

Ellipse's Perimeter Evaluation

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Abstract: This is a trendy problem since the time of Kepler (1609). He was asked what the length of the elliptical orbits is. Even today, thousand of mathematicians are working on this matter. Ramanujan, a super mathematician (1914) from India, is the Master of all these researchers. But, no one of them considered that the orbits are not elliptical. Their mind was blocked by the laws of Kepler for 400 years. Orbit's length and ellipse's perimeter are two different matters. In these papers we will treat mathematical ellipse. Orbits are not elliptical

Keywords: perimeter estimation, ellipse, other astroids, cracking Thales

I. INTRODUCTION

Thales theorem $B/A=c/d$ is well known by everyone. No! No one of the mathematicians knows the generalized Thales theorem. Generalized Thales theorem explains the total arc length on positive Cartesian. Like Pythagoras ($a^2+b^2=c^2$), generalized Thales is ($a^s+b^s=K^s$)

So first, we must start by understanding Thales theorem. Then after we will attack the total arc length of the astroids $(x/a)^r+(y/b)^r=1$. When $r=2$ the astroid is an ellipse.

Fig.1 shows what we know and what we should know about Thales.

On the left is what we know; on the right is what we must be aware.

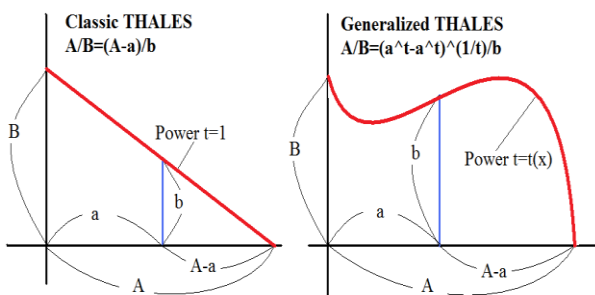


Fig.1

In fact, for an astroidal expression $(x/A)^t+(y/B)^t=1$ where $t=t(x)$, variable (t), simply when $x=a$ $y=b$ is found.

As a consequence, the relation of the coordinates at the touching point P of (t variable) astroid with (r constant) astroid is shown on Fig.2

$$A/B=(A^t-x^t)^{(1/t)}/y \quad (a)$$

$$a/b=(a^r-x^r)^{(1/r)}/y \quad (b)$$

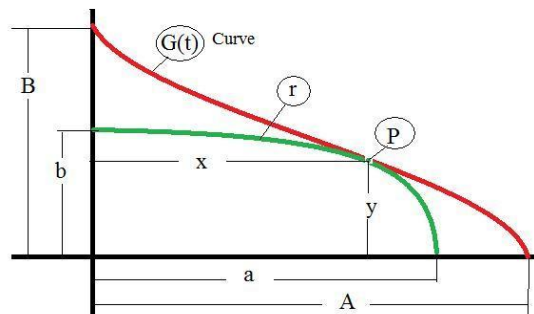


Fig. 2

And it exists an $s=r*t/(r-t)$ which gives the relation

$$A/B=(A^s-a^s)^{(1/s)}/b. \quad \text{Fig.3} \quad (c)$$

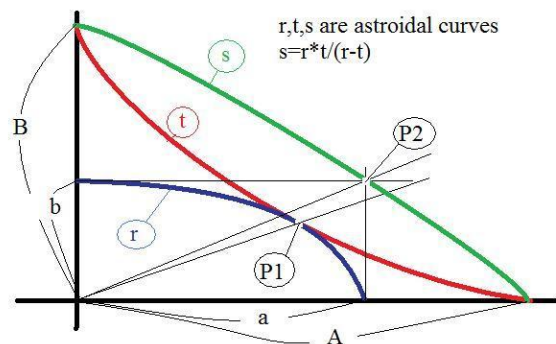


Fig. 3

$$\text{That is to say: when } A=B=K \quad a^s+b^s=K^s \quad (d)$$

And, when K is the length (L1) of the (r=constant) astroid (arc length on the positive Cartesian), the expression (d) is commented as

