as follows:

$$C^*(\omega) = \frac{\sigma_X}{\omega},$$

i.e. $C^*(\omega)$ is the total susceptance of this circuit divided by frequency:

$$L^*(\omega) = \frac{1}{\omega \sigma_X},$$

and $L^*(\omega)$ is the inverse value of the product of the total susceptance and the frequency.

Amount $C^*(\omega)$ is constricted mathematically so that it includes C and L simultaneously. The same is true for $L^*(\omega)$.

We shall not consider here any other cases, e.g., series or more complex circuits. It is however important to note that applying the above method, any circuit consisting of the reactive components C and L can be described either through frequency – dependent inductance or frequency – dependent capacitance.

But this is only a mathematical description of real circuits with constant – value reactive elements.

It is well known that the energy stored in the capacitor and inductance coil can be found as

$$W_C = \frac{1}{2} C U^2, \quad (2.6)$$

$$W_L = \frac{1}{2} L I^2. \quad (2.7)$$

But what can be done if we have $C^*(\omega)$ and $L^*(\omega)$? There is no way of substituting them into Eqs. (2.6) and (2.7) because they can be both positive and negative. It can be shown readily that the energy stored in the circuit analyzed is

$$W_\Sigma = \frac{1}{2} \cdot \frac{d \sigma_X}{d \omega} U^2, \quad (2.8)$$

or

$$W_\Sigma = \frac{1}{2} \cdot \frac{d [\omega C^*(\omega)]}{d \omega} U^2, \quad (2.9)$$

or

$$W_\Sigma = \frac{1}{2} \cdot \frac{d \left(\frac{1}{\omega L^*(\omega)} \right)}{d \omega} U^2. \quad (3.10)$$

Having written Eqs. (2.8), (2.9) or (2.10) in greater detail, we arrive at the same result:

$$W_\Sigma = \frac{1}{2} C U^2 + \frac{1}{2} L I^2,$$

Where U is the voltage at the capacitor and I is the current through the inductance coil. Below we consider the physical meaning of the magnitudes $\varepsilon(\omega)$ and $\mu(\omega)$ for material media.

A superconductor is a perfect plasma medium in which charge carriers (electrons) can move without friction. In this case the equation of motion is

$$m \frac{d \vec{V}}{d t} = e \vec{E} \quad (2.11)$$

Where m and e are the electron mass and charge, respectively; $\vec{E}$ is the electric field strength, $\vec{V}$ is the velocity. Taking into account the current density

$$\vec{j} = n e \vec{V}, \quad (2.12)$$

we can obtain from Eq. (2.11)

$$\vec{j}_L = \frac{n e^2}{m} \int \vec{E} d t \quad (2.13)$$

In Eqs. (2.12) and (2.13) n is the specific charge density. Introducing the notion

$$L_k = \frac{m}{n e^2},$$

we can write

$$\vec{j}_L = \frac{1}{L_k} \int \vec{E} d t \quad (2.14)$$

Here L_k is the kinetic inductivity of the medium [7-11]. Its existence is based on the fact that a charge carrier has a mass and hence it possesses inertia properties.

For harmonic fields we have $\vec{E} = \vec{E}_0 \sin \omega t$ and Eq. (2.14) becomes

$$\vec{j}_L = -\frac{1}{\omega L_k} E_0 \cos \omega t \quad (2.15)$$

Eqs. (2.14) and (2.15) show that $\vec{j}_L$ is the current through the inductance coil.

In this case the Maxwell equations take the following form

$$\operatorname{rot} \vec{E} = -\mu_0 \frac{\partial \vec{H}}{\partial t},$$

$$\operatorname{rot} \vec{H} = \vec{j}_C + \vec{j}_L = \varepsilon_0 \frac{\partial \vec{E}}{\partial t} + \frac{1}{L_k} \int \vec{E} d t, \quad (2.16)$$

Where ε_0 and μ_0 are the electric and magnetic inductivities in vacuum, $\vec{j}_C$ and $\vec{j}_L$ are the displacement and conduction currents, respectively. As was shown above, $\vec{j}_L$ is the inductive current.

Eq. (2.16) gives

$$\operatorname{rot} \operatorname{rot} \vec{H} + \mu_0 \varepsilon_0 \frac{\partial^2 \vec{H}}{\partial t^2} + \frac{\mu_0}{L_k} \vec{H} = 0 \quad (2.17)$$

For time-independent fields, Eq. (2.17) transforms into the London equation [12]

$$\operatorname{rot} \operatorname{rot} \vec{H} + \frac{\mu_0}{L_k} \vec{H} = 0,$$

where $\lambda_L^2 = \frac{L_k}{\mu_0}$ is the London depth of penetration.

As Eq. (2.16) shows, the inductivities of plasma (both electric and magnetic) are frequency – independent and equal to the corresponding parameters for vacuum. Besides, such plasma has another fundamental material characteristic – kinetic inductivity.

Eqs. (2.16) hold for both constant and variable fields. For harmonic fields $\vec{E} = \vec{E}_0 \sin \omega t$, Eq. (2.16) gives

$$\operatorname{rot} \vec{H} = \left(\varepsilon_0 \omega - \frac{1}{L_k \omega} \right) \vec{E}_0 \cos \omega t \quad (2.18)$$

Taking the bracketed value as the specific susceptance σ_x of plasma, we can write

$$\operatorname{rot} \vec{H} = \sigma_x \vec{E}_0 \cos \omega t \quad (2.19)$$

where

$$\sigma_x = \varepsilon_0 \omega - \frac{1}{\omega L_k} = \varepsilon_0 \omega \left(1 - \frac{\omega_p^2}{\omega^2} \right) = \omega \varepsilon^*(\omega), \quad (2.20)$$

$$\text{and } \varepsilon^*(\omega) = \varepsilon_0 \left(1 - \frac{\omega_p^2}{\omega^2} \right), \text{ where } \omega_p^2 = \frac{1}{\varepsilon_0 L_k}$$

is the plasma frequency.

Now Eq. (2.19) can be re-written as

$$\text{rot } \vec{H} = \omega \varepsilon_0 \left(1 - \frac{\omega_p^2}{\omega^2} \right) \vec{E}_0 \cos \omega t,$$

or

$$\text{rot } \vec{H} = \omega \varepsilon^*(\omega) \vec{E}_0 \cos \omega t.$$

The $\varepsilon^*(\omega)$ -parameter is conventionally called the frequency-dependent electric inductivity of plasma. In reality however this magnitude includes simultaneously the electric inductivity of vacuum and the kinetic inductivity of plasma. It can be found as

$$\varepsilon^*(\omega) = \frac{\sigma_X}{\omega}.$$

It is evident that there is another way of writing σ_X

$$\sigma_X = \varepsilon_0 \omega - \frac{1}{\omega L_k} = \frac{1}{\omega L_k} \left(\frac{\omega^2}{\omega_p^2} - 1 \right) = \frac{1}{\omega L_k^*}, \quad (2.21)$$

where

$$L_k^*(\omega) = \frac{L_k}{\left(\frac{\omega^2}{\omega_p^2} - 1 \right)} = \frac{1}{\sigma_X \omega}.$$

$L_k^*(\omega)$ written this way includes both ε_0 and L_k .

Eqs. (2.20) and (2.21) are equivalent, and it is safe to say that plasma is characterized by the frequency-dependent kinetic inductance $L_k^*(\omega)$ rather than by the frequency-dependent electric inductivity $\varepsilon^*(\omega)$.

Eq. (2.18) can be re-written using the parameters $\varepsilon^*(\omega)$ and $L_k^*(\omega)$

$$\text{rot } \vec{H} = \omega \varepsilon^*(\omega) \vec{E}_0 \cos \omega t, \quad (2.22)$$

or

$$\text{rot } \vec{H} = \frac{1}{\omega L_k^*(\omega)} \vec{E}_0 \cos \omega t. \quad (2.23)$$

Eqs. (2.22) and (2.23) are equivalent.

Thus, the parameter $\varepsilon^*(\omega)$ is not an electric inductivity though it has its dimensions. The same can be said about $L_k^*(\omega)$.

We can see readily that

$$\varepsilon^*(\omega) = \frac{\sigma_X}{\omega},$$

$$L_k^*(\omega) = \frac{1}{\sigma_X \omega}.$$

These relations describe the physical meaning of $\varepsilon^*(\omega)$ and $L_k^*(\omega)$.

Of course, the parameters $\varepsilon^*(\omega)$ and $L_k^*(\omega)$ are hardly usable for calculating energy by the following equations

$$W_E = \frac{1}{2} \varepsilon E_0^2$$

and

$$W_j = \frac{1}{2} L_k j_0^2.$$

For this purpose the Eq. (2.9)-type formula was devised in [2]:

$$W = \frac{1}{2} \cdot \frac{d[\omega \varepsilon^*(\omega)]}{d\omega} E_0^2. \quad (2.24)$$

Using Eq. (2.24), we can obtain

$$W_\Sigma = \frac{1}{2} \varepsilon_0 E_0^2 + \frac{1}{2} \cdot \frac{1}{\omega^2 L_k} E_0^2 = \frac{1}{2} \varepsilon_0 E_0^2 + \frac{1}{2} L_k j_0^2$$

The same result is obtainable from

$$W = \frac{1}{2} \cdot \frac{d \left[\frac{1}{\omega L_k^*(\omega)} \right]}{d\omega} E_0^2.$$

As in the case of a parallel circuit, either of the parameters $\varepsilon^*(\omega)$ and $L_k^*(\omega)$, similarly to $C^*(\omega)$ and $L^*(\omega)$, characterize completely the electro dynamic properties of plasma. The case

$$\varepsilon^*(\omega) = 0$$

$$L_k^*(\omega) = \infty$$

corresponds to the resonance of current.

We have found that $\alpha(\omega)$ is not dielectric inductivity permittivity. Instead, it includes two frequency-independent parameters ϵ_0 and L_k . What is the reason for the physical misunderstanding of the parameter $\alpha(\omega)$? This occurs first of all because for the case of plasma the $\frac{1}{L_k} \int \vec{E} d\vec{t}$ - type term is not explicitly present in the second Maxwell equation.

There is however another reason for this serious mistake in the present-day physics [2] as an example. This study states that there is no difference between dielectrics and conductors at very high frequencies. On this basis the authors suggest the existence of a polarization vector in conducting media and this vector is introduced from the relation

$$\vec{P} = \sum e \vec{r}_m = n e \vec{r}_m, \quad (2.25)$$

Where n is the charge carrier density, $\vec{r}_m$ is the current charge displacement. This approach is physically erroneous because only bound charges can polarize and form electric dipoles when the external field overcoming the attraction force of the bound charges accumulates extra electrostatic energy in the dipoles. In conductors the charges are not bound and their displacement would not produce any extra electrostatic energy. This is especially obvious if we employ the induction technique to induce current (i.e. to displace charges) in a ring conductor. In this case there is no restoring force to act upon the charges, hence, no electric polarization is possible. In [2] the polarization vector found from Eq. (2.25) is introduced into the electric induction of conducting media

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P},$$

Where the vector $\vec{P}$ of a metal is obtained from Eq. (2.25), which is wrong.
Since

$$\vec{r}_m = -\frac{e^2}{m \omega^2} \vec{E},$$

for free carriers, then

$$\vec{P}^*(\omega) = -\frac{n e^2}{m \omega^2} \vec{E},$$

for plasma, and

$$\vec{D}^*(\omega) = \epsilon_0 \vec{E} + \vec{P}^*(\omega) = \epsilon_0 \left(1 - \frac{\omega_p^2}{\omega^2} \right) \vec{E}.$$

Thus, the total accumulated energy is

$$W_\Sigma = \frac{1}{2} \epsilon_0 E^2 + \frac{1}{2} \cdot \frac{1}{L_k \omega^2} E^2. \quad (2.26)$$

However, the second term in the right-hand side of Eq. (2.26) is the kinetic energy (in contrast to dielectrics for which this term is the potential energy). Hence, the electric induction vector $\vec{D}^*(\omega)$ does not correspond to the physical definition of the electric induction vector.

The physical meaning of the introduced vector

$\vec{P}^*(\omega)$ is clear from

$$\vec{P}^*(\omega) = \frac{\sigma_L}{\omega} \vec{E} = \frac{1}{L_k \omega^2} \vec{E}.$$

The interpretation of $\epsilon(\omega)$ as frequency-dependent inductivity has been harmful for correct understanding of the real physical picture (especially in the educational processes). Besides, it has drawn away the researchers attention from some physical phenomena in plasma, which first of all include the transverse plasma resonance and three energy components of the magneto electro kinetic wave propagating in plasma [13-14].

III. DIELECTRIC MEDIA

Applied fields cause polarization of bound charges in dielectrics. The polarization takes some energy from the field source, and the dielectric accumulates extra electrostatic energy. The extent of displacement of the polarized charges from the equilibrium is dependent on the electric field and the coefficient of elasticity β , characterizing the elasticity of the charge bonds. These parameters are related as

$$-\omega^2 \vec{r}_m + \frac{\beta}{m} \vec{r}_m = \frac{e}{m} \vec{E}, \quad (3.1)$$

Where $\vec{r}_m$ is the charge displacement from the equilibrium.

Putting ω_0 for the resonance frequency of the bound charges and taking into account that $\omega_0 = \beta/m$ we obtain from Eq. (3.1)

$$\vec{r}_m = -\frac{e \vec{E}}{m (\omega^2 - \omega_0^2)}$$

The polarization vector becomes

$$\vec{P}^* = -\frac{n e^2}{m} \cdot \frac{1}{(\omega^2 - \omega_0^2)} \vec{E}.$$

Since

$$\vec{P} = \varepsilon_0 (\varepsilon - 1) \vec{E},$$

we obtain

$$\varepsilon'_{\partial} * (\omega) = 1 - \frac{n e^2}{\varepsilon_0 m} \cdot \frac{1}{\omega^2 - \omega_0^2}.$$

The quantity $\varepsilon'_{\partial} * (\omega)$ is commonly called the relative frequency dependably electric inductivity. Its absolute value can be found as

$$\varepsilon_{\partial} * (\omega) = \varepsilon_0 \left(1 - \frac{n e^2}{\varepsilon_0 m} \cdot \frac{1}{\omega^2 - \omega_0^2} \right). \quad (3.2)$$

Once again, we arrive at the frequency-dependent dielectric permittivity. Let us take a closer look at the quantity $\varepsilon_{\partial} * (\omega)$. As before, we introduce $L_{k \partial} = \frac{m}{n e^2}$ and $\omega_{p \partial} = \frac{1}{L_{k \partial} \varepsilon_0}$ and see immediately that the vibrating charges of the dielectric have masses and thus possess inertia properties. As a result, their kinetic inductivity would make itself evident too. Eq. (3.2) can be re-written as

$$\varepsilon_{\partial} * (\omega) = \varepsilon_0 \left(1 - \frac{\omega_{p \partial}^2}{\omega^2 - \omega_0^2} \right).$$

It is appropriate to examine two limiting cases: $\omega \gg \omega_0$ and $\omega < \omega_0$.

If $\omega \gg \omega_0$,

$$\varepsilon_{\partial} * (\omega) = \varepsilon_0 \left(1 - \frac{\omega_{p \partial}^2}{\omega^2} \right),$$

$$\mu_T * (\omega) = 1 - \frac{\Omega |\gamma| M_0}{\mu_0 (\omega^2 - \Omega^2)},$$

and the dielectric behaves just like plasma. This case has prompted the idea that at high frequencies there is no difference between dielectrics and plasma. The idea served as a basis for introducing the polarization vector in conductors [2]. The difference however exists and it is of fundamental importance. In dielectrics, because of inertia, the amplitude of charge vibrations is very small at high frequencies and so is the polarization vector. The polarization vector is always zero in conductors.

For $\omega < \omega_0$,

$$\varepsilon_{\partial} * (\omega) = \varepsilon_0 \left(1 + \frac{\omega_{p \partial}^2}{\omega_0^2} \right),$$

and the permittivity of the dielectric is independent of frequency. It is $\left(1 + \frac{\omega_{p \partial}^2}{\omega_0^2} \right)$ times higher than in vacuum. This result is quite clear. At $\omega \gg \omega_0$ the inertia properties are inactive and permittivity approaches its value in the static field.

IV. MAGNETIC MEDIA

The resonance phenomena in plasma and dielectrics are characterized by repeated electrostatic-kinetic and kinetic-electrostatic transformations of the charge motion energy during oscillations. This can be described as an electrokinetic process, and devices based on it (lasers, masers, filters, etc.) can be classified as electrokinetic units.

However, another type of resonance is also possible, namely, magnetic resonance. Within the current concepts of frequency-dependent permeability, it is easy to show that such dependence is related to magnetic resonance. For example, let us consider ferromagnetic resonance. A ferrite magnetized by applying a stationary field H_0 parallel to the z-axis will act as an anisotropic magnet in relation to the variable external field. The complex permeability of this medium has the form of a tensor [15]:

$$\mu = \begin{pmatrix} \mu_T * (\omega) & -i \alpha & 0 \\ i \alpha & \mu_T * (\omega) & 0 \\ 0 & 0 & \mu_L \end{pmatrix},$$

where

$$\alpha = \frac{\omega |\gamma| M_0}{\mu_0 (\omega^2 - \Omega^2)}, \quad \mu_L = 1,$$

$$\Omega = |\gamma| H_0. \quad (4.1)$$

Being the natural professional frequency, and

$$M_0 = \mu_0 (\mu - 1) H_0 \quad (4.2)$$

is the medium magnetization.

Taking into account Eqs. (4.1) and (4.2) for $\mu_T * (\omega)$, we can write

$$\mu_T * (\omega) = 1 - \frac{\Omega^2 (\mu - 1)}{\omega^2 - \Omega^2}. \quad (4.3)$$

Assuming that the electromagnetic wave propagates along the x-axis and there are H_y and H_z components, the first Max well equation becomes

$$\text{rot } \vec{E} = \frac{\partial \vec{E}_z}{\partial x} = \mu_0 \mu_T \frac{\partial \vec{H}_y}{\partial t}.$$

Taking into account Eq. (4.3), we obtain

$$\text{rot } \vec{E} = \mu_0 \left[1 - \frac{\Omega^2(\mu-1)}{\omega^2 - \Omega^2} \right] \frac{\partial \vec{H}_y}{\partial t}.$$

For $\omega \gg \Omega$

$$\text{rot } \vec{E} = \mu_0 \left[1 - \frac{\Omega^2(\mu-1)}{\omega^2} \right] \frac{\partial \vec{H}_y}{\partial t}. \quad (4.4)$$

Assuming $\vec{H}_y = \vec{H}_{y0} \sin \omega t$ and taking into account that

$$\frac{\partial \vec{H}_y}{\partial t} = -\omega^2 \int \vec{H}_y dt.$$

Eq. (4.4) gives

$$\text{rot } \vec{E} = \mu_0 \frac{\partial \vec{H}_y}{\partial t} + \mu_0 \Omega^2(\mu-1) \int \vec{H}_y dt,$$

or

$$\text{rot } \vec{E} = \mu_0 \frac{\partial \vec{H}_y}{\partial t} + \frac{1}{C_k} \int \vec{H}_y dt.$$

For $\omega \ll \Omega$

$$\text{rot } \vec{E} = \mu_0 \mu \frac{\partial \vec{H}_y}{\partial t}.$$

The quantity

$$C_k = \frac{1}{\mu_0 \Omega^2 (\mu - 1)}$$

can be described as kinetic capacitance [16-17]. What is its physical meaning? If the direction of the magnetic moment does not coincide with that of the external magnetic field, the vector of the moment starts precessional motion at the frequency Ω about the magnetic field vector. The magnetic moment $\vec{m}$ has the potential energy $U_m = -\vec{m} \cdot \vec{B}$. Like in a charged condenser, U_m is the potential energy because the precessional motion is inertia less (even though it is mechanical) and it stops immediately when the magnetic field is lifted. In the magnetic field the precessional motion lasts until the accumulated potential energy is exhausted and the vector of the magnetic moment becomes parallel to the vector $\vec{H}_0$.

Magnetic resonance occurs at the point $\omega = \Omega$ and $\mu_r^*(\omega) \rightarrow \infty$. It is seen that the resonance frequency of the macroscopic magnetic resonator is independent of the line size and equals Ω .