$$1+\text{TAN}^s=L1^s \quad (e)$$

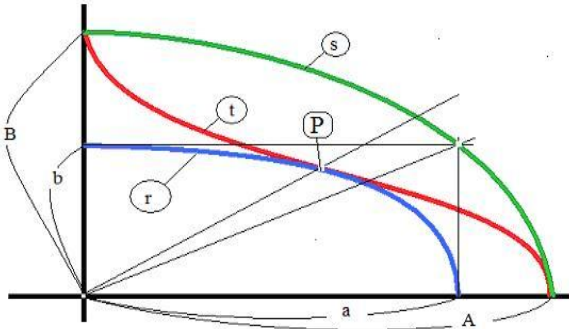
Where $\text{TAN}=b/a$.

Therefore the expression (d) is an **equivalent** to the elliptic integrals, with which we evaluate the total arc length on the positive Cartesian.

Then we may evaluate any astroidal value (area, length,...) without use of integrals for any (r):
 Say K=total arc length on positive Cartesian, evaluate L1
 Say K=total area on positive Cartesian, evaluate Areas
 Say K= any elliptical subject, evaluate this subject, without use of integrals.

Existence of (s) : proof (dated 1959.03.24
 Istanbul/Turkey)

Consider Fig.4



. 4

The astroid family

$$(x/a)^r + (y/b)^r = 1 \quad (1)$$

where $r = \text{Constant}$, is enveloped by

$$(x/A)^t + (y/B)^t = 1 \quad \text{where } t = t(x) \quad (2)$$

We search for a relation $f(a, b, r, A, B, t) = 0$

At the touching point (P) of the graphs we write

-the slopes are equal

-the coordinates are equal

For the coordinates we write

$$y = b/a * (a^r - x^r)^{1/r} = B/A * (A^t - x^t)^{1/t} \quad (3)$$

For the slope of the enveloped astroid we write

$$\begin{aligned} dy/dx &= -(b/a)^r * (x/y)^{r-1} \\ dy/dx &= -(b/a) * ((x^r)/(a^r - x^r))^{(r-1)/r} \end{aligned} \quad (4)$$

For the slope of the envelope itself :

$$\text{say } (x/A)^t = U ; (y/B)^t = V \text{ then,} \quad U + V = 1 \quad (5)$$

$$dU + dV = 0 \quad (6)$$

we have

$$\begin{aligned} t * \ln(x/A) &= \ln U \\ t * \ln(y/B) &= \ln V \end{aligned} \quad (7)$$

When we differentiate (7), we write

$$\begin{aligned} dt * \ln(x/A) + t * (dx/x) &= dU/U \\ dt * \ln(y/B) + t * (dy/y) &= dV/V \end{aligned} \quad (8)$$

and there from,

$$\begin{aligned} dU &= U * (dt * \ln(x/A) + t * (dx/x)) \\ dV &= V * (dt * \ln(y/B) + t * (dy/y)) \end{aligned} \quad (9)$$

Considering (7), the expression (6) is written as

$$U * (dt * 1/t * \ln U + t * dx/x) + V * (dt * 1/t * \ln V + t * dy/y) = 0 \quad (10)$$

and there from

$$V * t * dy/y = -U * (dt * \ln U + t * dx/x) - V * (dt * \ln V \quad (11)$$

$$dy/dx = y/(V * t) * U * ((dt/dx * 1/t * \ln U + t/x) + V * dt/dx * 1/t * \ln V) \quad (12)$$

taking (U and t/x) out of the parenthesis

$$dy/dx = U/V * y/x * (1 + dt/dx * x/t^2 * 1/U * (U * \ln U + V * \ln V)) \quad \text{is written} \quad (13)$$

say

$$N = (1 + dt/dx * x/t^2 * 1/U * (U * \ln U + V * \ln V)) \quad (14)$$

$$dy/dx = -U/V * y/x * N \quad \text{is written} \quad (15)$$

For the equality of the slopes, we write (15)=(4). Considering also (3), we write

$$(b/a) * ((x^r)/(a^r - x^r))^{(r-1)/r} = U/V * 1/x * (B/A) * (A^t - x^t)^{1/t} * N \quad (16)$$