Thus, the parameter

$$\mu_H^*(\omega) = \mu_0 \left[1 - \frac{\Omega^2(\mu-1)}{\omega^2 - \Omega^2} \right]$$

is not a frequency-dependent permeability.

V. CONCLUSION

Thus, it has been found that along with the fundamental parameters $\epsilon\epsilon_0$ and $\mu\mu_0$ characterizing the electric and magnetic energy accumulated and transferred in the medium, there are two more basic material parameters L_k and C_k . They characterize kinetic and potential energy that can be accumulated and transferred in material media. L_k was sometimes used to describe certain physical phenomena, for example, in superconductors, C_k has never been known to exist. These four fundamental parameters $\epsilon\epsilon_0$, $\mu\mu_0$, L_k and C_k clarify the physical picture of the wave and resonance processes in material media in applied electromagnetic fields. Previously, only electromagnetic waves were thought to propagate and transfer energy in material media. It is clear now that the concept was not complete. In fact, magneto electro kinetic, or electro magneto potential waves travel in material media. The resonances in these media also have specific features. Unlike closed planes with electromagnetic resonance and energy exchange between electric and magnetic fields, material media have two types of resonance – electro kinetic and magneto potential. Under the electro kinetic resonance the energy of the electric field changes to kinetic energy. In the case of magneto potential resonance the potential energy accumulated during the precessional motion can escape outside at the precession frequency.

The notions of permittivity and permeability dispersion thus become physically groundless though $\epsilon^*(\omega)$ and $\mu^*(\omega)$ are handy for a mathematical description of the processes in material media. We should however remember their true meaning especially where educational processes are involved.

It is surprising that Eq. (3.29) actually accounts for the whole of electrodynamics because all current electrodynamics problems can be solved using this equation. What is then a magnetic field? This is merely a convenient mathematical procedure which is not necessarily gives a correct result (e.g., in the case of parallel-moving charges). Now we can state that electrocurrent, rather than electromagnetic, waves travel in space. Their electric field and displacement current vectors are in the same plane and displaced by $\pi/2$.

Any theory is dead unless important practical results are obtained of its basis. The use of the previously unknown transverse plasma resonance [14] is one of the most important practical results following from this study.

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Passenger Safe Car

By D. Giftson Felix & P. Mohan Kumar

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Abstract- In today's world there are more and more cars in the road. For the past few years the amount of automobiles in the road has been increased at the same time number of accidents is also increased. We cannot blame anyone for buying a car it's their wish. Now-a-days many automobile companies are manufacturing cars with high safety for passengers by placing front and side air bag but all these prevent him from a major accident. During accident the injuries to the passenger especially to the driver are caused only by the place where he sits (i.e.) due to the steering column. Hence apart from air bags this idea moves the passenger's seat little backwards so that they move away from the accident zone hence injuries can be reduced. This is done by the use of two master cylinders and two slave cylinders.

Keywords: *master cylinder, slave cylinder, base plate.*

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D. Giftson Felix^a & P. Mohan Kumar^σ

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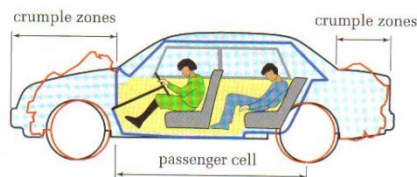
I. INTRODUCTION

Today the number of cars has been increased due to the congestion many accidents occur here and there and many lose their life in this. To overcome this many automobiles are now assisted with air bags, anti lock system, etc. yes, this prevents but it does not moves the passenger from things which hit them especially steering column, Dash board, etc. Hence in this idea the passenger seat itself moves so that injuries are reduced. This in turn saves many lives.

a) Disadvantages of previous improvements

i. Crumple Zones

- Passengers are still at risk due to the small distance of the car moving even after the crumple zone acts.
- Crumple zones can cause glass to shatter which can cause more injury to the passenger.



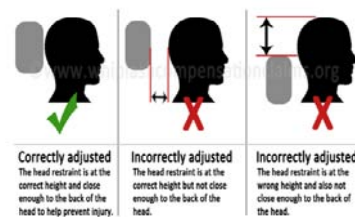
ii. Air Bags

- The impact of an airbag can hurt a passenger who is improperly positioned.
- Injuries from airbags include chest injuries, concussions and whiplash.



iii. Head Rests

- It should be in position to prevent whiplash the head rest should be at least as high as the head's centre of gravity (eye level and higher) and as close to the back of the head as possible.
- But we adjust it often for our comfort and now-a-days TV is fitted in it so the position is completely altered.



II. COMPONENTS PRESENT



MASTER
CYLINDER



SLAVE
CYLINDER



FLEXIBLE
HOSE

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III. PRINCIPLE BEHIND OUR IDEA

The working principle of the idea presented in this paper is when a speeding car hits an object or another vehicle the very first part which hits is the bumper hence behind this there will be a master cylinder which has a piston rod in the extended form so that as soon as the car hits the object the bumper presses the piston rod so inside so that the fluid inside it gets compressed and moves to actuate the slave cylinder, this slave cylinder has a piston rod attached to the passenger seats assembly so that it moves backwards thus the injuries during the accident can be minimized.

IV. CONSTRUCTION

The construction of this idea is very simple the passenger seats are welded or joined to a movable plate which moves on a sliding bearing. The master cylinder is placed at the front end at the backside of the bumper so that during collision the bumper touches the master cylinders piston rod. Then the plate in which the passenger seats are welded (or) joined is attached to the piston rod of the slave cylinder. Then the both cylinders are joined by means of flexible hosing or by a solid one with a check valve in it so that it allows the fluid in only one direction. To the same hosing after the check valve a variable orifice is attached so that the fluid returns at slow speed.

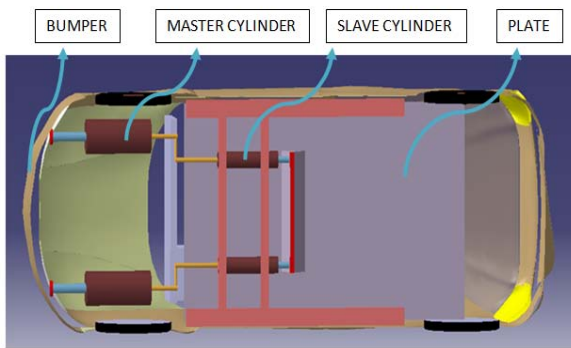
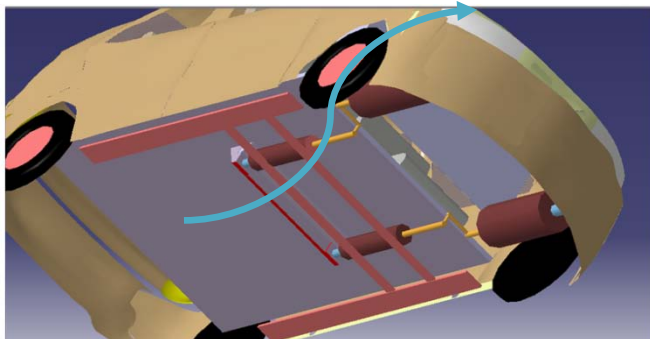
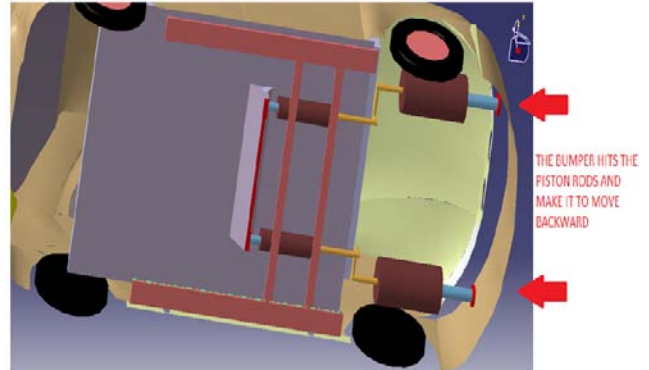


Plate in which seats are welded

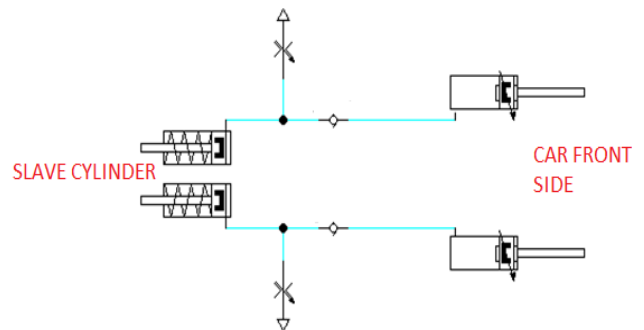


V. WORKING

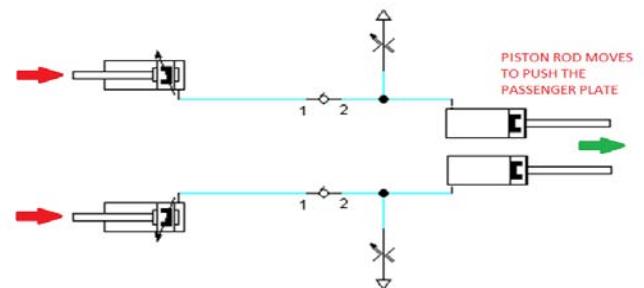
- ✓ When the car hits an object or another car bumper is the first part which faces the collision.
- ✓ As soon as it hits the bumper deforms inside so that it pushes the piston rod of the master cylinder.



- ✓ Below diagram shows the circuit of the above diagram.

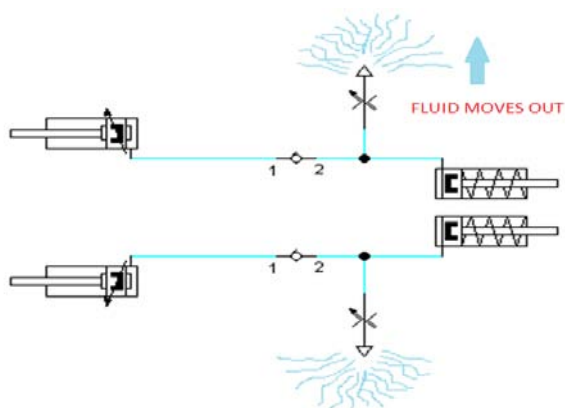


- ✓ When the piston rod of the master cylinder moves it compresses the fluid which is present inside the cylinder so that it sends the fluid to the slave cylinder.
- ✓ Due to the pressure of the fluid it pushes the slave cylinders piston rod.

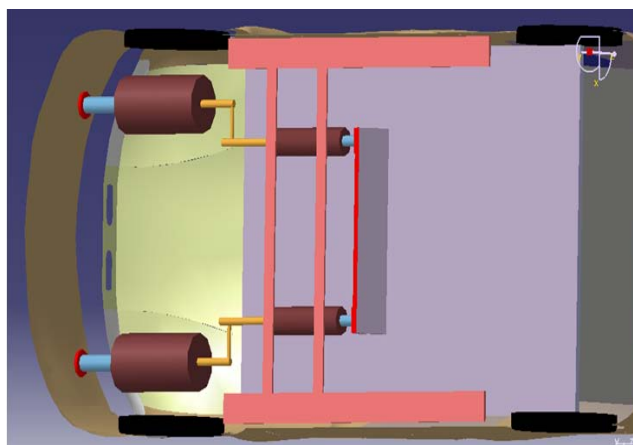
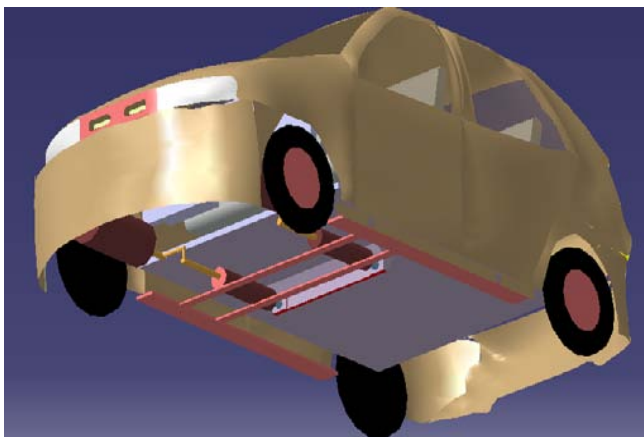
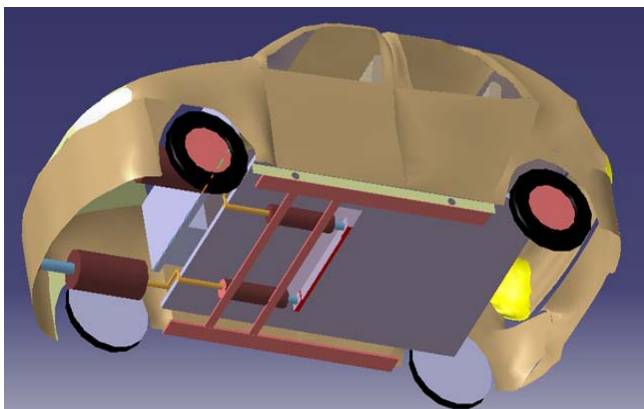


- ✓ Thus the plate in which the passenger seat is welded or joined moves backward and so the passenger especially the driver moves away and avoids major injuries like finger, hands fractures, etc.

- ✓ During minor collisions also this process takes place but this has to be recovered (i.e.) the plate should again come to its original position so that the driver can drive away during minor accidents. For this process to occur a check valve is provided the single acting cylinder is spring return one so its moves to its original position automatically.
- ✓ But the return stroke must be at very low speed hence the fluid is bypassed through a variable orifice valve it allows a very small amount of fluid to move out so the return stroke is achieved at very slow speed.



VI. OTHER IMAGES



a) Advantages of this idea

- ✓ Prevents the injury to the passenger by 80%
- ✓ Simpler process
- ✓ Easy construction and assembly
- ✓ Process is quite cheap

b) Disadvantages of this idea

- ✓ The fluid pressure must be checked frequently
- ✓ May result in vibration

VII. CONCLUSION

On the way of many improvements to increase the safety of passengers now we have found a new way to reduce the injuries caused during accidents. By implementing this idea in the automobiles will be very useful and so the loss of lives can be somehow prevented.

VIII. ACKNOWLEDGEMENT

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Impact of the Smart Textile on the High Level Sport Performance and Patient Behavior in Medicine

By R. Taiar

Université de Reims, France

Abstract- In the present study we developed several proto types which will be intended for the high level sport performance like swimming, triathlon, skiing and medicine. 6 innovative fabric proto types where developed in the aim to answer to the exigencies of the high level sport and medicine. We opted for the high-tech polyamide fiber; in the production of the textile. These innovative processes will be adapted for medical use. The medical example relates the contribution of fabrics in helping hemiplegic patients float on the water's surface. This water rehabilitation will help decrease scabs on hemiplegics by reducing the contact between the body and the wheelchair for instance. Physicochemical analysis has been done for the comparison of the different simple. No significant difference where observed between the textiles in static and dynamic behavior ($P > 0.05$). In the future work the solution that we consider rests on the implementation of a data-processing platform of virtual prototyping in order to simulate all the stages of clothes industry and to lead to the most powerful model of textile specification within times much shorter. CFD (Computational Fluid Dynamics) and human modelization were used for the simulation and where compared to the experimental data for the validation.

Keywords: *wettability, static impact angle, dynamic impact angle, textiles, biomechanics.*

GJRE-A Classification : *FOR Code: 091399*



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I. INTRODUCTION

The textile fibers are of vegetable origin, animal, mineral or chemical (artificial or synthetic). The synthetic fibers or yarns are realized from polymers obtained by synthesis of chemical compounds. The artificial fibers are manufactured, inter alia, starting from regenerated cellulose. The textile innovation in high level sport is characterized by the performance, the functionality, comfort, the fashion and aesthetics. The requirements of the sports activities direct industries towards several optimizations, such as the reduction of friction, the thermoregulation improvement, the mechanical resistance, the safety, and the reduction in perspiration. In the medical environment, a technological development was observed during the ten last years. Based on their barrier effect, at their capacity of absorption, their biocompatibility and their contention capacity, the technical textiles manage to answer multiple features in this sector. For example, the introduction of hydrophilic polymers made it possible to produce perfectly adhesive bandages. The arrival of

certain elastanes and the improvement of a new method of knitting permitted the production of special compression stockings that are pleasant to carry. The development of biocompatible polymeric fibers made possible the use of the textiles in the osteosynthesis prostheses or in vascular surgery. The textile developments today concern not only the imitation of natural fibers, but also the envelopment of new materials that adapt and react to the sensory and body conditions—the clothes we will use in the future will seem like second skin. After breathing fibers, the smart textile fibers adapt to the biological environment of the body. Reference [1] used the microcapsules in the t-shirt and the socks. Several laboratories work on textiles using of the microcapsules containing of the substances with phase shift [2], [3]. The fabrics of Nylon and Lycra, coated with a conducting polymer (polypyrrole) conform to the shape of the human body [4], and function ideally as the biomechanical sensors which can be used in a range of applications to control the human movement. References [5], [6] studied the intrinsic electronic conducting polymers and the installation of the methods of manufacturing of conducting textile fibers. In medicine, 10% of the world technical textile volume are employed for health and can be improved with different technical future textile utilizations [7]. Currently, the smart textiles with integrated sensors are used in the medical field [8]. The new generation of biomedical sensors provides the opportunity for monitoring continually, ambulatory, as well as in residential environments. This generates complete information and allows for improvement of prevention, as well as treatment. Applications of the system “Sensate Liner” are intended for the medical supervision. This program develops and shows useful technologies to apply a systematic approach, making it possible to supervise the medical state of the patients, with a uniform equipped with sensors [8]. Current and future potential applications of three-dimensional polymeric reinforced fabrics manufactured by the processes: weaving, braiding, pricking and knitting, are studied [9]. [10; 11] showed the preliminary results of the application of the textile in the high level sport and medicine. The aim of our study is to show our last textiles development for the high level sport and medicine. The concerns of the present study include swimming, triathlon and skiing

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textiles for sports, and textile used for hemiplegic rehabilitation patients. Different engineering methods were used for the simulation, modelization and optimization fabrics.

II. MATERIAL AND METHODS

a) Fabric

We developed 6 innovative fabric prototypes to answer to the exigencies of the high level athletes in swimming and Triathlon in term of increasing performance and hemiplegic patients in terms of

rehabilitation. The objective is to develop a hydrophobic textile in the aim to decrease the interaction between the drop and the fibers. We opted for the high-tech polyamide fiber and elastanes, in the production of the textile Figure 1. The low density of the fibers makes it possible to produce a very lightweight fabric. The textile absorbs an extremely small amount of moisture, which means that the material cannot become saturated, hence slowing the swimmer down. When wet, polyamide fibers are almost as strong as when they are dry.