Replacing (4) and (5) in (16) we write

$$(b/a)^r * (x/y)^{r-1} = (B/A)^t * (x/y)^{t-1} * N \quad (17)$$

$$\text{say} \quad (B/A) = E \quad (18)$$

Use (3), we write (17) as follows

$$(b/a)^r = E^t * (x/(E * (A^t - x^t)^{1/t}))^{t-1} * N \quad (19)$$

and there from

$$b^r = E^r * a^r * (x^t/(A^t - x^t))^{(t-r)/t} * N \quad (20)$$

is written

using (3) and (20), the expression (1) is written as follows

$$(x/a)^r + ((A^t - x^t)^{1/r} / t) * (A^t - x^t)^{1/t} / (t-r) / a^r * x^{t-r} * N = 1 \quad (21)$$

$$x^t * N + A^t - x^t = a^r * x^{t-r} * N \quad (22)$$

$$A^t = a^r * x^{t-r} * N - x^t * (N-1) \quad (23)$$

Then, from (23) we get

$$x = ((A^t - x^t * (1-N)) / a^r * N)^{1/(t-r)} \quad (24)$$

$$a^r * x^{t-r} * N = A^t - x^t * (1-N) \quad (25)$$

using (25) in (20)

$$b^r = E^r * (A^t - x^t * (1-N)) / (A^t - x^t)^{1/t} / t$$

$$A^t = (b/E)^r * (A^t - x^t)^{1/t} / t + x^t * (1-N) \quad (26)$$

is written

$$(26) = (23) \quad \text{then,}$$

$$(a/b^r * E)^r * x^{t-r} * N = (A^t - x^t)^{1/t} / t \quad (27)$$

is written

$$A^t - x^t = (a/b^r * E)^r * (r^t / (t-r)) * x^t * N^{1/t} / t \quad (28)$$

is written

$$A^t = x^t * (1 + ((a/b^r * E)^r * (r^t / (t-r)) * N^{1/t} / t)) \quad (29) \text{ is written}$$

$$\text{From (29) we get (x)}$$

$$x = A / (1 + ((a/b^r * E)^r * (r^t / (t-r)) * N^{1/t} / t))^{1/t} \quad (30)$$

$$(30) = (24) \quad \text{then,}$$

$$((A^t - x^t * (1-N)) / a^r * N)^{1/(t-r)} = A / (1 + ((a/b^r * E)^r * (r^t / (t-r)) * N^{1/t} / t))^{1/t} \quad (31)$$

$$(A^t - x^t * (1-N)) / a^r * N = (A^t - x^t)^{1/t} / t + (a^r * E)^r * (r^t / (t-r)) * N^{1/t} / t \quad (32)$$

We take $((t-r)/r^t)$ power of both sides,

We proceed, then we take the power $(r^t/(t-r))$ of both sides

$$\text{say} \quad r^t/(t-r) = s \quad (33)$$

we write

$$(A^t - x^t * (1-N))^{1/s} * A^t = a^s * N^{1/s} + (b/E)^s \quad (34)$$

For the astroids of the same power, when $b/a = \text{TAN} = \text{Constant}$

$dt/dx = dt/d\text{TAN} * d\text{TAN}/dx = 0$ and $N=1$ then, Figure 5.

(35)

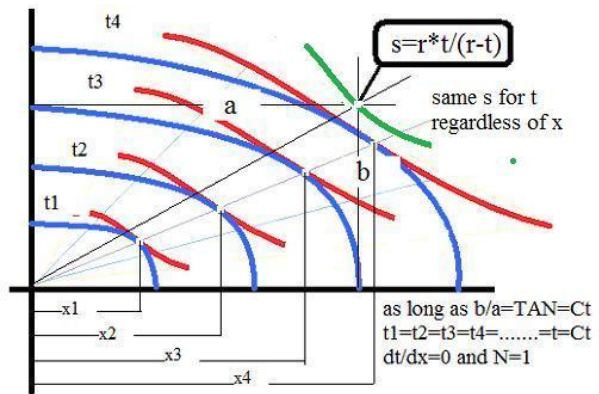


Fig.5

$$A^t * (t^s/r) * A^t = A^s = a^s + (b/E)^s \quad (36)$$

is written

that is as a general expression:

$$(a/A)^s + (b/B)^s = 1 \quad (37)$$

In a symmetric case, when $(A=B=K)$, we write

$$K^s = a^s + b^s \quad (38)$$

$$\text{Say} \quad (K/a = L1); \quad \text{also say } b/a = \text{TAN}$$

$$L1^s = 1 + \text{TAN}^s \quad (38)L$$

is written

$$L1 = (1 + \text{TAN}^s)^{1/s} \quad \text{is proofed, found.}$$

That is the equivalent of the astroidal finite integrals . Insolvable integrals!!!

$$L = a \int_0^1 (1 + (b/a)^2 * (k' / (1 - k'^2))^{(2r-2)/r})^{1/2} dk$$

Expression (38) treats all the mathematical astroids

$(x/a)^r + (y/b)^r = 1$, ellipse included (case $r=2$)

Give any meaning to (K/a) , crack the implicit expression $(K/a)^s = 1 + \text{TAN}^s$

Say:

(K/a) is the total arc length

evaluate $L1$ on the positive Cartesian

(K/a) is the total area

evaluate Area1 on the positive Cartesian

(K/a) is any astroidal subject

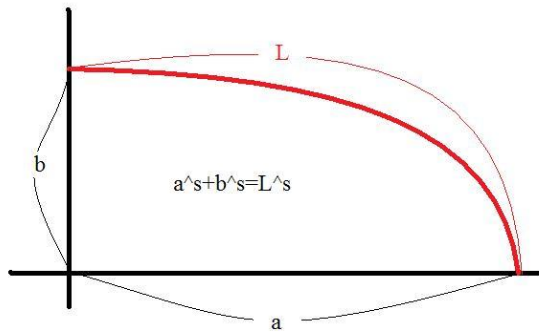
evaluate this

subject on the positive Cartesian

A cracking method:

By trend, ellipse's perimeter will be estimated. Consider

Fig.6. According Thales $a^s + b^s = L^s$



g.6

$s = s(a, b, r) = r \cdot t / (r - t)$ where (t) is variable. So (s) is variable, is an implicit power. When speaking about lengths, one should know the length (L) to evaluate (s) . But if we know (L) we don't need to evaluate (s) . If we know (s) we know (L) . So first, we must crack Thales $L^s = a^s + b^s$ and find an estimable expression for (s) .

Various approximation steps are indicated here below to reach to the "most accurate cracking" When we say we know $(L1)$, the unit length on the positive Cartesian, we mean $(L1)$ evaluated by summing billion of $(dL1)$ arc segments. Suppose, we don't know what an integral is!

Version $s = \text{Constant}$

we know $L1_{\text{exact}} = (\pi/2) \cdot R$, when we speak of circles.
from $L1 = (1 + (R/R)^s)^{1/s} = (\pi/2) \cdot R$ we get
 $s_{\text{min}} = \ln(2) / \ln(\pi/2)$
 $s_{\text{min}} = 1,53492853566138..$

When used for the whole TAN range, this gives the error graph (Fig.7). Max.error % = 0,003605937....at TAN = 5,006784983..

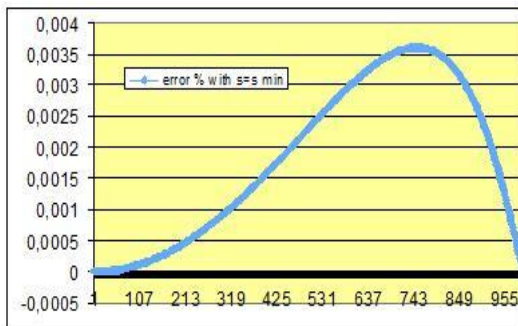


Fig.7

Error % for $1 < \text{TAN} < \infty$. Max.error % = 0,003605937....at TAN = 5,006784983..