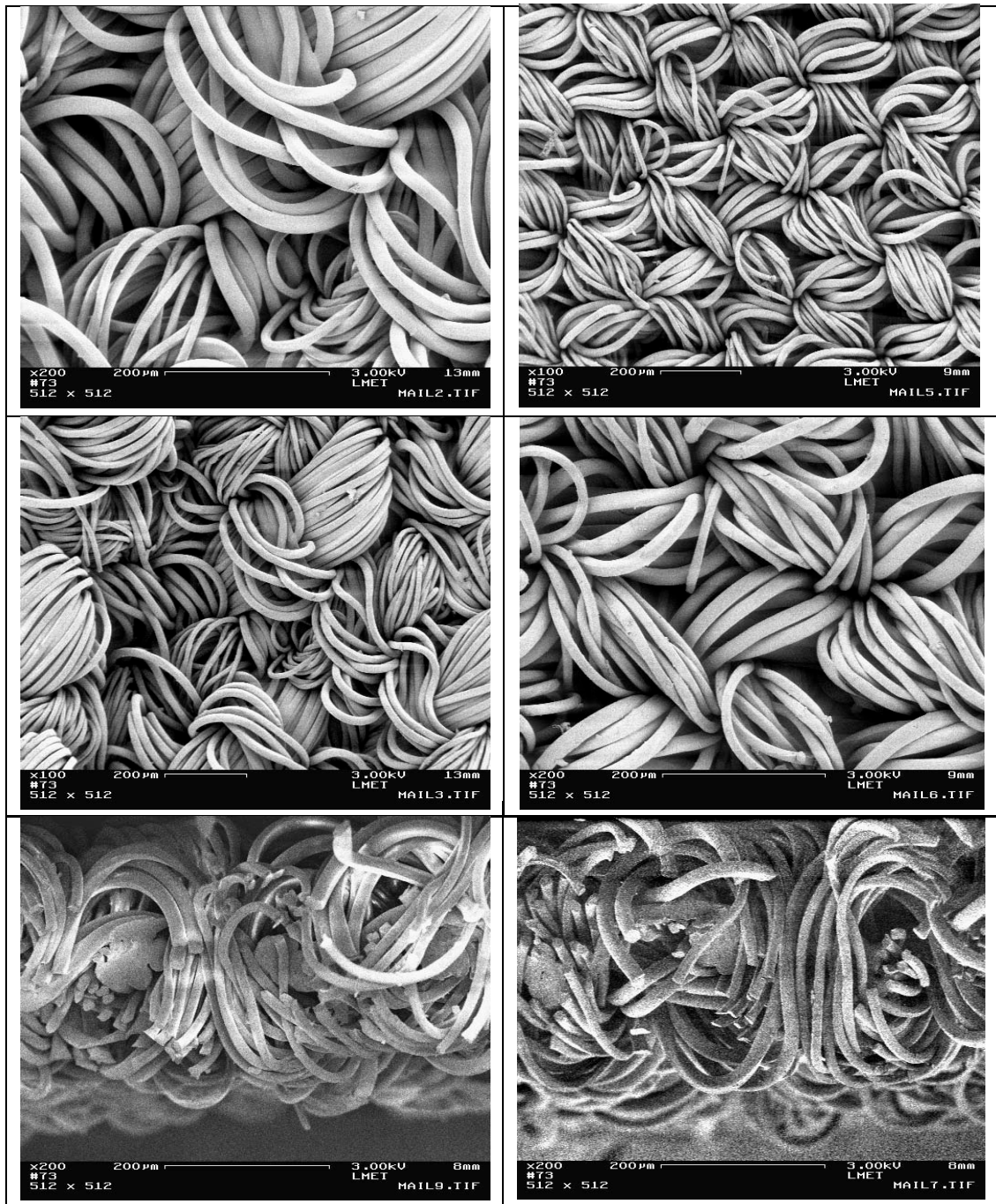


Figure 1 : Scanning Electron Microscopy SEM for the 6 polyamide fibers developed. The pictures obtained are in expansion x 100 and 200

b) In static mode study: Contact angle and disconnecting liquid drop measurements

Static contact angles were measured with a GBX Digidrop apparatus fitted to a tiltable sample carrier supported by an x-y adjustable stage (Figure 2). This sample carrier was capable of a full of 360° rotation. Video cameras with a light source permit the view of the liquid drop. A schematic description of this apparatus is presented in figure below. A finite drop volume of liquid was deposited on the horizontal substrate using a micro syringe. The contact angle is given as a function of time. Contact angle calculation was performed with the GBX scientific instrumentation software. This program allows a 50 image per second's analysis. Image of both side of the drop was captured on a computer. Then the boundary of the drop was analyzed and contact angles

were calculated. An equilibrium contact angle is determined when the drop reaches a metastable equilibrium. All equilibrium contact angles measurements were performed with 5 μ l drops. A minimum of ten measurements are often made and the numbers averaged. A minimum drop volume is predicted for the critical inclined plane conditions. A 15 μ l liquid drop is retained for this experiment, and after drop deposition the plane was slowly tilted. The experimental configuration meant that the camera, light source, and substrate rotated in synchro which made it easier to detect initial drop movement. Just before the drop began to move, the receding contact angle, the advancing contact angle and the critical angle of tilt were recorded. Ten measurements were done for each result.

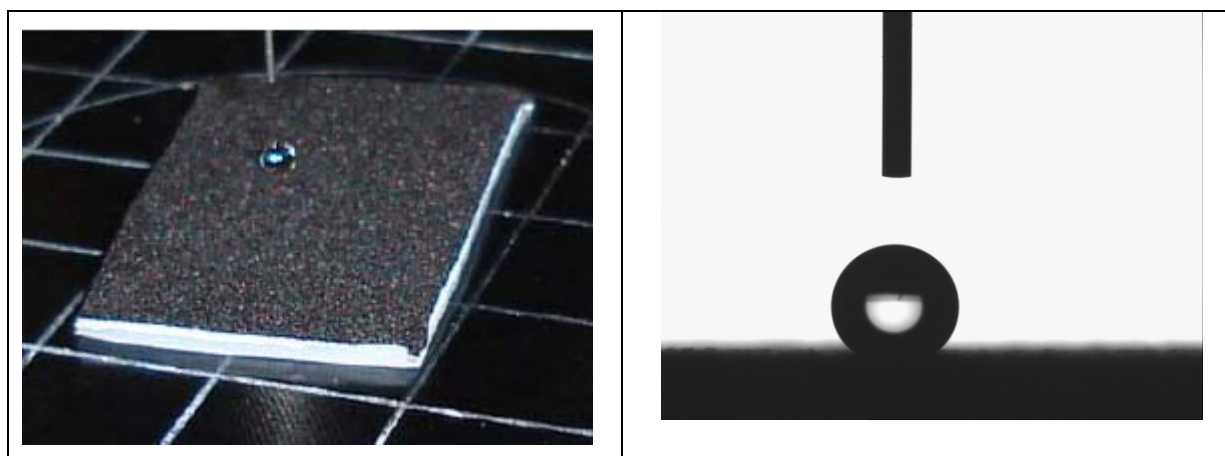


Figure 2 : GBX Digidrop destined for the measure of the contact angle of different material

c) Experience in dynamic mode: method of Wilhelmy

The dynamic advancing and dynamic receding contact angles of water on the swimsuit sample were measured by the Wilhelmy plaque method with K12 Krüss tensiometer. A schematic description of this apparatus is presented in figure below. To begin the measurements, the sample suspended with the bottom edge nearly touching the surface of the liquid. This is the position of the zero force. The sample is lowered until it touches the liquid. This is the zero position. The force on the sample is measured as it is cycled slowly down and up. The depth of immersion of the sample is chosen to 15 mm and the rate of immersion and withdrawal cycles is fixed to 3 mm/min. The waiting time at the returned point is 10 seconds. For a swimsuit sample given, when the immersion and withdrawal cycle is terminated the sample is replaced by another dry sample and the wetting cycle is repeated. Three cycles are repeated in that way. The analysis of these curves allows determining the angles of dynamic impact (angles of

impact forward and backward). In dynamic conditions the name of hysteresis is used. He is defined as the difference between the minimum of the values of contact angle measured, so called receding contact angle (θ_r), and the maximum of the values of contact angle measured, so called advancing contact angle (θ_a). In dynamic, we push the fabric forward we calculate the contact angle and after the same in a backward (Figure 3).

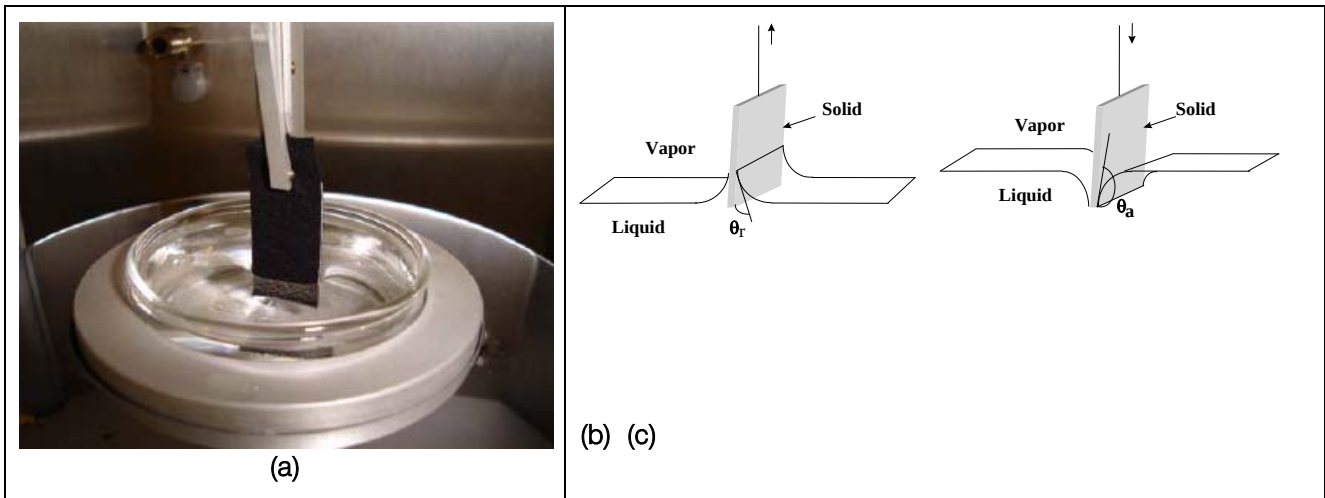


Figure 3 : Illustration of the Wilhelmy plate method in (a), Withdrawal cycle in (b) and Immersion cycle in (c)

III. RESULTS AND DISCUSSION

Different tests were used in the aim to quantify the interaction between the water drop and the fabric. These tests were allowed to study hydrophobicity of the fabric. If the fabric is hydrophobic the materials remain dry and don't get wet. Contrary, if the fabric is hydrophilic the material wet. In this experimentation 6

fabrics have been studied in static (Figure 4) and dynamic conditions (Figure 5). In the figure 4 we can observe the behavior of the drop on the textile. The textile stay hydrophobic in (c) and for another simple (d) the textile absorb the drop and become hydrophilic. In figure 5 the kinetic of the textile behavior during the immersion and immersion phases.

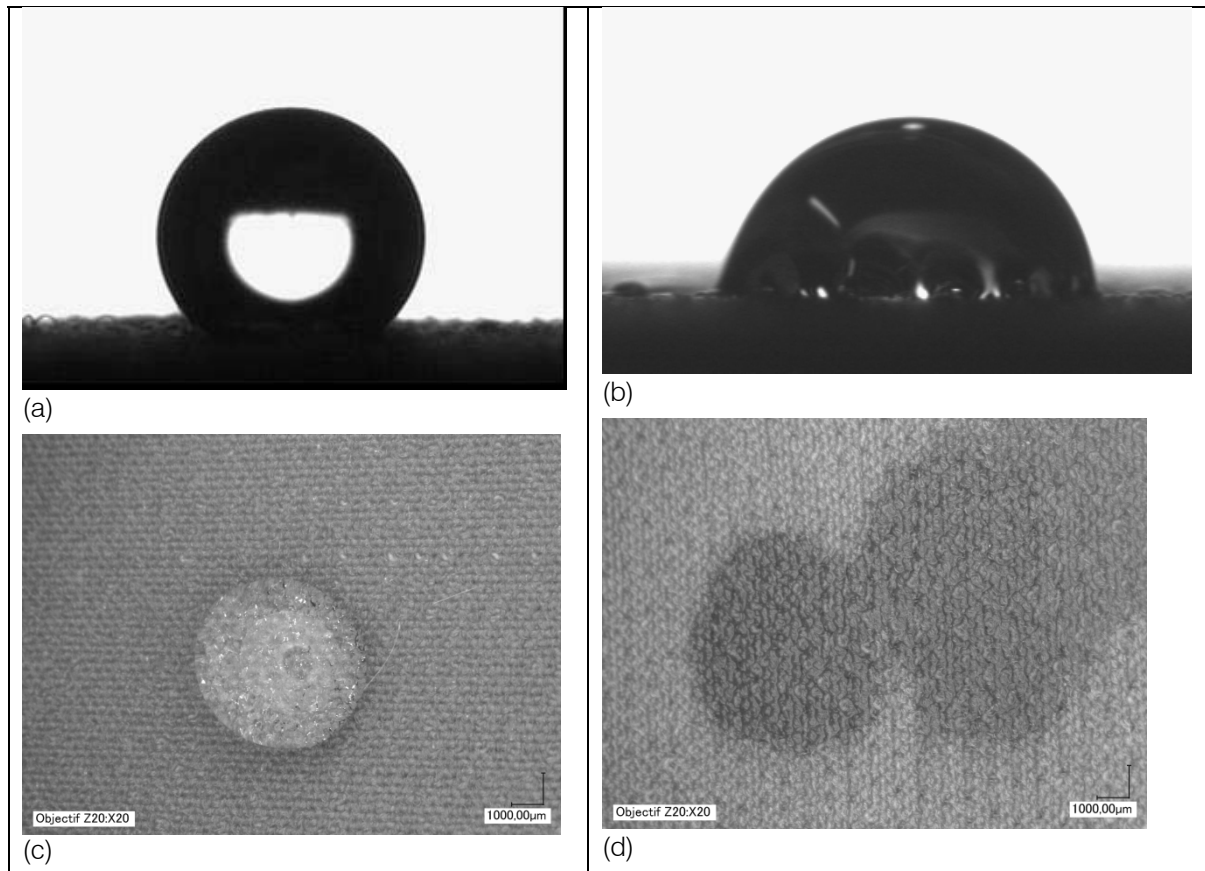


Figure 4 : static drop behavior on the fabric: hydrophobic material in (a) and hydrophilic material in (b). In (c) the behavior of the drop on textile and his absorption in (c)

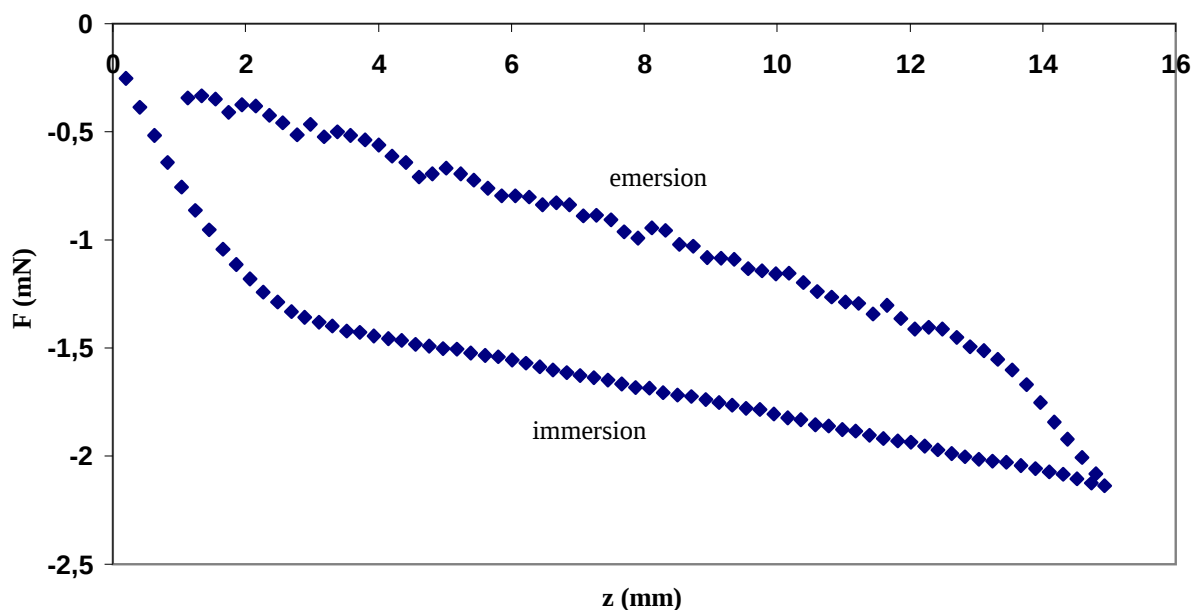


Figure 5 : dynamic drop behavior on the fabric (hysteresis). The material stays hydrophobic during the both phase's emersion and immersion (Wilhelmy plate method)

Our Results showed the hydrophobic characteristics of all the fabrics. In static and dynamic, the angles achieved are close for all the fabrics we studied. They are hydrophobic and stay dry during the experimentation. Like mentioned above the objective

was to develop a hydrophobic textile in the aim to decrease the interaction between the drop and the different fabrics. The Table 1 summarizes the different values of the static and dynamic angles that we obtained.

Table 1 : static and dynamic behaviors of the different textiles

<i>Fabric</i>	θ_E <i>static</i>	θ_A <i>dynamic</i>	θ_R <i>dynamic</i>	$\theta_A - \theta_R$ <i>hystérésis</i>	% diff between static and dynamic teta E and teta A
Textile 1	142°	141°	~ 107°	~ 34°	0,70
Textile 2	140°	136°	~ 117°	~ 19°	2,86
Textile 3	141,5°	132°	~ 109°	~ 23°	6,71
Textile 4	141	139°	~ 90°	~ 49°	1,42
Textile 5	141,5°	132°	~ 108°	~ 24°	6,71
Textile 6	141	133°	~108	~25°	7,13

In the static conditions the angle values are very close numerically to each other (between 140° and 142° in average). The high angle values indicated the hydrophobic characteristics of the different textiles tested. In static the drop maintained its morphology for a long time. The results for the textile behavior stay hydrophobic and remain dry. In dynamic mode, the values for the forward angles are equally close, between 132° and 141°. But, for the backwards contact angle the difference between fabrics is more significant (between 90° and 117°). In dynamic, during the fabric entry into the water the force necessary is more beneficial when the textile is hydrophobic. For the results, the drop doesn't glue to the fabric decreasing, friction and the boundary layer. We noted for both measurements, static and dynamic, that the fabrics stay dry during the experimentations. The hysteresis corresponding to the difference between the forward angle and the backward

angle indicated that the fabrics present hydrophobic behavior. It was weakest for the fabric T2 and strongest for the fabric T4 and can be due to the roughness, or to the heterogeneity of the surface. No significant difference was obtained in comparison of the hysteresis of the fabrics in dynamics and static ($p > 0.05$). In the present study we developed several prototypes which will be intended for high level sport performance like swimming and the triathlon. These innovative processes will be adapted for medical use. The medical example relates the contribution of fabrics in helping hemiplegic patients float on the water's surface. This water rehabilitation will help decrease scabs on hemiplegics by reducing the contact between the body and the wheelchair. The figure 5 showed our first modelization of the wheelchair patient position (a) [12; 13], swimming CAD analysis (b) [14] and skiing in (c).

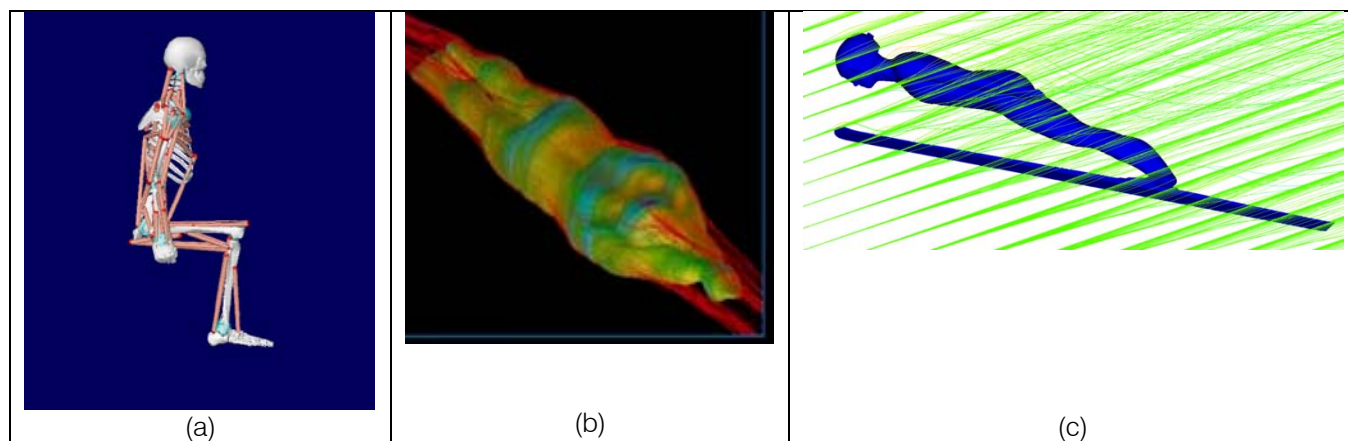


Figure 5 : Modelization and simulation of the body behavior in the different aims of our study: in (a) modelization and simulation of the wheelchair position, in (b) and (c) the swimming and triathlon simulation and skiing in (c)

IV. CONCLUSION

The solutions for medical and sports needs will increasingly take into account mechanical human specifications. In sports, performance improvement in the great events such as the Olympic Games is tributary in part by these textile technologies. They will find their contribution in the amelioration of muscular work, the reduction of hydrodynamical and aerodynamical resistance. In medicine, the advanced textiles will permit the development of assistance solutions tools for patient function, such as passive or active resistance. Our future work will permit to present the results after the experimentation on patients' utilization.