Version $s = s_{\text{min}} + m \cdot \text{TAN}$ (Linear variable)

we know $L1_{\text{Exact}} = 636,62517105986...$ for TAN(89,91 o) = 636,6192488...

from $L1_{\text{max}} = (1 + \text{TAN}_{\text{max}}^s)^{1/s}$ we get
 $s_{\text{max}} = 1,71122902010321...$ then, according to the value of TAN

$s = s_{\text{min}} + (s_{\text{max}} - s_{\text{min}}) / (\text{TAN}_{\text{max}} - 1) \cdot (\text{TAN} - 1)$
 $s = 1,53492853566138 + 0,000277355 \cdot (\text{TAN} - 1)$ is evaluated

This gives the error graph (Fig.8)

Max.error % = 0,003477761.....at TAN = 4,966157118..

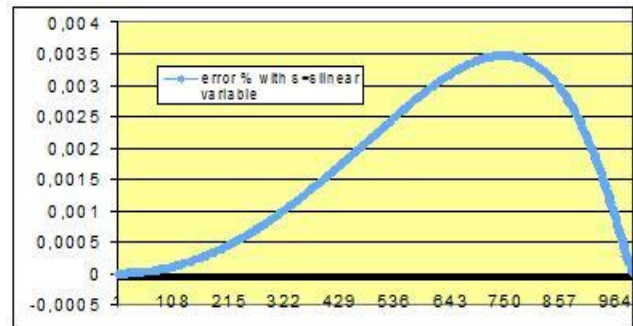


Fig.8

Error % for $1 < \text{TAN} < \infty$. Max.error % = 0,003477761.....at TAN = 4,966157118..

Version $(s = s_{\text{Mod}}; \text{a power version, with } p = 2,98 \text{ constant})$
we know all $L1_{\text{Exact}}$.
an (s_{Exact}) data is obtained. Fig.9

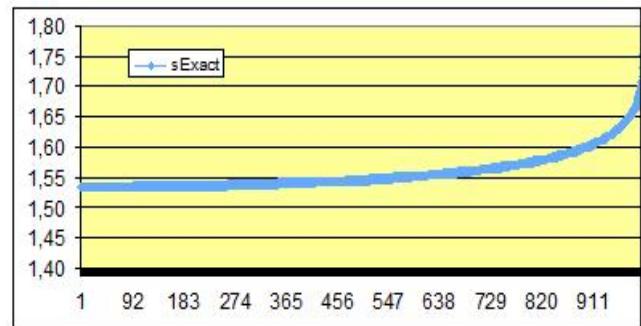


Fig.9

s_{Real} for $1 < \text{TAN} < \infty$

By similarity to an astroid, we write an (s_{Mod}) overlapping the (s_{Real}) . We start a cracking.

$s_{\text{Mod}} = \text{astroid} + \text{polynome}$

$s_{\text{Mod}} = d1 + b1 \cdot (1 - (x - c1)/a1)^p)^{1/p} + (F + m1 \cdot x^{v1} + n1 \cdot x^{w1})$. Proposed as a cracking method.

where, for 1000 lines of evaluation on an excel table

Angle step	$= (90 - 45) / 1000$
x	$= (\text{Angle} - 45) / \text{Angle step}$
Angle o	$= (45 + \text{angle step} \cdot x)$
ATAN	$= \text{angle o} \cdot \pi / 180$
Angle o	$= \text{ATAN} \cdot 180 / \pi$

Fig.10 shows the overlapping with the proposed parameter values of the Table I

parameters	values
	$\sim \sim \sim$ 1,534928535661380

Table I

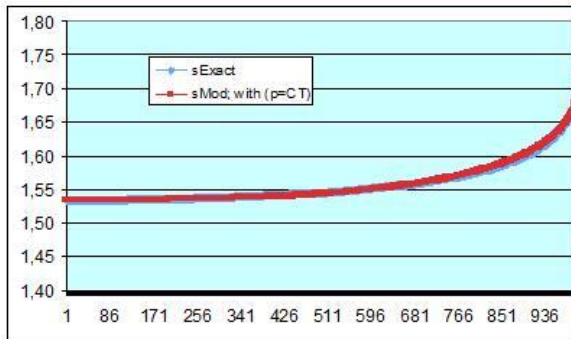


Fig.10 Overlapping of sExact&sMod with
p=Constant=2,98

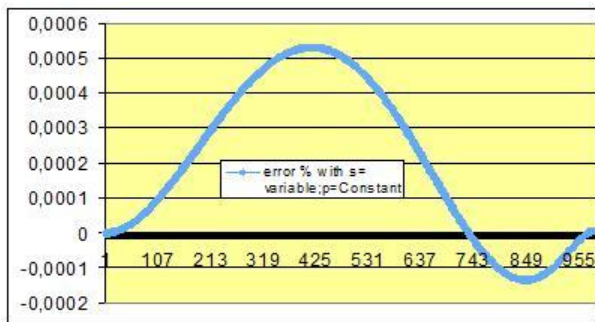


Fig.11
Error % for $1 < \text{TAN} < \text{infinity}$ with $p=2,89$. Max error
%=0,000529940 ..at $\text{TAN}=2,0211255..$

Version (s=sMod with p=pMod; power version, with p=variable)

we know all L1 exact

we know the overlapping sExact&sMod

we write error %, for this overlapping=0,this is to

write: $(sMod-sExact)/sMod=0$

which gives a new value for (p) at every different TAN.

The graph of this new (p) looks like an astroid.

We write a pMod for this pExact data, with the following parameters of Table II

$$pMod = d2 + b2 * (1 - ((x - c2) / a2)^q)^{(1/q)} + (G + m2 * x^v2 + n2 * x^w2)$$

parameters	values
a2	500
b2	0,3
c2	500
d2	0,000
q	6
G	1,965
m2	0,000996000
v2	1
n2	0
w2	1

Table. II

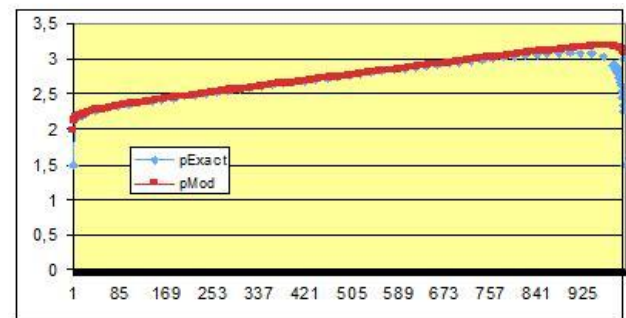


Fig.12
Overlapping of pExact&pMod. For $1 < TAN < infinity$

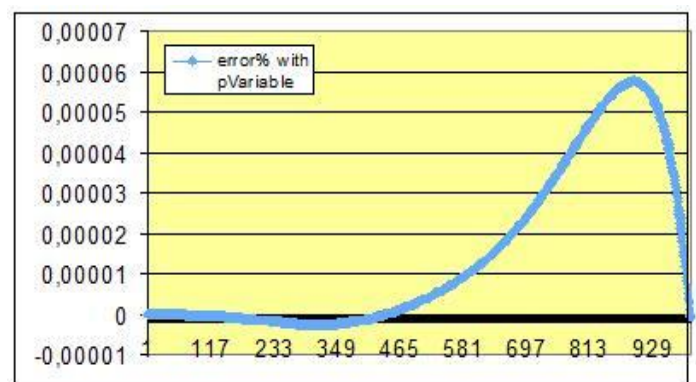


Fig.13 Error % for (1<TAN<infinity) (p variable)
 .Max.Error %=0,00005769.... at TAN=12,0985895...

Version (s=sMod with p=pMod; power version, with p=variable, corrected)

we know all L1 exact

we know the overlapping pExact&pMod

we write error % for this overlapping=0, that is:

$$(pMod-pExact)/pMod=0 \text{ and}$$

we attack the parameter (b2,m2,G) of pMod consecutively.