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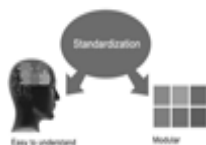
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Based on potential and nature, the manuscript can be categorized under the following heads:

Original research paper: Such papers are reports of high-level significant original research work.

Review papers: These are concise, significant but helpful and decisive topics for young researchers.

Research articles: These are handled with small investigation and applications

Research letters: The letters are small and concise comments on previously published matters.

5. STRUCTURE AND FORMAT OF MANUSCRIPT

The recommended size of original research paper is less than seven thousand words, review papers fewer than seven thousands words also. Preparation of research paper or how to write research paper, are major hurdle, while writing manuscript. The research articles and research letters should be fewer than three thousand words, the structure original research paper; sometime review paper should be as follows:

Papers: These are reports of significant research (typically less than 7000 words equivalent, including tables, figures, references), and comprise:

- (a) Title should be relevant and commensurate with the theme of the paper.
- (b) A brief Summary, "Abstract" (less than 150 words) containing the major results and conclusions.
- (c) Up to ten keywords, that precisely identifies the paper's subject, purpose, and focus.
- (d) An Introduction, giving necessary background excluding subheadings; objectives must be clearly declared.
- (e) Resources and techniques with sufficient complete experimental details (wherever possible by reference) to permit repetition; sources of information must be given and numerical methods must be specified by reference, unless non-standard.
- (f) Results should be presented concisely, by well-designed tables and/or figures; the same data may not be used in both; suitable statistical data should be given. All data must be obtained with attention to numerical detail in the planning stage. As reproduced design has been recognized to be important to experiments for a considerable time, the Editor has decided that any paper that appears not to have adequate numerical treatments of the data will be returned un-refereed;
- (g) Discussion should cover the implications and consequences, not just recapitulating the results; conclusions should be summarizing.
- (h) Brief Acknowledgements.
- (i) References in the proper form.

Authors should very cautiously consider the preparation of papers to ensure that they communicate efficiently. Papers are much more likely to be accepted, if they are cautiously designed and laid out, contain few or no errors, are summarizing, and be conventional to the approach and instructions. They will in addition, be published with much less delays than those that require much technical and editorial correction.



The Editorial Board reserves the right to make literary corrections and to make suggestions to improve briefness.

It is vital, that authors take care in submitting a manuscript that is written in simple language and adheres to published guidelines.

Format

Language: The language of publication is UK English. Authors, for whom English is a second language, must have their manuscript efficiently edited by an English-speaking person before submission to make sure that, the English is of high excellence. It is preferable, that manuscripts should be professionally edited.

Standard Usage, Abbreviations, and Units: Spelling and hyphenation should be conventional to The Concise Oxford English Dictionary. Statistics and measurements should at all times be given in figures, e.g. 16 min, except for when the number begins a sentence. When the number does not refer to a unit of measurement it should be spelt in full unless, it is 160 or greater.

Abbreviations supposed to be used carefully. The abbreviated name or expression is supposed to be cited in full at first usage, followed by the conventional abbreviation in parentheses.

Metric SI units are supposed to generally be used excluding where they conflict with current practice or are confusing. For illustration, 1.4 l rather than $1.4 \times 10^{-3} \text{ m}^3$, or 4 mm somewhat than $4 \times 10^{-3} \text{ m}$. Chemical formula and solutions must identify the form used, e.g. anhydrous or hydrated, and the concentration must be in clearly defined units. Common species names should be followed by underlines at the first mention. For following use the generic name should be constricted to a single letter, if it is clear.

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All manuscripts submitted to Global Journals Inc. (US), ought to include:

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Abstract, used in Original Papers and Reviews:

Optimizing Abstract for Search Engines

Many researchers searching for information online will use search engines such as Google, Yahoo or similar. By optimizing your paper for search engines, you will amplify the chance of someone finding it. This in turn will make it more likely to be viewed and/or cited in a further work. Global Journals Inc. (US) have compiled these guidelines to facilitate you to maximize the web-friendliness of the most public part of your paper.

Key Words

A major linchpin in research work for the writing research paper is the keyword search, which one will employ to find both library and Internet resources.

One must be persistent and creative in using keywords. An effective keyword search requires a strategy and planning a list of possible keywords and phrases to try.

Search engines for most searches, use Boolean searching, which is somewhat different from Internet searches. The Boolean search uses "operators," words (and, or, not, and near) that enable you to expand or narrow your affords. Tips for research paper while preparing research paper are very helpful guideline of research paper.

Choice of key words is first tool of tips to write research paper. Research paper writing is an art. A few tips for deciding as strategically as possible about keyword search:



- One should start brainstorming lists of possible keywords before even begin searching. Think about the most important concepts related to research work. Ask, "What words would a source have to include to be truly valuable in research paper?" Then consider synonyms for the important words.
- It may take the discovery of only one relevant paper to let steer in the right keyword direction because in most databases, the keywords under which a research paper is abstracted are listed with the paper.
- One should avoid outdated words.

Keywords are the key that opens a door to research work sources. Keyword searching is an art in which researcher's skills are bound to improve with experience and time.

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Acknowledgements: Please make these as concise as possible.

References

References follow the Harvard scheme of referencing. References in the text should cite the authors' names followed by the time of their publication, unless there are three or more authors when simply the first author's name is quoted followed by et al. unpublished work has to only be cited where necessary, and only in the text. Copies of references in press in other journals have to be supplied with submitted typescripts. It is necessary that all citations and references be carefully checked before submission, as mistakes or omissions will cause delays.

References to information on the World Wide Web can be given, but only if the information is available without charge to readers on an official site. Wikipedia and Similar websites are not allowed where anyone can change the information. Authors will be asked to make available electronic copies of the cited information for inclusion on the Global Journals Inc. (US) homepage at the judgment of the Editorial Board.

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Tables: Tables should be few in number, cautiously designed, uncrowned, and include only essential data. Each must have an Arabic number, e.g. Table 4, a self-explanatory caption and be on a separate sheet. Vertical lines should not be used.

Figures: Figures are supposed to be submitted as separate files. Always take in a citation in the text for each figure using Arabic numbers, e.g. Fig. 4. Artwork must be submitted online in electronic form by e-mailing them.

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Even though low quality images are sufficient for review purposes, print publication requires high quality images to prevent the final product being blurred or fuzzy. Submit (or e-mail) EPS (line art) or TIFF (halftone/photographs) files only. MS PowerPoint and Word Graphics are unsuitable for printed pictures. Do not use pixel-oriented software. Scans (TIFF only) should have a resolution of at least 350 dpi (halftone) or 700 to 1100 dpi (line drawings) in relation to the imitation size. Please give the data for figures in black and white or submit a Color Work Agreement Form. EPS files must be saved with fonts embedded (and with a TIFF preview, if possible).

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Upon approval of a paper for publication, the manuscript will be forwarded to the dean, who is responsible for the publication of the Global Journals Inc. (US).

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TECHNIQUES FOR WRITING A GOOD QUALITY RESEARCH PAPER:

1. Choosing the topic: In most cases, the topic is searched by the interest of author but it can be also suggested by the guides. You can have several topics and then you can judge that in which topic or subject you are finding yourself most comfortable. This can be done by asking several questions to yourself, like Will I be able to carry our search in this area? Will I find all necessary recourses to accomplish the search? Will I be able to find all information in this field area? If the answer of these types of questions will be "Yes" then you can choose that topic. In most of the cases, you may have to conduct the surveys and have to visit several places because this field is related to Computer Science and Information Technology. Also, you may have to do a lot of work to find all rise and falls regarding the various data of that subject. Sometimes, detailed information plays a vital role, instead of short information.

2. Evaluators are human: First thing to remember that evaluators are also human being. They are not only meant for rejecting a paper. They are here to evaluate your paper. So, present your Best.

3. Think Like Evaluators: If you are in a confusion or getting demotivated that your paper will be accepted by evaluators or not, then think and try to evaluate your paper like an Evaluator. Try to understand that what an evaluator wants in your research paper and automatically you will have your answer.

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7. Use right software: Always use good quality software packages. If you are not capable to judge good software then you can lose quality of your paper unknowingly. There are various software programs available to help you, which you can get through Internet.

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11. Revise what you wrote: When you write anything, always read it, summarize it and then finalize it.



12. Make all efforts: Make all efforts to mention what you are going to write in your paper. That means always have a good start. Try to mention everything in introduction, that what is the need of a particular research paper. Polish your work by good skill of writing and always give an evaluator, what he wants.

13. Have backups: When you are going to do any important thing like making research paper, you should always have backup copies of it either in your computer or in paper. This will help you to not to lose any of your important.

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16. Use proper verb tense: Use proper verb tenses in your paper. Use past tense, to present those events that happened. Use present tense to indicate events that are going on. Use future tense to indicate future happening events. Use of improper and wrong tenses will confuse the evaluator. Avoid the sentences that are incomplete.

17. Never use online paper: If you are getting any paper on Internet, then never use it as your research paper because it might be possible that evaluator has already seen it or maybe it is outdated version.

18. Pick a good study spot: To do your research studies always try to pick a spot, which is quiet. Every spot is not for studies. Spot that suits you choose it and proceed further.

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21. Arrangement of information: Each section of the main body should start with an opening sentence and there should be a changeover at the end of the section. Give only valid and powerful arguments to your topic. You may also maintain your arguments with records.

22. Never start in last minute: Always start at right time and give enough time to research work. Leaving everything to the last minute will degrade your paper and spoil your work.

23. Multitasking in research is not good: Doing several things at the same time proves bad habit in case of research activity. Research is an area, where everything has a particular time slot. Divide your research work in parts and do particular part in particular time slot.

24. Never copy others' work: Never copy others' work and give it your name because if evaluator has seen it anywhere you will be in trouble.

25. Take proper rest and food: No matter how many hours you spend for your research activity, if you are not taking care of your health then all your efforts will be in vain. For a quality research, study is must, and this can be done by taking proper rest and food.

26. Go for seminars: Attend seminars if the topic is relevant to your research area. Utilize all your resources.



27. Refresh your mind after intervals: Try to give rest to your mind by listening to soft music or by sleeping in intervals. This will also improve your memory.

28. Make colleagues: Always try to make colleagues. No matter how sharper or intelligent you are, if you make colleagues you can have several ideas, which will be helpful for your research.

29. Think technically: Always think technically. If anything happens, then search its reasons, its benefits, and demerits.

30. Think and then print: When you will go to print your paper, notice that tables are not be split, headings are not detached from their descriptions, and page sequence is maintained.

31. Adding unnecessary information: Do not add unnecessary information, like, I have used MS Excel to draw graph. Do not add irrelevant and inappropriate material. These all will create superfluous. Foreign terminology and phrases are not apropos. One should NEVER take a broad view. Analogy in script is like feathers on a snake. Not at all use a large word when a very small one would be sufficient. Use words properly, regardless of how others use them. Remove quotations. Puns are for kids, not grunt readers. Amplification is a billion times of inferior quality than sarcasm.

32. Never oversimplify everything: To add material in your research paper, never go for oversimplification. This will definitely irritate the evaluator. Be more or less specific. Also too, by no means, ever use rhythmic redundancies. Contractions aren't essential and shouldn't be there used. Comparisons are as terrible as clichés. Give up ampersands and abbreviations, and so on. Remove commas, that are, not necessary. Parenthetical words however should be together with this in commas. Understatement is all the time the complete best way to put onward earth-shaking thoughts. Give a detailed literary review.

33. Report concluded results: Use concluded results. From raw data, filter the results and then conclude your studies based on measurements and observations taken. Significant figures and appropriate number of decimal places should be used. Parenthetical remarks are prohibitive. Proofread carefully at final stage. In the end give outline to your arguments. Spot out perspectives of further study of this subject. Justify your conclusion by at the bottom of them with sufficient justifications and examples.

34. After conclusion: Once you have concluded your research, the next most important step is to present your findings. Presentation is extremely important as it is the definite medium through which your research is going to be in print to the rest of the crowd. Care should be taken to categorize your thoughts well and present them in a logical and neat manner. A good quality research paper format is essential because it serves to highlight your research paper and bring to light all necessary aspects in your research.

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Key points to remember:

- Submit all work in its final form.
- Write your paper in the form, which is presented in the guidelines using the template.
- Please note the criterion for grading the final paper by peer-reviewers.

Final Points:

A purpose of organizing a research paper is to let people to interpret your effort selectively. The journal requires the following sections, submitted in the order listed, each section to start on a new page.

The introduction will be compiled from reference matter and will reflect the design processes or outline of basis that direct you to make study. As you will carry out the process of study, the method and process section will be constructed as like that. The result segment will show related statistics in nearly sequential order and will direct the reviewers next to the similar intellectual paths throughout the data that you took to carry out your study. The discussion section will provide understanding of the data and projections as to the implication of the results. The use of good quality references all through the paper will give the effort trustworthiness by representing an alertness of prior workings.



Writing a research paper is not an easy job no matter how trouble-free the actual research or concept. Practice, excellent preparation, and controlled record keeping are the only means to make straightforward the progression.

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To make a paper clear

- Adhere to recommended page limits

Mistakes to evade

- Insertion a title at the foot of a page with the subsequent text on the next page
- Separating a table/chart or figure - impound each figure/table to a single page
- Submitting a manuscript with pages out of sequence

In every sections of your document

- Use standard writing style including articles ("a", "the," etc.)
- Keep on paying attention on the research topic of the paper
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- Align the primary line of each section
- Present your points in sound order
- Use present tense to report well accepted
- Use past tense to describe specific results
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Choose a revealing title. It should be short. It should not have non-standard acronyms or abbreviations. It should not exceed two printed lines. It should include the name(s) and address (es) of all authors.



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The summary should be two hundred words or less. It should briefly and clearly explain the key findings reported in the manuscript-- must have precise statistics. It should not have abnormal acronyms or abbreviations. It should be logical in itself. Shun citing references at this point.

An abstract is a brief distinct paragraph summary of finished work or work in development. In a minute or less a reviewer can be taught the foundation behind the study, common approach to the problem, relevant results, and significant conclusions or new questions.

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- Reason of the study - theory, overall issue, purpose
- Fundamental goal
- To the point depiction of the research
- Consequences, including definite statistics - if the consequences are quantitative in nature, account quantitative data; results of any numerical analysis should be reported
- Significant conclusions or questions that track from the research(es)

Approach:

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- Center on shortening results - bound background information to a verdict or two, if completely necessary
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The **Introduction** should "introduce" the manuscript. The reviewer should be presented with sufficient background information to be capable to comprehend and calculate the purpose of your study without having to submit to other works. The basis for the study should be offered. Give most important references but shun difficult to make a comprehensive appraisal of the topic. In the introduction, describe the problem visibly. If the problem is not acknowledged in a logical, reasonable way, the reviewer will have no attention in your result. Speak in common terms about techniques used to explain the problem, if needed, but do not present any particulars about the protocols here. Following approach can create a valuable beginning:

- Explain the value (significance) of the study
- Shield the model - why did you employ this particular system or method? What is its compensation? You strength remark on its appropriateness from a abstract point of vision as well as point out sensible reasons for using it.
- Present a justification. Status your particular theory (es) or aim(s), and describe the logic that led you to choose them.
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Approach:

- Use past tense except for when referring to recognized facts. After all, the manuscript will be submitted after the entire job is done.
- Sort out your thoughts; manufacture one key point with every section. If you make the four points listed above, you will need a least of four paragraphs.



- Present surroundings information only as desirable in order hold up a situation. The reviewer does not desire to read the whole thing you know about a topic.
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Materials:

- Explain materials individually only if the study is so complex that it saves liberty this way.
- Embrace particular materials, and any tools or provisions that are not frequently found in laboratories.
- Do not take in frequently found.
- If use of a definite type of tools.
- Materials may be reported in a part section or else they may be recognized along with your measures.

Methods:

- Report the method (not particulars of each process that engaged the same methodology)
- Describe the method entirely
- To be succinct, present methods under headings dedicated to specific dealings or groups of measures
- Simplify - details how procedures were completed not how they were exclusively performed on a particular day.
- If well known procedures were used, account the procedure by name, possibly with reference, and that's all.

Approach:

- It is embarrassed or not possible to use vigorous voice when documenting methods with no using first person, which would focus the reviewer's interest on the researcher rather than the job. As a result when script up the methods most authors use third person passive voice.
- Use standard style in this and in every other part of the paper - avoid familiar lists, and use full sentences.

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- Resources and methods are not a set of information.
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- Leave out information that is immaterial to a third party.

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The principle of a results segment is to present and demonstrate your conclusion. Create this part a entirely objective details of the outcome, and save all understanding for the discussion.

The page length of this segment is set by the sum and types of data to be reported. Carry on to be to the point, by means of statistics and tables, if suitable, to present consequences most efficiently. You must obviously differentiate material that would usually be incorporated in a study editorial from any unprocessed data or additional appendix matter that would not be available. In fact, such matter should not be submitted at all except requested by the instructor.



Content

- Sum up your conclusion in text and demonstrate them, if suitable, with figures and tables.
- In manuscript, explain each of your consequences, point the reader to remarks that are most appropriate.
- Present a background, such as by describing the question that was addressed by creation an exacting study.
- Explain results of control experiments and comprise remarks that are not accessible in a prescribed figure or table, if appropriate.
- Examine your data, then prepare the analyzed (transformed) data in the form of a figure (graph), table, or in manuscript form.

What to stay away from

- Do not discuss or infer your outcome, report surroundings information, or try to explain anything.
- Not at all, take in raw data or intermediate calculations in a research manuscript.
- Do not present the similar data more than once.
- Manuscript should complement any figures or tables, not duplicate the identical information.
- Never confuse figures with tables - there is a difference.

Approach

- As forever, use past tense when you submit to your results, and put the whole thing in a reasonable order.
- Put figures and tables, appropriately numbered, in order at the end of the report
- If you desire, you may place your figures and tables properly within the text of your results part.

Figures and tables

- If you put figures and tables at the end of the details, make certain that they are visibly distinguished from any attach appendix materials, such as raw facts
- Despite of position, each figure must be numbered one after the other and complete with subtitle
- In spite of position, each table must be titled, numbered one after the other and complete with heading
- All figure and table must be adequately complete that it could situate on its own, divide from text

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The Discussion is expected the trickiest segment to write and describe. A lot of papers submitted for journal are discarded based on problems with the Discussion. There is no head of state for how long a argument should be. Position your understanding of the outcome visibly to lead the reviewer through your conclusions, and then finish the paper with a summing up of the implication of the study. The purpose here is to offer an understanding of your results and hold up for all of your conclusions, using facts from your research and generally accepted information, if suitable. The implication of result should be visibly described. Infer your data in the conversation in suitable depth. This means that when you clarify an observable fact you must explain mechanisms that may account for the observation. If your results vary from your prospect, make clear why that may have happened. If your results agree, then explain the theory that the proof supported. It is never suitable to just state that the data approved with prospect, and let it drop at that.

- Make a decision if each premise is supported, discarded, or if you cannot make a conclusion with assurance. Do not just dismiss a study or part of a study as "uncertain."
- Research papers are not acknowledged if the work is imperfect. Draw what conclusions you can based upon the results that you have, and take care of the study as a finished work
- You may propose future guidelines, such as how the experiment might be personalized to accomplish a new idea.
- Give details all of your remarks as much as possible, focus on mechanisms.
- Make a decision if the tentative design sufficiently addressed the theory, and whether or not it was correctly restricted.
- Try to present substitute explanations if sensible alternatives be present.
- One research will not counter an overall question, so maintain the large picture in mind, where do you go next? The best studies unlock new avenues of study. What questions remain?
- Recommendations for detailed papers will offer supplementary suggestions.

Approach:

- When you refer to information, differentiate data generated by your own studies from available information
- Submit to work done by specific persons (including you) in past tense.
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INDEX

A

Amelioration · 40
Anisotropic · 23

C

Collisions · 30

H

Hemiplegic · 33, 35, 39, 41

S

Susceptance · 14, 16, 17

T

Triathlon · 33, 34, 39, 40
Tributary · 40

V

Vividly · 14

W

Wettability · 33



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