All these parameters have an astroidal looking. (This is a proposal)

parameters	values
	500
	0,000000
	1,600000

Table III. b2 parameter correcting pMod

parameters	values
	1

Table IV.m2 parameter correcting pMod

parameters	values
	1,4

TableV. G parameter correcting pMod

Now, with these corrections we write

$$pMod = d2 + b2Mod * (1 - ((x - c2)/a2)^q)^{(1/q)} + (GMod + m2Mod * x^v2 + n2 * x^w2)$$

$$sMod = d1 + b1 * (1 - ((x - c1)/a1)^pMod)^{(1/pMod)} + (F + m1 * x^v1 + n1 * x^w1)$$

Error % is reduced as shown on Fig.14

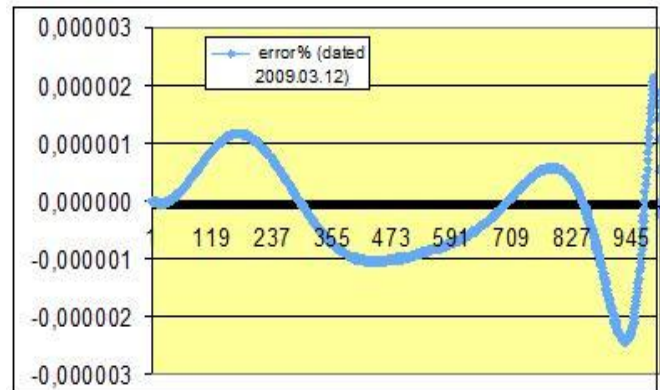


Fig.14 Error % for $1 < TAN < \infty$ (p corrected, coarse).Max.error %=-0,0000024328...at $TAN=18,43467933..$

A numerical example

Evaluate the total arc length of the ellipse ($a=1;b=5$), on positive Cartesian

Consider 1000 evaluating lines on an excel table, for $1 < TAN < \infty$. Use the following designations:

	ATAN*180/Pi

We calculate:

$$\begin{aligned} TAN &= b/a &= 5 \\ ATAN & &= 1,373400767.. \\ Angle \ o & &= 78,69006753 \ o \\ x & &= 748,66817.. \end{aligned}$$

we use (x) value in b2,m2,G,in their formula we get

$$\begin{aligned} b2Mod &= 0,288740099 \\ m2Mod &= 0,000997983 \\ GMod &= 1,948787387 \quad \text{then,} \\ pMod &= 2,99518385 \\ sMod &= 1,567203335 \end{aligned}$$

are evaluated

Use (sMod) in L1 $= (1 + \text{TAN}^{\text{sMod}})^{(1/\text{sMod})}$
 Find L1Estimated $= 5,25251332979251$
 L1 Exact $= 5,25251113492227$ (with tools,
 mathematica, or)
 Error % $= 0,000000418041087.. !!!$

The cracking method is valid for all mathematical astroid.

$(x/a)^r + (y/b)^r = 1$

For all $(0 < r < \infty)$

For all $(1 < \text{TAN} < \infty)$

Error % level is depending of the proposed math-Model.

Proposed math-Models may be cycloidal, polynomial, any function suitable for overlapping.

The equivalency formula of the elliptic finite integrals $K = (1 + \text{TAN}^s)^{(1/s)}$ means: total arc length, or area of the astroids, or ... what else.

It is explained by the generalized Thales theorem!

It has nothing common with Hölder mean.

One may go further for better accuracy, with better proposition of math-Models

II. CONCLUSION

Fig.15 is a comparison graph of Ramanujan's and

Necat's estimation

Ramanujan is Master when $\text{TAN} < 2,5$

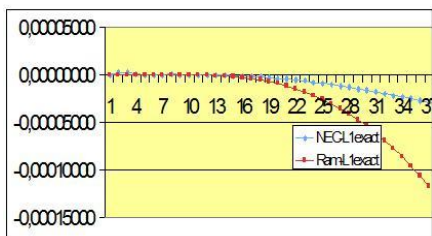


Fig.15 Field $1 < \text{TAN} < 10$ is considered.

Ref: IAENG WCECS2008 conference book, page 944